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SHARP NOSE LENS DESIGN
USING REFRACTIVE INDEX
GRADIENT

ODED AMICHAH

JUNE 1982

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Prepared for:
Naval Postgraduate School
Monterey, California 93940

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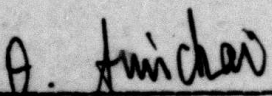
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The work reported herein was carried out for the Naval Postgraduate School by Dr. Oded Amichai under Contract Number N00228-81-C-H231. The work presented in this report is in support of the DARPA/AIFS project. The work is a continuation of earlier research efforts by several thesis students. An age-old problem is the conflict between optical quality and aerodynamic performance for infrared domes. The research may provide a means to circumvent the problem through use of gradient refractive index. The project on Navy Applications of AIFS is funded by Defense Advanced Research Projects Agency and is under the cognizance of Professor A. E. Fuhs.

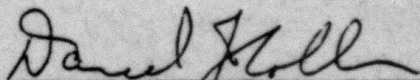
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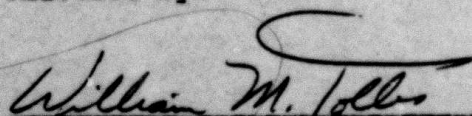

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Features of the computer program include the following: use of many subroutines for clarity and for easy modification, and use of program structure for easy integration into an optimization code.

Sample lens designs and lens performance are presented. The computer code provides the tools for lens design. Considerable additional work is needed for selecting the best lens design.

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ABSTRACT

For infrared sensors located at the nose of a missile or a projectile, an age-old problem occurs. A conflict between optical quality and aerodynamic drag exists. A new approach for solving this problem is being developed using gradient refractive index, GRIN, for lens design. The equations for lens design incorporating GRIN are formulated for the special case of spherically symmetrical GRIN. A computer code for designing a GRIN lens and for determining aberrations has been developed. A different program (LENS) calculates lens design and lens performance for the case of homogeneous refractive index. Results of this program provide a check on the more complex program which includes GRIN. The computed program calculates the spot diagram for both meridional and skew rays. The spot diagram, which is the intersection of rays with the focal plane, is plotted, and the σ_{rms} and centroid location of the spot diagram are calculated. Also a cumulative energy diagram is obtained from the program. The computer code has been organized to calculate the items enumerated above for either a circular cone for the inside or outside surface of the pointed lens. For homogeneous refractive index, both cases are included in the program discussed in this report. However, for the GRIN case, only the complete program for a lens with a conical surface on the outside is reported here. The alternate case is being developed by a thesis student.

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1. INTRODUCTION

A long-term conflict exists between optics and aerodynamics for missile nose design. Optics requires a blunt shaped nose similar to that used on the Sidewinder missile. Favorable aerodynamics for supersonic missiles requires a sharp nose which permits an attached shock wave. For rocket powered missiles or projectiles, the sensor and associated optics occupies the complete nose area. The penalty of a blunt nose is high drag. For ramjet propelled missiles or projectiles, the penalty of a blunt nose is poor pressure recovery by the inlet; this statement assumes a nose inlet is used.

In times past, the lens designer had available three design parameters; a satisfactory lens in the general shape of a cone has not been designed. A lens can be designed using homogeneous refractive index which focuses rays; however, off-axis rays have very large aberrations. The thesis by Terrell [1] discusses the design of a conical lens.

A fourth design parameter has become available which is spatially variable refractive index. The associated technology is known as GRIN; see references [2-13]. GRIN is short notation for Gradient Refractive Index. The thesis by Frazier [14] briefly introduced the use of GRIN in lens design; likewise the thesis of Terrell [1] has a brief discussion. The thesis of Carr [15] will have more extensive results.

The development of materials which have variable refractive index has been motivated by optical fiber technology. Optical fibers can propagate a single mode with low losses if an ap-

appropriate spatial variation of refractive index exists. Based on the information in reference [2], the maximum variation of GRIN is limited to a few percent. The report contains twelve sections. In section 3 the problem of the homogeneous case is solved (program LENS) while the GRIN lens design is formulated in section 4 (program GRIN). The flow charts to the computer programs are given in section 5 and 6, and a user's guide to each of the programs is illustrated in section 7. The programs are listed in sections 9 and 10.

2. BRIEF OVERVIEW OF PROBLEM FORMULATION

Define the axial distance as x and radial distance as r in a cylindrical coordinate system. The lens is to be axisymmetric so that angle is not a variable.

In general the shape of the front surface, is a function of r

$$x = F_f(r) \quad (2.1)$$

where subscript f denotes front surface. Likewise the rear surface is a function of r

$$x = F_r(r) \quad (2.2)$$

where subscript r indicates the rear surface.

As a simplification, either the front or rear surface is a circular cone. Terrell [1] treated the case of a conical front surface; Carr [15] is investigating the case of a conical rear surface. This report develops a computer code which calculates either case. A single consistent computer program is used for both cases; this fact is important for application

of optimization codes.

In general, the GRIN can be specified as

$$n = F(x, r) \quad (2.3)$$

The function F involves both spatial variables. However, a less complex GRIN is used which is spherically symmetrical refractive index. In this case

$$n = n(x_c, r') \quad (2.4)$$

where r' is radial distance from the center of symmetry for the sphere. The location of the center of the spherical GRIN is on the lens axis at axial position x_c .

One very important computational advantage of spherical GRIN is that the rays within the lens are confined to a single plane. In the case of skew rays, the plane of the rays is not a meridional plane of the lens.

The equation for a ray trajectory in a spherically symmetric GRIN geometry is

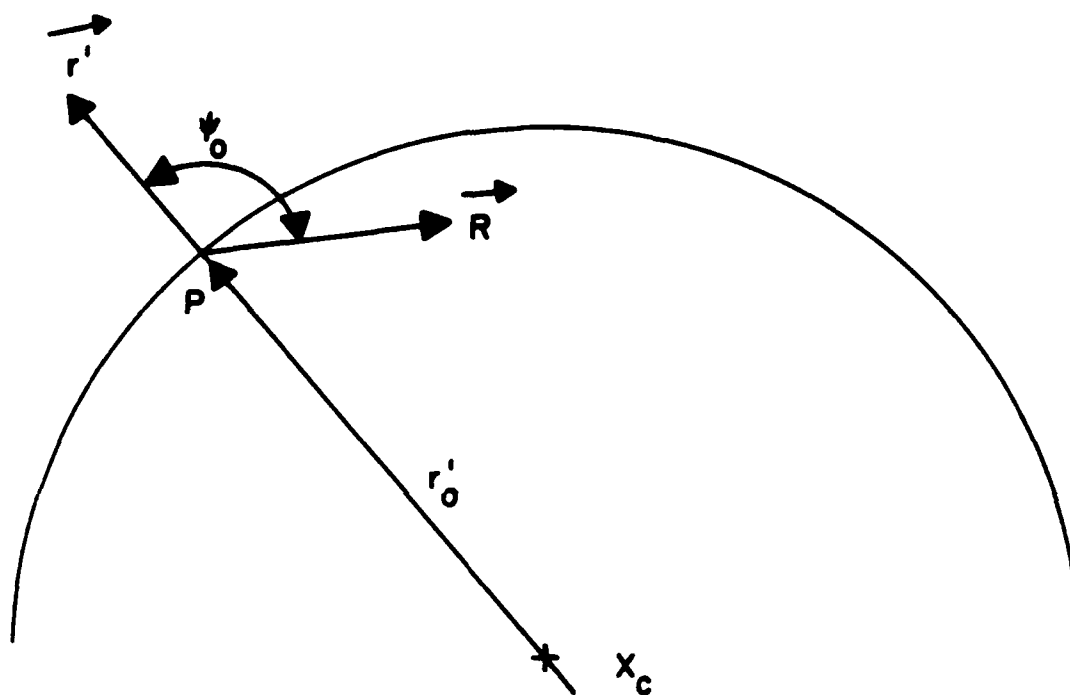
$$\theta_e = \theta_0 + E \int \frac{dr'}{r' \sqrt{r'^2 n^2(r') - E^2}} \quad (2.5)$$

where E is a constant for a ray. The value of E is obtained from

$$E = n_0(r'_0) r'_0 \sin \psi_0 \quad (2.6)$$

Define \vec{r}' as a unit vector in the direction of a line extending from x_c to point P in Figure 1. Define \vec{R} as a unit vector of a ray which has been refracted by the surface at point P . The angle ψ_0 is obtained from

$$\cos \psi_0 = \vec{r}'_0 \cdot \vec{R} \quad (2.7)$$



CENTER OF SYMMETRY OF GRIN

Figure 1. Geometry for Ray Tracing in a Spherically Symmetrical GRIN medium. The ray vector, \vec{R} , and the radius vector, \vec{r}' , are illustrated.

In equation (2.6), the ϵ is a sign function having a value of + 1.0 or - 1.0 depending on the value of ψ within the lens.

$$\epsilon = \begin{cases} + 1.0 & \psi \leq \pi/2 \\ - 1.0 & \psi > \pi/2 \end{cases} \quad (2.8)$$

Equation (2.5) can be integrated for certain functions $n(r')$. One function is

$$n(r') = \left[A + B(r'/r_0)^2 \right]^{1/2} \quad (2.9)$$

where A and B are constants. r_0 is a value associated with a specific lens design; a convenient value for r_0 is that value for the ray defining the lens aperture.

Combining equations (2.5) and (2.9) and completing the integration yields

$$\theta_e(r') = -\frac{1}{2} \left[\sin^{-1} \left\{ \frac{2E^2/r_r'^2 - A}{(A^2 + 4BE^2/r_0^2)^{1/2}} \right\} - \sin^{-1} \left\{ \frac{2E^2/r_f'^2 - A}{(A^2 + 4BE^2/r_0^2)^{1/2}} \right\} \right] \quad (2.10)$$

Equation (2.10) is an explicit relation for θ_e as a function of r' . r_r , r_f are the radii to the rear surface and to the front surface respectively. An explicit relation for r' as a function of θ_e can be derived; the result is

$$r'_{(r, f)}(\theta_e) = \frac{\sqrt{2} |E|}{\left(A + \sqrt{A^2 + 4BE^2/r_0^2} \cdot \sin \left\{ \mp 2\theta_e + \sin^{-1} \left[\frac{2E^2/r_{(r, f)} - A}{\sqrt{A^2 + 4BE^2/r_0^2}} \right] \right\} \right)^{1/2}} \quad (2.11)$$

For details look at section 4.1. For certain phases of the calculation equation (2.11) is needed.

Thinking ahead to numerical optimization, the function of equation (2.9) was chosen to avoid numerical integration of equation (2.5). Equation (2.5) must be evaluated several times for each ray. A lens design may involve 100 to 1000 rays. Numerical optimization of the lens requires calculation of many different lens shapes. Hence, evaluation of equation (2.5) may occur several thousand times in the process of lens optimization. The GRIN-related parameters to be determined in optimization are A, B and x_c .

3. EQUATIONS FOR THE HOMOGENEOUS CASE

3.1 Meridian Plane

The homogeneous case is included here for several reasons. First, the homogeneous case is a simple example in which the intricacies of lens design are apparent in considerable clarity. Iteration is not required for design of a lens with a homogeneous refractive index, whereas for GRIN, iteration is necessary. Second, the homogeneous case provides a meaningful check of the GRIN program. To conduct the check, the value of B is zero in equation (2.9). Obviously the answers from GRIN program with B equal to zero must agree with answers from the homogeneous case.

The book by Kingslake [16] has been helpful in the program development.

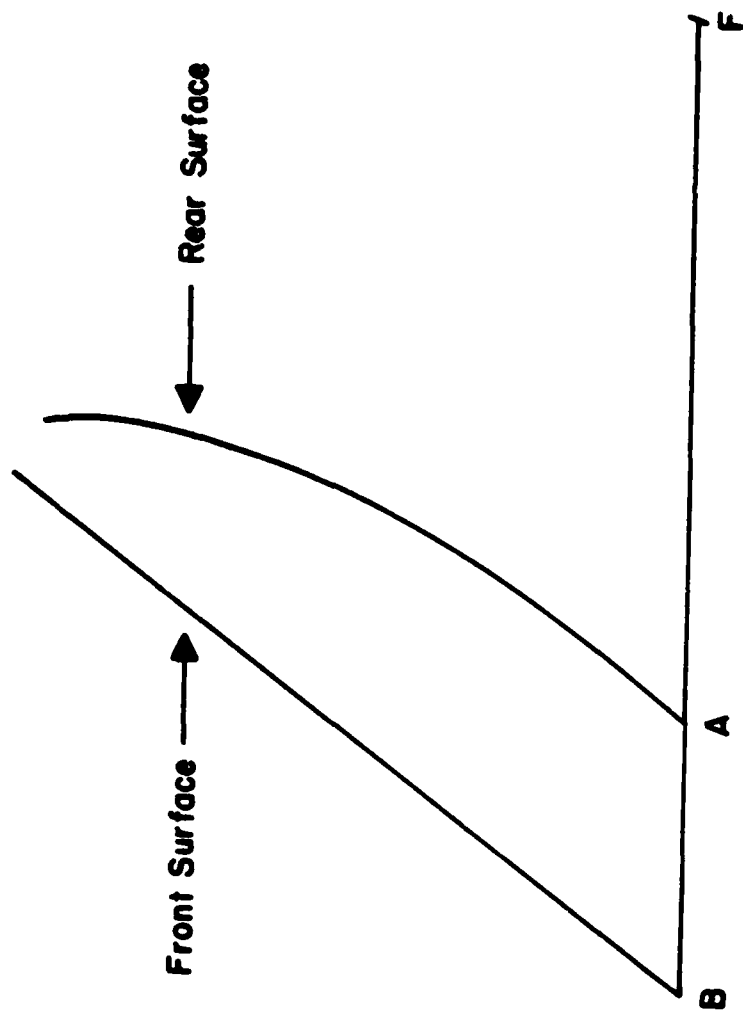


Figure 2. Diagram illustrating the shape of the front and rear surfaces of a GRIN lens. BAF is axis of symmetry. F is the focal point.

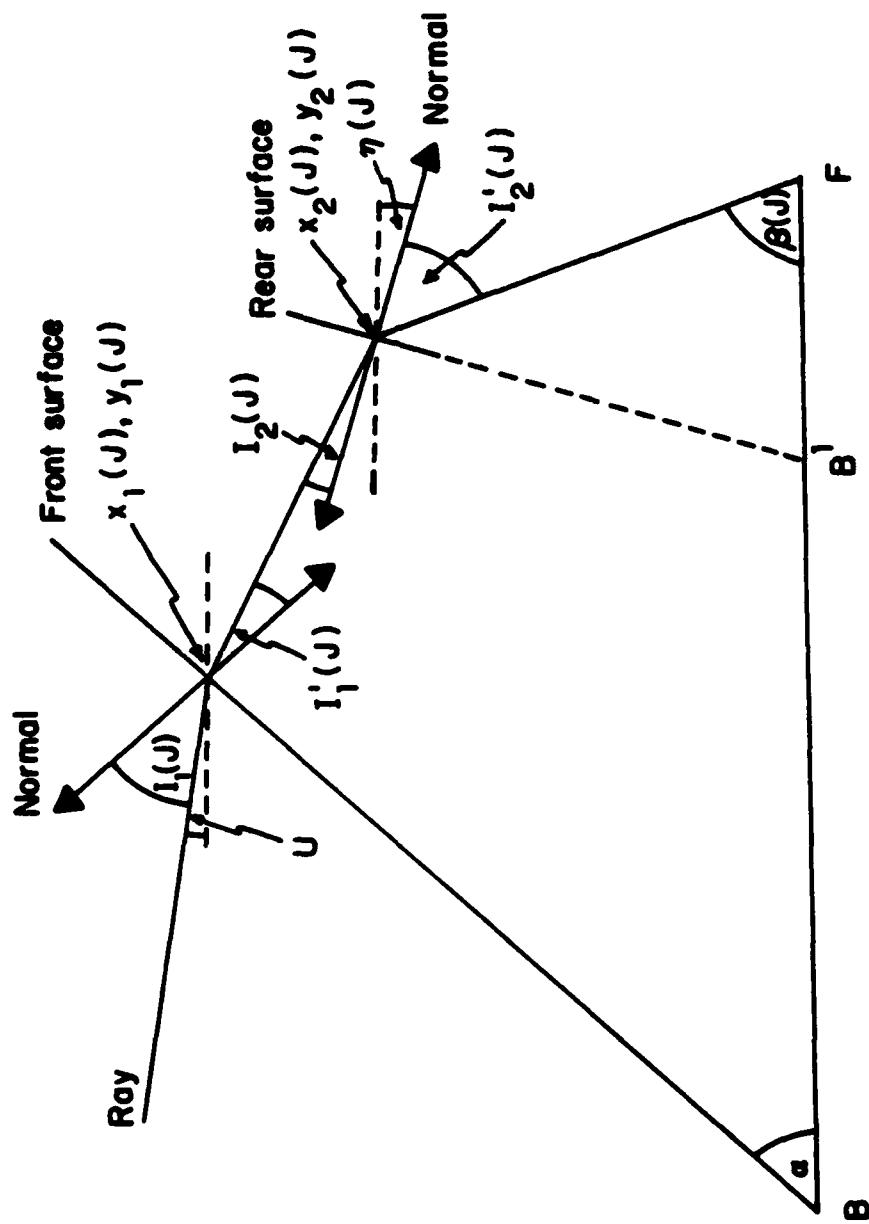


Figure 3. Geometry and angle definitions for the homogeneous refractive index case.

3.1.1 The Equations

Refer to Figure 3 for definition of the symbols.

$$\eta(J) + I_2'(J) = \beta(J) \quad (3.1)$$

$$\sin(I_2[J]) = n_{32} \cdot \sin(I_2'[J]) \quad (3.2)$$

The notation n_{32} is used for the ratio n_3/n_2 .

$$I_1'(J) = (\pi/2 - \alpha) - (\eta(J) + I_1(J)) \quad (3.3)$$

$$\sin(I_1[J]) = n_{21} \cdot \sin(I_1'[J]) \quad (3.4)$$

$$\alpha + I_1(J) + U = \pi/2 \quad (3.5)$$

3.1.2 Solution

The angles α , $\beta(J)$ are inputs and are known.

From eq. (3.5):

$$I_1(J) = \pi/2 - \alpha - U \quad (3.5.1)$$

From eq. (3.4):

$$I_1'(J) = \sin^{-1}[n_{12} \cdot \sin(I_1[J])] \quad (3.4.1)$$

Substitute eq. (3.5) to eq. (3.3):

$$\eta(J) + I_2(J) = I_1(J) - I_1'(J) + U \quad (3.3.1)$$

But from eq. (3.2):

$$I_2'(J) = \sin^{-1}[n_{32} \cdot \sin(I_2[J])] \quad (3.2.1)$$

From eq. (3.3.1):

$$I_2(J) = [I_1(J) - I_1'(J)] - \eta(J) - U \quad (3.3.2)$$

Substitute eq. (3.3.2) into eq. (3.2.1):

$$I_2'(J) = \sin^{-1}[n_{23} \cdot \sin\{I_1(J) - I_1'(J) - \eta(J) + U\}] \quad (3.2.2)$$

Substitute eq. (3.2.2) into eq. (3.1):

$$\eta(J) + \sin^{-1}[n_{23} \cdot \sin\{I_1(J) - I_1'(J) - \eta(J) + U\}] = \beta(J) \quad (3.1.1)$$

Equation (3.1.1) is solved for $n(J)$:

$$n_{23} \cdot \sin(I_1(J) - I_1'(J) - n(J) + U) = \sin[\beta(J) - n(J)] \quad (3.1.2)$$

Use the formula:

$$\sin(A \pm B) = \sin A \cos B \pm \cos A \sin B$$

And substitute:

$$x = \sin(n(J)) ; \sqrt{1 - x^2} = \cos(n(J))$$

Equation (3.1.2) will turn into the form:

$$x = \sqrt{\frac{1}{1 + A^2}} \quad (3.1.3)$$

Where:

$$A = \frac{n_{23} \cdot \cos[I_1(J) - I_1'(J) + U] - \cos[\beta(J)]}{n_{23} \cdot \sin[I_1(J) - I_1'(J) + U] - \sin[\beta(J)]} \quad (3.1.4)$$

Therefore:

$$n(J) = \sin^{-1}[x] \quad (3.1.5)$$

Knowing $n(J)$, $I_2'(J)$ can be solved from equation (3.1), and then, $I_2(J)$ can be solved from equation (3.2).

3.1.3 Coordinates of the Front and of the Rear Surfaces

3.1.3.1 The First Ray

All the magnitudes will be normalized with respect to the radius R . R is the aperture for the lens.

Therefore:

$$R = 1.0 \begin{cases} y_1(1) = R \\ x_1(1) = \frac{R}{\tan(\alpha)} \end{cases} \quad (3.6)$$

The thickness of the lens is defined:

$$T(1) = \sqrt{[x_2(1) - x_1(1)]^2 + [y_1(1) - y_2(1)]^2} \quad (3.7)$$

Therefore, the appropriate coordinates of the rear surface are:

$$\begin{cases} x_2(1) = x_1(1) + T(1) \cdot \cos[\pi/2 - \alpha - I_1'(1)] \\ y_2(1) = y_1(1) - T(1) \cdot \sin[\pi/2 - \alpha - I_1'(1)] \end{cases} \quad (3.8)$$

3.1.3.2 The Other Rays: Coordinates of the Rear Surface

The new point of the rear surface

$x_2(J), y_2(J)$ will be the intersection between the surface and the ray.

(a) The equation of the surface:

$$y_2(J) = m[x_2(J) - BB'] \quad (3.9)$$

$$m = \tan[\pi/2 - \eta(J - 1)] = \cot[\eta(J - 1)] \quad (3.9.1)$$

$$BB' = BF - B'F$$

$$B'F = y_2(J - 1) \cdot [\cot[\pi/2 - \eta(J - 1)] + \cot[\beta(J - 1)]]$$

$$\therefore B'F = y_2(J - 1) \cdot \{\tan[\eta(J - 1)] + \cot[\beta(J - 1)]\} \quad (3.9.2)$$

$$\therefore y_2(J) = \cot[\eta(J - 1)]\{x_2(J) - [BF - B'F]\} \quad (3.9.3)$$

(b) The equation of the ray:

$$y_2(J) = -\tan[\beta(J)]x_2(J) + BF \cdot \tan[\beta(J)] \quad (3.10)$$

$$\therefore y_2(J) = \tan[\beta(J)] \cdot \{-x_2(J) + BF\} \quad (3.10.1)$$

From equations (3.9.3) and (3.10.1), the coordinates of the next point at the rear surface are found; those are:

$$\begin{cases} x_2(J) = \frac{BF\{\tan[\beta(J)] + \cot[\eta(J - 1)]\} - \cot[\eta(J - 1)] \cdot B'F}{\cot[\eta(J - 1)] + \tan[\beta(J)]} \\ y_2(J) = \tan[\beta(J)]\{-x_2(J) + BF\} \end{cases} \quad (3.11)$$

3.1.3.3 Coordinates of the Front Surface

(a) Equation of the rear surface:

$$y_1(J) = (\tan \alpha) \cdot x_1(J) \quad (3.12)$$

(b) Equation of the ray:

$$y_1(J) = m[x_1(J) - x_2(J)] + y_2(J) \quad (3.13)$$

where: $m = -\tan[\pi/2 - \alpha - I_1'(J)] \quad (3.13.1)$

or: $m = -\cot[\alpha + I_1'(J)] \quad (3.13.2)$

From equations (3.12) and (3.13) the intercept point is calculated:

$$x_1(J) = \frac{y_2(J) + x_2(J) \cdot \cot[\alpha + I_1'(J)]}{\tan \alpha + \cot[\alpha + I_1'(J)]} \quad (3.14)$$

$$y_1(J) = (\tan \alpha) \cdot x_1(J)$$

3.1.3.4 The Thickness at the New Point

$$T(J) = \sqrt{[x_2(J) - x_1(J)]^2 + [y_1(J) - y_2(J)]^2} \quad (3.15)$$

3.2 Skew Rays in the Homogeneous Case

3.2.1 Coordinate Transformation

The x,y coordinates will be shifted by the angle α_p .

$$x' = x \cdot \cos(\alpha_p) - y \cdot \sin(\alpha_p) \quad (3.16.1)$$

$$y' = x \cdot \sin(\alpha_p) + y \cdot \cos(\alpha_p) \quad (3.16.2)$$

$$z' = z \quad (3.16.3)$$

3.2.2 Calculate the Intercept Point of the Front Surface

Assuming that the (0,0) point is at point A

(Refer to figure 2.), the following equations can be derived:

$$(a) \text{ Ray: } R_{\text{ray}}^2 = y^2 + z^2 \quad (3.17.1)$$

$$\bullet R_{\text{ray}} = \left[\frac{y_0'}{\cos(\alpha_p)} - (x + AB) \cdot \tan(\alpha_p) \right]^2 + z_0'^2 \quad (3.17.2)$$

Where R_{ray} is the radius of the ray and the values for y_0' , z_0' are known.

$$(b) \text{ Cone: } R_{\text{cone}} = \tan(\alpha) \cdot [x + AB] \quad (3.18)$$

Solving equations (3.17.2), (3.18) for x results:

$$\left\{ \begin{array}{l} XO = - \frac{CDS}{A_2 D_2} + \frac{\sqrt{CDS^2 + A_2 D_2 \cdot CZD}}{A_2 D_2} \end{array} \right. \quad (3.19.1)$$

$$\left\{ \begin{array}{l} YO = \frac{y_0'}{\cos(\alpha_p)} - XO \cdot \tan(\alpha_p) \end{array} \right. \quad (3.19.2)$$

$$\left\{ \begin{array}{l} ZO = z_0' \end{array} \right. \quad (3.19.3)$$

Where:

$$A_2 D_2 = (\tan \alpha)^2 - (\tan \alpha_p)^2 \quad (3.20.1)$$

$$CDS = \frac{y_0'}{\cos \alpha_p} \tan \alpha_p + (AB) [A_2 D_2] \quad (3.20.2)$$

$$CZD = \left(\frac{y_0'}{\cos \alpha_p} \right)^2 + z_0'^2 - (AB)^2 [A_2 D_2]^2 - 2(AB) \frac{y_0'}{\cos \alpha_p} \tan \alpha_p \quad (3.20.3)$$

3.2.3 Direction Cosines of the Normal

$$f = y^2 + z^2 - (\tan \alpha)^2 (x + AB)^2 = 0 \quad (3.21)$$

$$\frac{\delta f}{\delta x} = -2(\tan \alpha)^2 (x + AB) \quad (3.21.1)$$

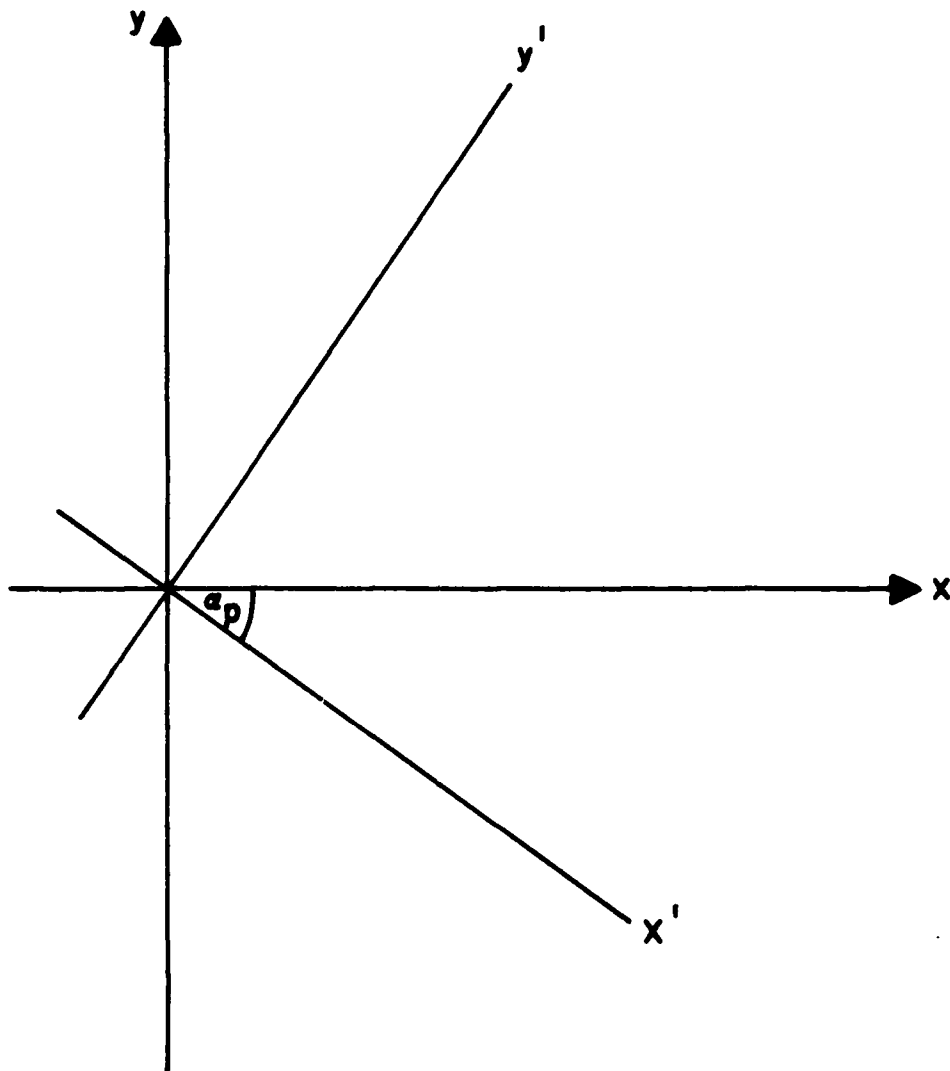


Figure 4. Diagram showing coordinate transformation for off-axis rays.

$$\frac{\delta f}{\delta y} = 2y ; \frac{\delta f}{\delta z} = 2z \quad (3.21.2)$$

$$|\vec{\Delta f}| = 2[(\tan \alpha)^4 (x + AB)^2 + y^2 + z^2]^{\frac{1}{2}} \quad (3.21.4)$$

Substituting equation (3.21) can turn equation (3.21.4) into the form:

$$|\vec{\Delta f}| = \frac{2 \tan \alpha}{\cos \alpha} (x + AB) \quad (3.21.5)$$

The direction cosines of the normal are therefore:

$$n_x = \frac{(\delta f / \delta x)}{|\vec{\Delta f}|} = -\sin \alpha \quad (3.22)$$

$$n_y = \frac{(\delta f / \delta y)}{|\vec{\Delta f}|} = \frac{2y}{2 \tan \alpha / \cos \alpha (x + AB)} \quad (3.23)$$

$$\text{Define: } \sigma = \tan^{-1}(z/y) \quad (3.23.1)$$

$$y^2 + z^2 = (\tan \alpha)^2 (x + AB)^2$$

$$y^2 (1 + \tan^2 \sigma) = \tan^2 \alpha (x + AB)^2$$

$$y = (\cos \sigma) (\tan \alpha) (x + AB) \quad (3.23.2)$$

Therefore:

$$n_y = (\cos \sigma) (\cos \alpha) \quad (3.23.3)$$

Similiarly:

$$n_z = \frac{(\delta f / \delta z)}{|\vec{\Delta f}|} = (\sin \sigma) (\cos \alpha) \quad (3.24)$$

3.2.4 Refraction at the Front Surface

The skew ray \vec{R} will be defined:

$$\vec{R} = R_x \cdot (\hat{e}_x) + R_y \cdot (\hat{e}_y) + R_z \cdot (\hat{e}_z) \quad (3.25)$$

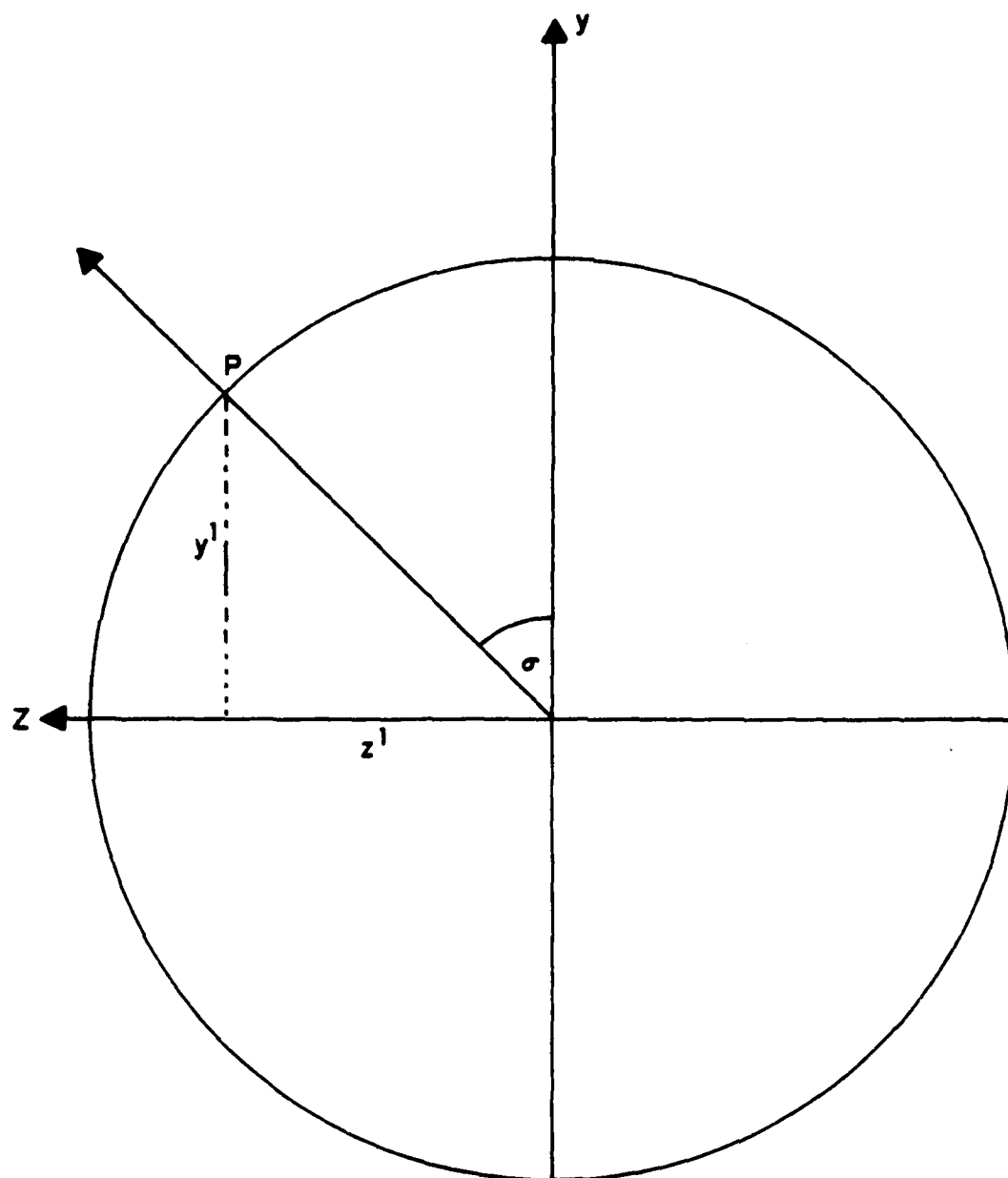


Figure 5. Cross section of lens in a plane normal to the lens axis. Point P is the point where an off-axis ray intersects the front surface of the lens.

Where R_X , R_Y , R_Z are the direction cosines of the ray,
and they have the value:

$$R_X = \cos \alpha_p ; R_Y = -\sin \alpha_p ; R_Z = 0 \quad (3.26)$$

The surface normal is defined by the following expression:

$$\vec{N} = n_X \cdot (\hat{e}_X) + n_Y \cdot (\hat{e}_Y) + n_Z (\hat{e}_Z) \quad (3.27)$$

Where the direction cosines of the normal surface were
defined previously (equations 3.22, 3.23.3, 3.24).

The refracted angle at the front surface is defined:

$$\theta = \cos^{-1} \left\{ \frac{\vec{R} \cdot \vec{N}}{|\vec{R}| \cdot |\vec{N}|} \right\} \quad (3.28)$$

$$\text{Where: } \left. \begin{aligned} |\vec{R}| &= \sqrt{R_X^2 + R_Y^2 + R_Z^2} = 1 \\ |\vec{N}| &= \sqrt{n_X^2 + n_Y^2 + n_Z^2} = 1 \end{aligned} \right\} \quad (3.29)$$

Therefore:

$$\theta = \cos^{-1} \{ R_X \cdot n_X + R_Y \cdot n_Y + R_Z \cdot n_Z \} \quad (3.30)$$

$$\left. \begin{aligned} \phi &= \pi - \theta \\ \phi' &= \sin^{-1} [n_{12} \cdot \sin \phi] \end{aligned} \right\} \quad (3.31)$$

3.2.5 Refraction Equations

Referring to figure 6 the refraction at the
rear surface with regard to the front surface will be as
follows [16, p. 147]:

$$n_2 \vec{R}' = n_1 \vec{R} + [n_2 \cos(\phi') - n_1 \cos(\phi)] \vec{N}$$

The direction cosines of the normal surface were defined in

equations (3.22), (3.23.3), (3.24) and the direction cosines of the ray at the front surface were defined in equation (3.26). The direction cosines of the skew ray at the rear surface, will therefore be:

$$\left. \begin{aligned} K' &= n_{12} R_Z + [\cos(\phi') - n_{12} \cos(\phi)] \cdot n_X \\ L' &= n_{12} R_Y + [\cos(\phi') - n_{12} \cos(\phi)] \cdot n_Y \\ M' &= n_{12} R_Z + [\cos(\phi') - n_{12} \cos(\phi)] \cdot n_Z \end{aligned} \right\} \quad (3.32)$$

3.2.6 Intercept at the Rear Surface

The equation of the cone of the rear surface is:

$$y^2 + z^2 = [ax - b]^2 \quad (3.33)$$

where a is the slope and is defined from figure 7.

$$a = \tan(\xi_J) = \frac{R_J}{X_J - X_V} = \frac{R_J + 1 - R_J}{X_J + 1 - X_J} \quad (3.33.1)$$

b is the intercept at the X - axis and is calculated from equation (3.33.1):

$$b = X_V = \frac{R_J + 1 \cdot X_J - R_J \cdot X_J + 1}{R_J + 1 - R_J} \quad (3.33.2)$$

(XI, YI, ZI) is the point of intercept at the rear surface.

The equation of the rear surface is therefore:

$$YI^2 + ZI^2 - (aXI - b) = 0 \quad (3.33.3)$$

where a,b were defined in equations (3.33.1), (3.33.2).

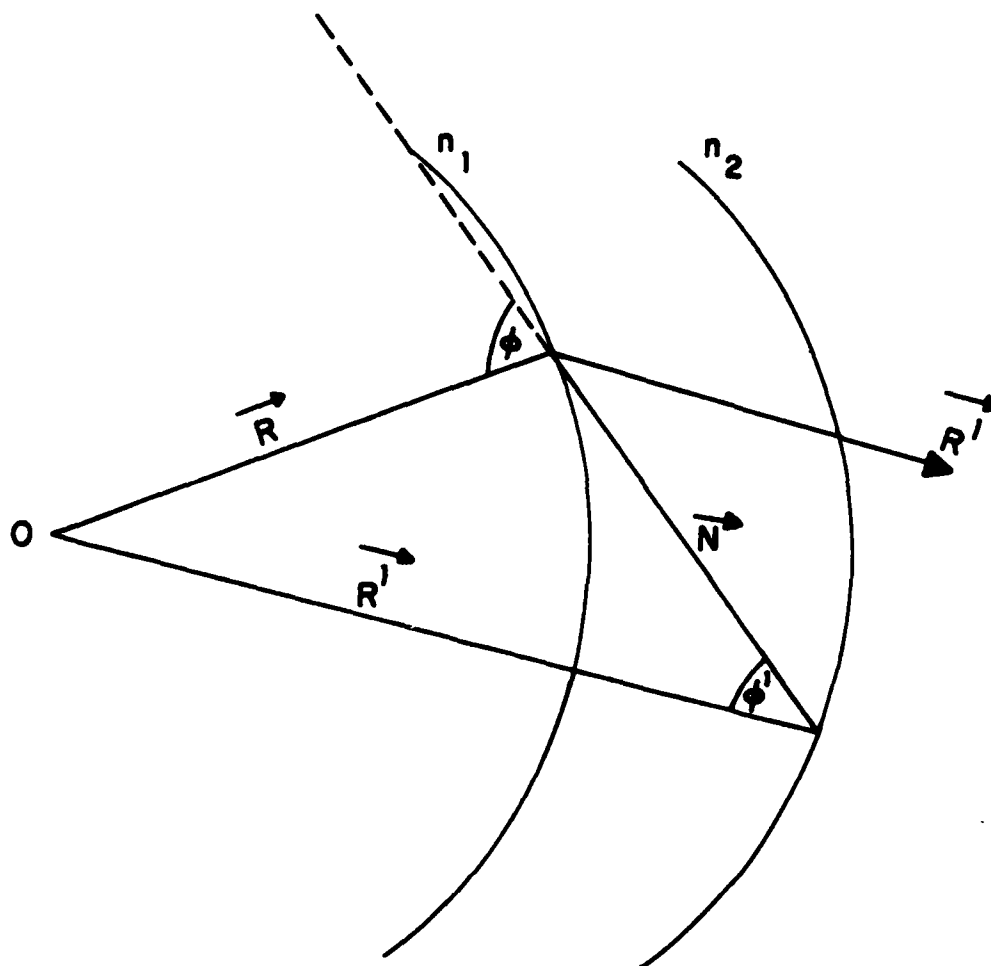


Figure 6. Diagram used to calculate the direction cosines of skew rays at the rear surface. This diagram is based on Kingslake [16].

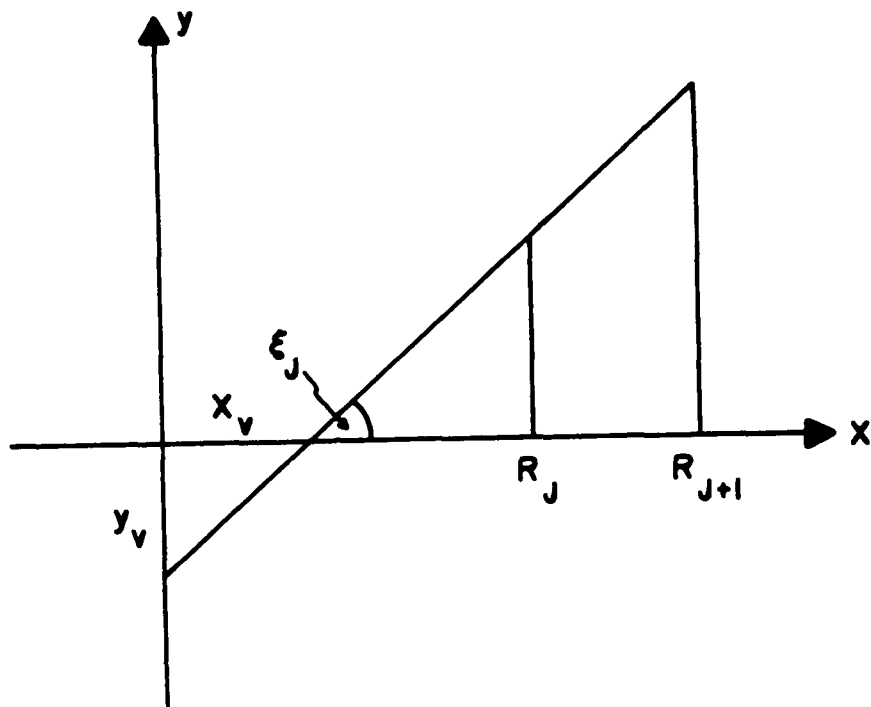


Figure 7. Geometry of a truncated cone which represents a small portion of the rear surface of the lens. The cone angle is ξ_J .

The direction cosines of the ray at the rear surface were defined previously (3.32). They are:

$$K' = \frac{XI - XO}{D} ; L' = \frac{YI - YO}{D} ; M' = \frac{ZI - ZO}{D} \quad (3.34)$$

(XO, YO, ZO) is the point of intercept at the front surface (3.19.1, 3.19.2, 3.19.3).

$$D = \sqrt{(XI - XO)^2 + (YI - YO)^2 + (ZI - ZO)^2} \quad (3.35)$$

Solving for D from equations (3.33.3) and (3.34) one gets:

$$D = -\frac{b'}{a'} + \frac{\sqrt{b'^2 - a'c'}}{a'} \quad (3.36)$$

Where:

$$a' = (L')^2 + (M')^2 - a^2(K')^2 \quad (3.36.1)$$

$$b' = (L')YO + (M')ZO - (K')a^2(XO - b/a) \quad (3.36.2)$$

$$c' = YO^2 + ZO^2 - a^2XO(XO - 2b/a) - b^2 \quad (3.36.3)$$

Knowing D, the intercept point at the rear surface can be verified using equation (3.34):

$$\left\{ \begin{array}{l} XI = K'D + XO \end{array} \right. \quad (3.37.1)$$

$$\left\{ \begin{array}{l} YI = L'D + YO \end{array} \right. \quad (3.37.2)$$

$$\left\{ \begin{array}{l} ZI = M'D + ZO \end{array} \right. \quad (3.37.3)$$

3.2.7 Equation of the Normal to the Rear Surface

The equation of the cone of the rear surface was defined previously (eq. 3.33):

$$f(x,y,z,) = -(ax - b)^2 + y^2 + z^2 = 0 \quad (3.33)$$

a,b are defined in equations (3.33.1), (3.33.2).

$$\vec{\nabla}f = \hat{e}_x \frac{\delta f}{\delta x} + \hat{e}_y \frac{\delta f}{\delta y} + \hat{e}_z \frac{\delta f}{\delta z} \quad (3.38.1)$$

Similar to what was done at the front surface:

$$\frac{\delta f}{\delta x} = -2a(ax - b) \quad (3.38.2)$$

$$\frac{\delta f}{\delta y} = 2y \quad ; \quad \frac{\delta f}{\delta z} = 2z \quad (3.38.3)$$

$$\begin{aligned} |\vec{\nabla}f| &= \left[\left(\frac{\delta f}{\delta x} \right)^2 + \left(\frac{\delta f}{\delta y} \right)^2 + \left(\frac{\delta f}{\delta z} \right)^2 \right]^{1/2} \\ &= 2[a^2(ax - b)^2 + y^2 + z^2]^{1/2} \\ &= 2(ax - b)[(1 + a^2)^{1/2}] \end{aligned} \quad (3.38.4)$$

The direction cosines of the normal to the surface are as follows:

$$n_x = \frac{(\delta f / \delta x)}{|\vec{\nabla}f|} = \frac{-a}{(1 + a^2)^{1/2}} \quad (3.39.1)$$

$$n_y = \frac{y}{(y^2 + z^2)^{1/2}(1 + a^2)^{1/2}} \quad (3.39.2)$$

$$n_z = \frac{z}{(y^2 + z^2)^{1/2}(1 + a^2)^{1/2}} \quad (3.39.3)$$

3.2.8 Refraction at the Rear Surface

Similar to what was done at the front surface:

$$\vec{R}' = K'(\hat{e}_x) + L'(\hat{e}_y) + M'(\hat{e}_z) \quad (3.40.1)$$

$$\vec{N} = n_x(\hat{e}_x) + n_y(\hat{e}_y) + n_z(\hat{e}_z) \quad (3.40.2)$$

Where the direction cosines of the refracted ray (\vec{R}') and the normal (\vec{N}) were defined previously (equations 3.32, 3.39).

The refracted angle at the rear surface:

$$\phi_I = \cos^{-1} \frac{\vec{R}' \cdot \vec{N}'}{|\vec{R}'| \cdot |\vec{N}'|} \quad (3.41)$$

Both the ray and the normal are normalized; therefore:

$$\phi_I = K'n_X + L'n_Y + M'n_Z \quad (3.41.1)$$

$$\phi_I' = \sin^{-1}[n_{23} \cdot \sin\phi_I] \quad (3.41.2)$$

3.2.9 Direction Cosines of Rear External Refracted

Ray

As done previously (equation 3.32):

$$\left. \begin{aligned} K'' &= n_{23}K' - [\cos(\phi_I') - n_{23}\cos(\phi_I)] \cdot n_X \\ L'' &= n_{23}L' - [\cos(\phi_I') - n_{23}\cos(\phi_I)] \cdot n_Y \\ Z'' &= n_{23}Z' - [\cos(\phi_I') - n_{23}\cos(\phi_I)] \cdot n_Z \end{aligned} \right\} \quad (3.42)$$

3.2.10 Intersection with the Image Plane

$$\left. \begin{aligned} X_{Im} &= BF = D_3K'' + XI \\ Y_{Im} &= D_3L'' + YI \\ Z_{Im} &= D_3M'' + ZI \end{aligned} \right\} \quad (3.43)$$

Solving equation (3.43), the intercept with the image plane can be calculated:

$$\left. \begin{aligned} D_3 &= (BF - XI)/K'' \\ Y_{Im} &= \left(\frac{BF - XI}{K''} \right) L'' + YI \\ Z_{Im} &= \left(\frac{BF - XI}{K''} \right) M'' + ZI \end{aligned} \right\} \quad (3.43.1)$$

4. FORMULATION OF EQUATIONS FOR GRIN LENS DESIGN

4.1 Solving the Integral for θ_e

As mentioned in section 2:

$$\theta_e = \theta_0 + E \int_{r_f}^{r_r} \frac{dr}{r \{ r^2 n(r)^2 - E^2 \}^{1/2}} \quad (4.1)$$

r_f , r_r are the radii to the front surface and to the rear surface, respectively.

$$E = \epsilon \cdot n_2(r_f) \cdot r_f \cdot \sin \psi_f \quad (4.2)$$

$$n = \sqrt{A + B \left(\frac{r}{r_0} \right)^2} \quad (4.3)$$

Substituting:

$$v = \left(\frac{r_0}{r} \right)^2 ; \quad \frac{dv}{dr} = -2r_0^2 r^{-3} \quad (4.1.1)$$

Equation (4.1) turns into the form:

$$\theta_e = \theta_0 - \frac{E}{2r_0} \int_{v_f}^v \frac{dv}{\left\{ AV + b - v^2 \frac{E^2}{r_0^2} \right\}^{1/2}} \quad (4.1.2)$$

Therefore:

$$\theta_e = -\frac{1}{2} \left[\sin^{-1} \left\{ \frac{2(E/r_0)^2 v - A}{(A^2 + 4BE^2/r_0^2)^{1/2}} \right\} \right]_{(r_0/r_f)^2}^{(r_0/r_r)^2}$$

or:

$$\theta_e = -\frac{1}{2} \left[\sin^{-1} \left\{ \frac{2E^2/r_r^2 - A}{(A^2 + 4BE^2/r_0^2)^{1/2}} \right\} - \sin^{-1} \left\{ \frac{2E^2/r_f^2 - A}{(A^2 + 4BE^2/r_0^2)^{1/2}} \right\} \right] \quad (4.1.3)$$

The appropriate expression for the radius will therefore be:

$$r_{(r,f)} = \frac{\sqrt{2}|E|}{\sqrt{A + \sqrt{A^2 + 4BE^2/r_0^2}} \cdot \sin \left\{ \mp 2\theta_e + \sin^{-1} \frac{2E^2/r_{(f,r)} - A}{\sqrt{A^2 + 4BE^2/r_0^2}} \right\}} \quad (4.4)$$

If the radius to the rear surface (r_r) is calculated from a known radius to the front surface (r_f) the minus sign is used in front of the angle θ_e . This situation occurs with skew ray calculation. The plus sign is used when r_f is calculated from a known r_r . This situation occurs for lens design.

4.2 Meridian Plane

4.2.1 Solution for the First Ray

(a) Define Point $X_1(1), Y_1(1)$

As in the homogeneous case:

$$\left. \begin{aligned} R &= 1.0 \\ Y_1(1) &= R \\ X_1(1) &= \frac{R}{\tan \alpha} \end{aligned} \right\} \quad (4.5)$$

(b) Define Angle to the Front Radius

$$\tan(\theta_0 + \theta_e) = \frac{R}{X_1(1) - X_C} \quad (4.6)$$

$$r_f(1) = r_0 = \frac{R}{\sin(\theta_0(1) + \theta_e(1))} \quad (4.7)$$

Referring to figure 8, θ_0 is the angle to the rear radius, θ_e

is the angle between the rear and the front radii, and X_C is the location of the center of symmetry.

(c) Choose θ_e from Initial Thickness

$$\left. \begin{aligned} \theta_e(1) &= T(1)/r_f(1) \\ \theta_0(1) &= (\theta_0(1) + \theta_e(1)) - \theta_e(1) \end{aligned} \right\} \quad (4.8)$$

(d) Solve for ψ_f

$$\left. \begin{aligned} \alpha + I_1(1) + u &= \pi/2 \\ I_1(1) &= \pi/2 - \alpha - u \end{aligned} \right\} \quad (4.9)$$

Knowing $r_f(1)$, the initial index of refraction ($n_2(r_f)$) can be calculated from eq. (4.3). Therefore:

$$\begin{aligned} \sin(I_1(1)) &= n_2(r_f)/n_3 \cdot \sin(I_1'(1)) \\ I_1'(1) &= \sin^{-1}[n_3/n_2(r_f) \cdot \sin[I_1(1)]] \end{aligned} \quad (4.10)$$

Referring to figure 8, ψ_f can be calculated.

$$\begin{aligned} \theta_e(1) + \theta_0(1) &= \alpha + \delta \\ \delta &= \theta_e(1) + \theta_0(1) - \alpha \end{aligned} \quad (4.11)$$

$$\begin{aligned} \delta + \psi_f(1) - I_1'(1) &= \pi/2 \\ \psi_f(1) &= \pi/2 + I_1'(1) - \delta \end{aligned} \quad (4.12)$$

(e) Solve for E

$$E = \epsilon \cdot n_r(r_f) \cdot r_f \cdot \sin\psi_f \quad (4.2)$$

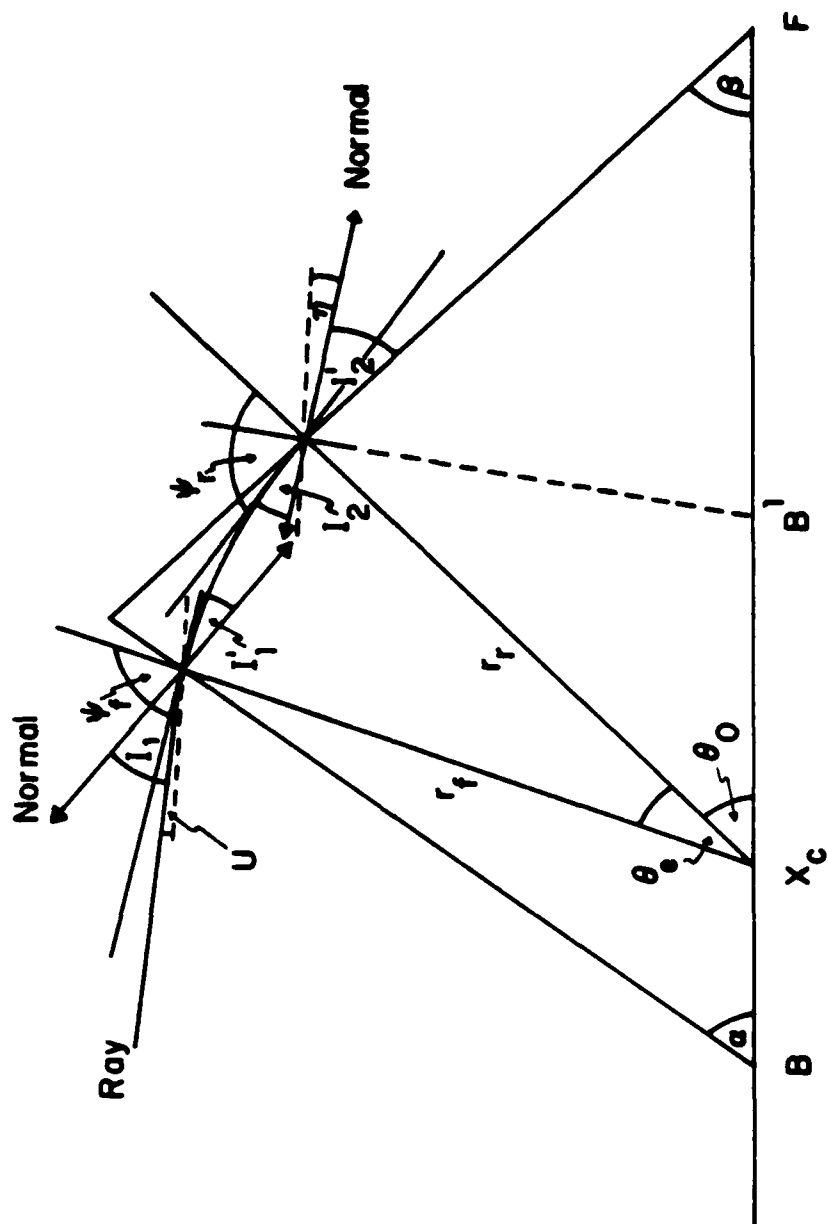


Figure 8. Diagram defining angles and coordinates for a ray transmitted by the GRIN lens. For the case illustrated B is negative.

Where:
$$\epsilon = \pm 1 \begin{cases} \psi \leq \pi/2 \rightarrow \epsilon = +1 \\ \psi > \pi/2 \rightarrow \epsilon = -1 \end{cases} \quad (4.2.1)$$

(f) Solve for r_f, ψ_r

Knowing the radius to the front surface (r_f) and the angle between the two radii (θ_e), the radius to the rear surface (r_r) can be calculated using equation (4.4). Using equation (4.2), ψ_r can be calculated:

$$\psi_r = \sin^{-1} \left[\frac{E}{\epsilon \cdot n_2(r_r) \cdot r_r} \right] \quad (4.2.2)$$

(g) Solve for $\beta(1)$

The focal length, which is an input, is known:

$$BF = F/R$$

The coordinates at the rear surface are:

$$\left. \begin{aligned} Y_2(1) &= r_r \sin(\theta_0(1)) \\ X_2(1) &= X_C + r_r \cos(\theta_0(1)) \end{aligned} \right\} \quad (4.13)$$

Using equation (4.13), $\beta(1)$ can be calculated:

$$\beta(1) = \tan^{-1} \left[\frac{Y_2(1)}{BF - X_2(1)} \right] \quad (4.14)$$

(h) Solve for the Refractive Angles at the Front Surface

As in the homogeneous case:

$$n(J) + I_2'(J) = \beta(J) \quad (4.15)$$

$$\sin[I_2(J)] = n_3/n_2(r_r) \cdot \sin[I_2'(J)] \quad (4.16)$$

$$\psi_r(J) + I_2(J) + n(J) + \theta_0(J) = \pi \quad (4.17)$$

Solve for $n(J)$ in a manner similar to the homogeneous case:

$$n(J) = \sin^{-1} \left[\sqrt{\frac{1}{1 + A^2}} \right] \quad (4.18)$$

Where:

$$A = \frac{\cos \delta' - n_3/n_2(r_r) \cdot \cos \beta(J)}{\sin \delta' - n_3/n_2(r_r) \cdot \sin \beta(J)} \quad (4.18.1)$$

Where:

$$\delta' = \pi - \theta_0(J) - \psi_0(J) \quad (4.18.2)$$

Knowing $n(J)$, $I_2'(J)$ can be solved from eq. (4.15) and then, $I_2(J)$ can be solved from equation (4.16).

4.2.2 Solution for Next Rays

4.2.2.1 Coordinates at the Rear Surface

Solve for the subsequent rays the same way as in the homogeneous case (equations 3.10, 3.10.1).

4.2.2.2 Calculate Radius and Angle to the Rear Surface

$$r_r(J) = \sqrt{(x_2(J) - x_C)^2 + y_2(J)^2} \quad (4.19)$$

$$\theta_0(J) = \tan^{-1}[y_2(J)/(x_2(J) - x_C)] \quad (4.20)$$

4.2.2.3 Solve Front Surface Parameters

Refer to Figure 8 for a definition of geometrical variables.

(a) Equations

$$\eta(J) + I_2'(J) = \beta(J) \quad (4.15)$$

$$\sin[I_2(J)] = n_3/n_2(r_r) \cdot \sin[I_2'(J)] \quad (4.16)$$

$$\psi_r(J) + I_2(J) + \eta(J) + \theta_0(J) = \pi \quad (4.17)$$

$$E = \epsilon \cdot n_2(r_r) \cdot r_r \cdot \sin[\psi_r(J)] \quad (4.2.2)$$

$$E = \epsilon \cdot n_2(r_f) \cdot r_f \cdot \sin[\psi_f(J)] \quad (4.2)$$

$$\theta_e(J) + \theta_0(J) = \alpha + \delta \quad (4.21)$$

$$\delta + \psi_f(J) - I_1'(J) = \pi/2 \quad (4.22)$$

$$r_f = f(r_r, \theta_e(J)) \quad (4.4)$$

$$\sin[I_1(J)] = n_2(r_f)/n_1 \cdot \sin[I_1'(J)] \quad (4.23)$$

$$\alpha + I_1(J) + u = \pi/2 \quad (4.24)$$

(b) Solution by Iteration

An explicit solution is not possible. An iterative solution is necessary.

(b1) Assume $\theta_e(J)$.

(b2) Solve for coordinates

of the front surface:

- Calculate $I_1(J)$ from eq. (4.24)
- Calculate δ from eq. (4.21)
- Calculate front surface coordinates and radius:

$$Y_1(J) = \tan(\theta_0(J) + \theta_e(J)) \cdot (X_1(J) - X_C) \quad (4.25)$$

$$Y_1(J) = \tan \alpha \cdot X_1(J) \quad (4.26)$$

The result is:

$$\begin{cases} X_1(J) = \frac{X_C \cdot \tan[\theta_0(J) + \theta_e(J)]}{\tan[\theta_0(J) + \theta_e(J)] - \tan \alpha} \\ Y_1(J) = \tan \alpha \cdot X_1(J) \end{cases} \quad (4.27)$$

$$r_f = Y_1(J) / \sin[\theta_0(J) + \theta_e(J)] \quad (4.28)$$

$$= \frac{X_C \cdot \tan \alpha}{\sin[\theta_0(J) + \theta_e(J)] - \tan \alpha \cdot \cos[\theta_0(J) + \theta_e(J)]} \quad (4.28.1)$$

(b3) Knowing r_f , $I_1'(J)$ can be solved using equation (4.23).

- Calculate ψ_f from eq. (4.22)
- Calculate E from eq. (4.2)

(b4) Calculate second expression for front radius (r_f) from eq. (4.4).

(b5) The iteration routine:

The iteration search for correct θ_e uses the Newton-Raphson routine.
The function:

$$F = r_{ff} - r_f = 0 \quad (4.29)$$

r_{ff} is the expression from the formula (eq. 4.4) where r_f is the geometric expression (eq. 2.28).

The derivative is found with respect to θ_e :

$$F' = \frac{d(r_{ff})}{d(\theta_e)} - \frac{d(r_f)}{d(\theta_e)} \quad (4.30)$$

$$\frac{d(r_{ff})}{d(\theta_e)} = \pm \frac{(r_{ff})^3}{2E^2} \cdot B_1 \cdot \cos[\mp 2\theta_e + \sin^{-1}(B_2)] \quad (4.30.1)$$

Where:

$$B_1 = \sqrt{A^2 + 4B(E/r_r)^2} \quad (4.30.2)$$

$$B_2 = [2(E/r_r)^2 - A]/B_1 \quad (4.30.3)$$

The lower signs are used when the front radius (r_f) is calculated from a known rear radius (r_r) (this case occurs at $J > 1$), while the upper signs are used when r_r is calculated from r_f (for $J=1$).

$$\frac{d(r_f)}{d(\theta_e)} = \frac{-X_C \cdot \tan \alpha \cdot \{\cos[\theta_0(J) + \theta_e(J)] + \tan \alpha \cdot \sin[\theta_0(J) + \theta_e(J)]\}}{\{\sin[\theta_0(J) + \theta_e(J)] - \tan \alpha \cdot \cos[\theta_0(J) + \theta_e(J)]\}^2} \quad (4.30.4)$$

(c) Correct Solution

After knowing the correct value for $\theta_e(J)$, the procedure used in (b) can be followed resulting in the correct values for:

$I_1(J)$, δ , $X_1(J)$, $Y_1(J)$, $r_f(J)$, $I_1'(J)$, $\psi_f(J)$, E . Using equation (4.2.2) ψ_r can be calculated. Equations (4.15), (4.16), (4.17) can be solved for $n(J)$, $I_2'(J)$, $\beta(J)$ as shown previously for the $J=1$ case (equations 4.18, 4.15, 4.16).

4.3 Skew Rays

4.3.1 Front Surface

As in the homogeneous case, the intercept point at the front surface (X_0, Y_0, Z_0) can be found (equations 3.19.1, 3.19.2, 3.19.3).

Also, the direction cosines of the normal to the front surface can be calculated (equations 3.22, 3.23). The direction cosines of the ray can be found as well using equation (3.26).

4.3.2 Front Radius

Knowing the intercept point at the front surface, the front radius can be calculated:

$$r_f(J) = [(X_0 - X_C)^2 + (Y_0)^2 + (Z_0)^2]^{1/2} \quad (4.31)$$

Knowing $r_f(J)$, the initial index of refraction $[n_2(r_f)]$ can be calculated using equation (4.3).

4.3.3 Refraction at the Front Surface

As for the homogeneous case (section 3.2.4), the refracted angle at the front surface can be calculated using equations (3.30), (3.31).

4.3.4 Initial Direction Cosines for the Internal Refracted Ray

The initial direction cosines of the internal refracted ray (K', L', M') are calculated the same way as for the homogeneous case (section 3.2.5, equation 3.32). The vector form of the initial direction of the ray is therefore:

$$\vec{R} = K' \cdot \hat{e}_X + L' \cdot \hat{e}_Y + M' \cdot \hat{e}_Z \quad (4.32)$$

4.3.5 Front Radius Direction Cosines

The vector form of the front radius is defined as follows:

$$\vec{r}_f = r_{fX} \cdot \hat{e}_X + r_{fY} \cdot \hat{e}_Y + r_{fZ} \cdot \hat{e}_Z \quad (4.33)$$

Where the direction cosines are:

$$\left. \begin{aligned} r_{fX} &= (X_0 - X_C)/r_f(J) \\ r_{fY} &= Y_0/r_f(J) \\ r_{fZ} &= Z_0/r_f(J) \end{aligned} \right\} \quad (4.33.1)$$

4.3.6 Normal to Plane of the Curved Ray at (XO,YO,ZO)

The vector cross product of \vec{r}_f and \vec{R} is normal to the plane defined by the two vectors.

$$\vec{NP}_f = \vec{r}_f \times \vec{R} = \begin{vmatrix} \hat{e}_X & \hat{e}_Y & \hat{e}_Z \\ r_{fX} & r_{fY} & r_{fZ} \\ K' & L' & M' \end{vmatrix} \quad (4.34)$$

$$\vec{NP}_f = NP_{fX} \cdot \hat{e}_X + NP_{fY} \cdot \hat{e}_Y + NP_{fZ} \cdot \hat{e}_Z \quad (4.34.1)$$

Where:

$$\left. \begin{aligned} NP_{fX} &= r_{fY} \cdot M' - r_{fZ} \cdot L' \\ NP_{fY} &= r_{fZ} \cdot K' - r_{fX} \cdot M' \\ NP_{fZ} &= r_{fX} \cdot L' - r_{fY} \cdot K' \end{aligned} \right\} \quad (4.34.2)$$

and

$$NP_f = \sqrt{NP_{fX}^2 + NP_{fY}^2 + NP_{fZ}^2} \quad (4.34.3)$$

The normalized direction cosines of the normal to the plane of the curved ray at (XO,YO,ZO) are therefore:

$$NP_{fX}/NP_f ; NP_{fY}/NP_f ; NP_{fZ}/NP_f \quad (4.34.4)$$

4.3.7 Calculating the Angle Between the Ray and the Front Radius

$$\vec{r}_f \cdot \vec{R} = |\vec{r}_f| \cdot |\vec{R}| \cdot \cos(\psi_f) \quad (4.35)$$

Both the ray and the unit vector for the front surface radius are normalized, i.e.

$$\left. \begin{aligned} |\vec{r}_f| &= (r_{fX}^2 + r_{fY}^2 + r_{fZ}^2)^{1/2} = 1 \\ |\vec{R}| &= (K'^2 + L'^2 + M'^2)^{1/2} = 1 \end{aligned} \right\} \quad (4.35.1)$$

Therefore:

$$\begin{aligned} \psi_f &= \cos^{-1}[\vec{r}_f \cdot \vec{R}] \\ &= \cos^{-1}[r_{fX} \cdot K' + r_{fY} \cdot L' + r_{fZ} \cdot M'] \end{aligned} \quad (4.35.2)$$

4.3.8 Calculating constant E

Knowing ψ_f , constant E can be calculated using equation (4.2).

4.3.9 Intercept Point of the Curved Ray with Rear Surface (Point XI,YI,ZI)

4.3.9.1 Equations

As previously, θ_e is the angle between the front radius and the rear radius.

$$r_{rX} \cdot r_{fX} + r_{rY} \cdot r_{fY} + r_{rZ} \cdot r_{fZ} = \cos[\theta_e(J)] \quad (4.36)$$

The direction cosines of the front radius were calculated in equation (4.33). Similarly, the direction cosines of the rear radius are:

$$\left. \begin{aligned} r_{rX} &= (XI - X_C) / r_r(J) \\ r_{rY} &= YI / r_r(J) \\ r_{rZ} &= ZI / r_r(J) \end{aligned} \right\} \quad (4.36.1)$$

Therefore, equation (4.36) can have the form:

$$(XI - X_C)r_{rX} + (YI)r_{rY} + (ZI)r_{rZ} = r_r(J) \cdot \cos[\theta_e(J)] \quad (4.36.2)$$

The rear radius is defined as:

$$(XI - X_C)^2 + (YI)^2 + (ZI)^2 = [r_r(J)]^2 \quad (4.37)$$

The rear surface was defined previously. Consequently:

$$-(aXI - b)^2 + (YI)^2 + (ZI)^2 = 0 \quad (3.33)$$

a,b were defined by equations 3.33.1 and 3.33.2.

Also, from geometry:

$$(XI - X_C) = r_r(J) \cdot \cos[\theta_0(J)] \quad (4.38)$$

Another equation arrives from the connection between the two radii through eq. (4.4).

4.3.9.2 Solution

- a. Assume $\theta_e(J)$.
- b. Calculate $r_r(J)$ from the formula (equation 4.4).
- c. Calculate XI from equation (4.36.2):

$$XI = r_r(J) \cdot \cos[\theta_0(J)] + X_C \quad (4.36.3)$$

- d. Calculate radius from equations

(4.37) and (4.36.3):

$$\begin{aligned}
 \text{Radius} = R &= [(YI)^2 + (ZI)^2]^{\frac{1}{2}} \\
 &= r_r(J) [1 - \cos^2[\theta_0(J)]] \\
 &= r_r(J) \cdot \sin[\theta_0(J)] \quad (4.37.1)
 \end{aligned}$$

e. Calculate parameters

a and b from equations (3.33.1) and (3.33.2) as in the homogeneous case.

f. Substituting into equation (3.33):

$$XI = (R + b)/a = \{r_r(J) \cdot \sin[\theta_0(J)] + b\}/a \quad (4.38)$$

where R is the radius defined in equation (4.37.1).

g. Solving equations (4.36.3), (4.38) for $\theta_0(J)$ one gets:

$$\theta_0(J) = \sin^{-1} \left[-\frac{B'}{A'} + \frac{\sqrt{(B')^2 - (A')(C')}}{A'} \right] \quad (4.39)$$

Where:

$$\left. \begin{aligned}
 A' &= [r_r(J)]^2 (1 + a^2) \\
 B' &= [r_r(J)] (b - a \cdot X_C) \\
 C' &= (b - a \cdot X_C)^2 - a^2 \cdot [r_r(J)]^2
 \end{aligned} \right\} \quad (4.40)$$

h. Knowing $\theta_0(J)$, it is possible to calculate new value for $\theta_e(J)$ and iterate through steps (a) - (g) until the difference in the values of $\theta_0(J)$ is

small enough.

i. When an accurate value of $\theta_0(J)$ is received, XI is calculated from equation (4.36.3).
 YI and ZI are calculated using equations (4.36) and (4.37.1).
 Consequently:

$$\left. \begin{aligned} YI &= \frac{B''}{A''} + \frac{\sqrt{(B'')^2 - (A'')(C'')}}{A''} \\ ZI &= \sqrt{\{r_r(J) \cdot \sin[\theta_0(J)]\}^2 - \{YI\}^2} \end{aligned} \right\} \quad (4.41)$$

Where:

$$\left. \begin{aligned} A'' &= 1 + [r_{fY}]^2/[r_{fZ}]^2 \\ B'' &= \{r_r(J) \cdot \cos[\theta_e(J)] - (XI - X_C)r_{fX}\}r_{fY}/r_{fZ} \\ C'' &= \left\{ \frac{r_r(J)}{r_{fZ}} \cdot \cos[\theta_e(J)] - (XI - X_C)\frac{r_{fX}}{r_{fZ}} \right\}^2 - \left\{ r_r(J) \cdot \sin[\theta_0(J)] \right\}^2 \end{aligned} \right\} \quad (4.42)$$

When $r_{fZ} = 0$, the solution for YI and ZI is different:

$$YI = \{r_r(J) \cdot \cos[\theta_e(J)] - (XI - X_C)r_{fX}\}/r_{fY} \quad (4.43)$$

While ZI is calculated by equation (4.41).

4.3.10 Direction Cosines of the Ray at the Rear Surface

a. Similarly to what was done at the front surface (equation 4.35):

$$\vec{r}_r \cdot \vec{R} = |\vec{r}_r| \cdot |\vec{R}| \cdot \cos(\psi_r) \quad (4.44)$$

Both the ray and the rear radius are normalized; therefore:

$$r_{rX} \cdot K_r' + r_{rY} \cdot L_r' + r_{rZ} \cdot M_r' = \cos\psi_r \quad (4.44.1)$$

b. The ray remains within the same plane while transferring from the front surface to the rear surface.

i.e.:

$$NP_{fX} \cdot K'_r + NP_{fY} \cdot L'_r + NP_{fZ} \cdot M'_r = \cos(\pi/2) = 0 \quad (4.45)$$

c. The direction cosines of the ray are normalized, i.e.

$$(K'_r)^2 + (L'_r)^2 + (M'_r)^2 = 1 \quad (4.46)$$

d. Solution:

$$\begin{aligned} (d1) \quad & NP_{fX} \neq 0, NP_{fY} \neq 0, NP_{fZ} \neq 0 \\ & \left. \begin{aligned} (L'_r) &= \frac{B''}{2A''} \pm \frac{\sqrt{(B'')^2 - 4(A'')(C'')}}{2A''} \\ (M'_r) &= \frac{C}{B} - \frac{A}{B} (L'_r) \\ (K'_r) &= [-NP_{fY} \cdot (L'_r) - NP_{fZ} \cdot (M'_r)] / NP_{fX} \end{aligned} \right\} \quad (4.47) \end{aligned}$$

Where:

$$\begin{aligned} A &= NP_{fX} \cdot r_{rY} - NP_{fY} \cdot r_{rX} \\ B &= NP_{fX} \cdot r_{rZ} - NP_{fZ} \cdot r_{rX} \\ C &= NP_{fX} \cdot \cos(\psi_r) \\ A' &= \left(\frac{NP_{fY}}{NP_{fX}} \right)^2 + 1 \\ B' &= \left(\frac{NP_{fZ}}{NP_{fX}} \right)^2 + 1 \\ C' &= \frac{2(NP_{fY})(NP_{fZ})}{(NP_{fX})^2} \end{aligned} \quad (4.48)$$

$$\left. \begin{aligned}
 A'' &= (A') + (B') \left(\frac{A}{B}\right)^2 - \frac{(C')(A)}{(B)} \\
 B'' &= \frac{2(A)(C)(B')}{(B)^2} - \frac{(C')(C)}{(B)} \\
 C'' &= (B') \left(\frac{C}{B}\right)^2 - 1
 \end{aligned} \right\} \quad (4.48)$$

In (4.47) the (+) sign is used when $r_{rY} < 0$ while the (-) sign is used when $r_{rY} \geq 0$.

(d2) In the above case, when $B = 0$ (look for definition of B in equation (4.48)) the solution for direction cosines of the ray is different.

$$\left. \begin{aligned}
 (L'_r) &= \frac{C}{A} \\
 (M'_r) &= -\frac{(C')(L'_r)}{2(B')} \pm \sqrt{\frac{\left[\frac{(C')(L'_r)}{2}\right]^2 - (B')[(A')(L'_r)^2 - 1]}{B'}} \\
 (K'_r) &= [-NP_{fY} \cdot (L'_r) - NP_{fZ} \cdot (M'_r)]/NP_{fX}
 \end{aligned} \right\} \quad (4.49)$$

All the symbols used here were defined in equation (4.48) and the \pm sign is used as before.

$$(d3) \quad \underline{NP_{fX} = 0, NP_{fY} = 0, NP_{fZ} \neq 0, r_{rY} \neq 0}$$

$$(M'_r) = 0 \quad (4.50)$$

$$\left. \begin{aligned}
 (K'_r) &= \frac{B''}{A''} \pm \frac{\sqrt{(B'')^2 - (A'')(C'')}}{A''} \\
 (L'_r) &= \frac{1}{r_{rY}} [\cos(\psi_r) - r_{rX} \cdot K'_r]
 \end{aligned} \right\} \quad (4.50)$$

The (+) sign is used here.

While in this case:

$$\left. \begin{aligned}
 A'' &= 1 + \left(\frac{r_{rX}}{r_{rY}} \right)^2 \\
 B'' &= \cos(\psi_r) \frac{r_{rX}}{(r_{rY})^2} \\
 C'' &= \left[\frac{\cos(\psi_r)}{r_{rY}} \right]^2 - 1
 \end{aligned} \right\} \quad (4.51)$$

(d4) In the above case, when $r_{rY} = 0$ the solution is:

$$\left. \begin{aligned}
 (M'_r) &= 0 \\
 (K'_r) &= \frac{\cos(\psi_r)}{r_{rX}} \\
 (L'_r) &= \pm \sqrt{1 - (K'_r)^2}
 \end{aligned} \right\} \quad (4.52)$$

Again, the (+) sign is used here.

$$(d5) \quad \underline{NP_{fX} = 0, NP_{fY} \neq 0, NP_{fZ} = 0, r_{rZ} \neq 0}$$

The solution is similar to that in case (d3).

$$\left. \begin{aligned}
 (L'_r) &= 0 \\
 (K'_r) &= \frac{B''}{A''} \pm \frac{\sqrt{(B'')^2 - (A'')(C'')}}{(A'')} \\
 (M'_r) &= \frac{1}{r_{rZ}} [\cos(\psi_r) - r_{rX} \cdot K'_r]
 \end{aligned} \right\} \quad (4.53)$$

(A'') , (B'') , (C'') are the same as defined in (4.51) except that r_{rY} is replaced everywhere by r_{rZ} . The (+) sign is used here.

(d6) In the above case, when $r_{rZ} = 0$ the solution is similar to that in case (d4):

$$\left. \begin{aligned}
 (L'_r) &= 0 \\
 (K'_r) &= \frac{\cos(\psi_r)}{r_{rX}} \\
 (M'_r) &= \pm \sqrt{1 - (K'_r)^2}
 \end{aligned} \right\} \quad (4.54)$$

Also here, the (+) sign is used.

$$(d7) \quad \underline{NP_{fX} = 0, NP_{fY} \neq 0, NP_{fZ} \neq 0, r_{rX} = 0}$$

$$\left. \begin{aligned}
 (L'_r) &= \frac{\cos(\psi_r)}{r_{rY} - \frac{NP_{fY}}{NP_{fZ}} \cdot r_{rZ}} \\
 (M'_r) &= - \frac{NP_{fY}}{NP_{fZ}} (L'_r) \\
 (K'_r) &= \pm \sqrt{1 - (L'_r)^2 - (M'_r)^2}
 \end{aligned} \right\} \quad (4.55)$$

The (+) sign is used here.

$$(d8) \quad \text{As in (d7), but: } (r_{rY} - \frac{NP_{fY}}{NP_{fZ}} \cdot r_{rZ}) = 0;$$

$$\underline{r_{rX} \neq 0}$$

$$(K'_r) = \frac{\cos(\psi_r)}{r_{rX}}$$

$$(L'_r) = \pm \frac{1 - (K'_r)^2}{\sqrt{1 + \left(\frac{NP_{fY}}{NP_{fZ}}\right)^2}}$$

$$(M'_r) = -\frac{NP_{fY}}{NP_{fZ}} (L'_r)$$

(4.56)

$$(d9) \quad \text{As in (d7), but: } r_{rX} \neq 0$$

$$(L'_r) = \frac{(B'')}{2(A'')} \pm \frac{\sqrt{(B'')^2 - 4(A'')(C'')}}{2(A'')}$$

$$(M'_r) = -\frac{NP_{fY}}{NP_{fZ}} (L'_r)$$

$$(K'_r) = \frac{1}{r_{rX}} [\cos(\psi_r) - (r_{rY} - \frac{NP_{fY}}{NP_{fZ}} r_{rZ}) (L'_r)]$$

(4.57)

As in case (d1), the (+) sign is used when: $r_{rY} < 0$ while
the (-) sign is used when: $r_{rY} \geq 0$.

5. FLOW CHART OF PROGRAM LENS

(Homogeneous Case)

Note: Subroutines SHAPET, SKEWT compute the shape of lens and the skew rays as described in the previous sections (3,4). However, subroutines SHAPEC, SKEWC compute the shape and the skew rays of a different design of the lens. In this design, the fixed cone is the rear surface instead of the front surface (compare figure 9 to figure 2.). The equations for this different design are not included in the current report. The equations are part of Capt. Carr's thesis [15] and will be described there.

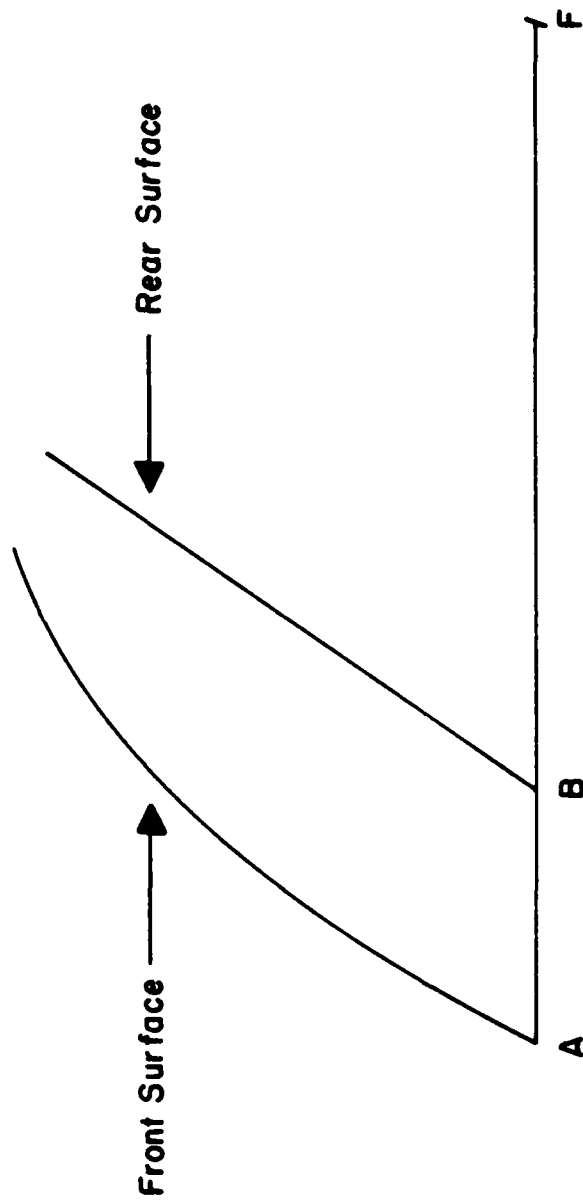
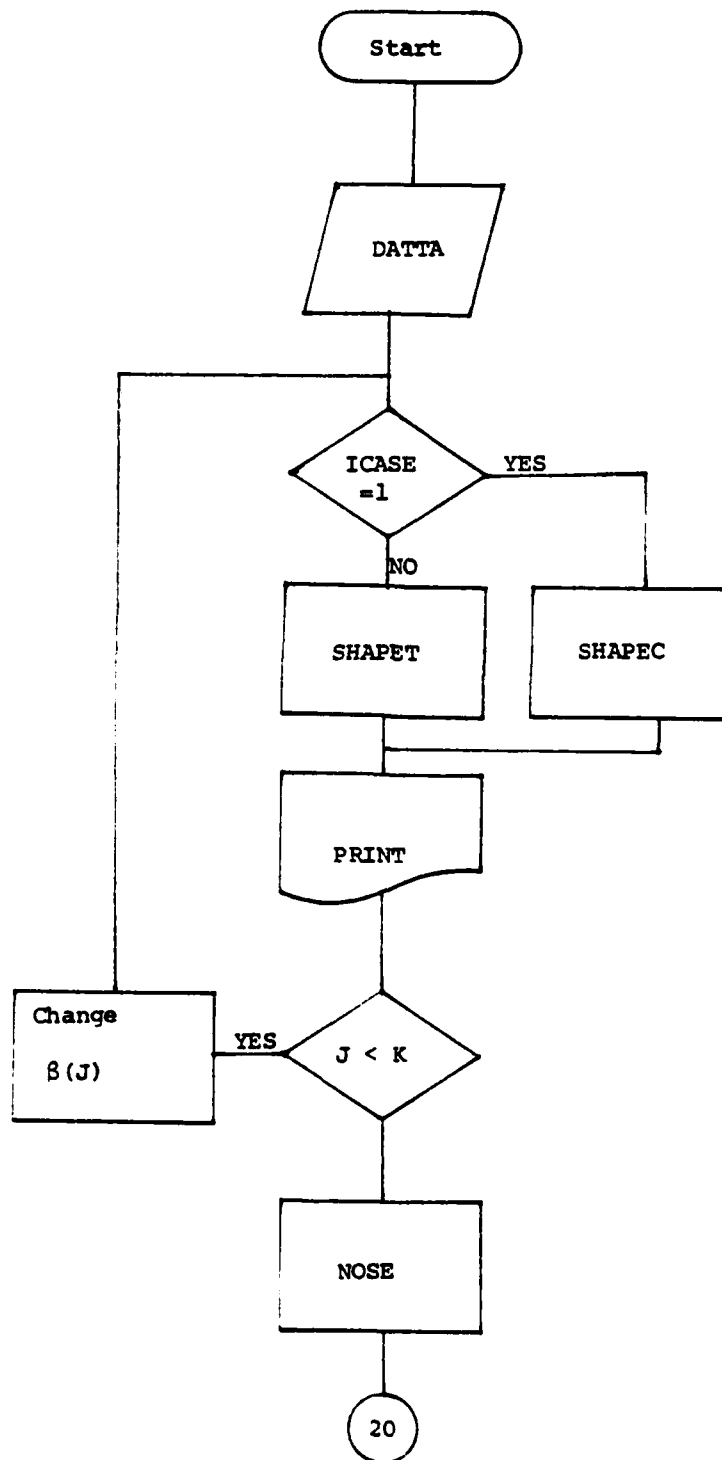
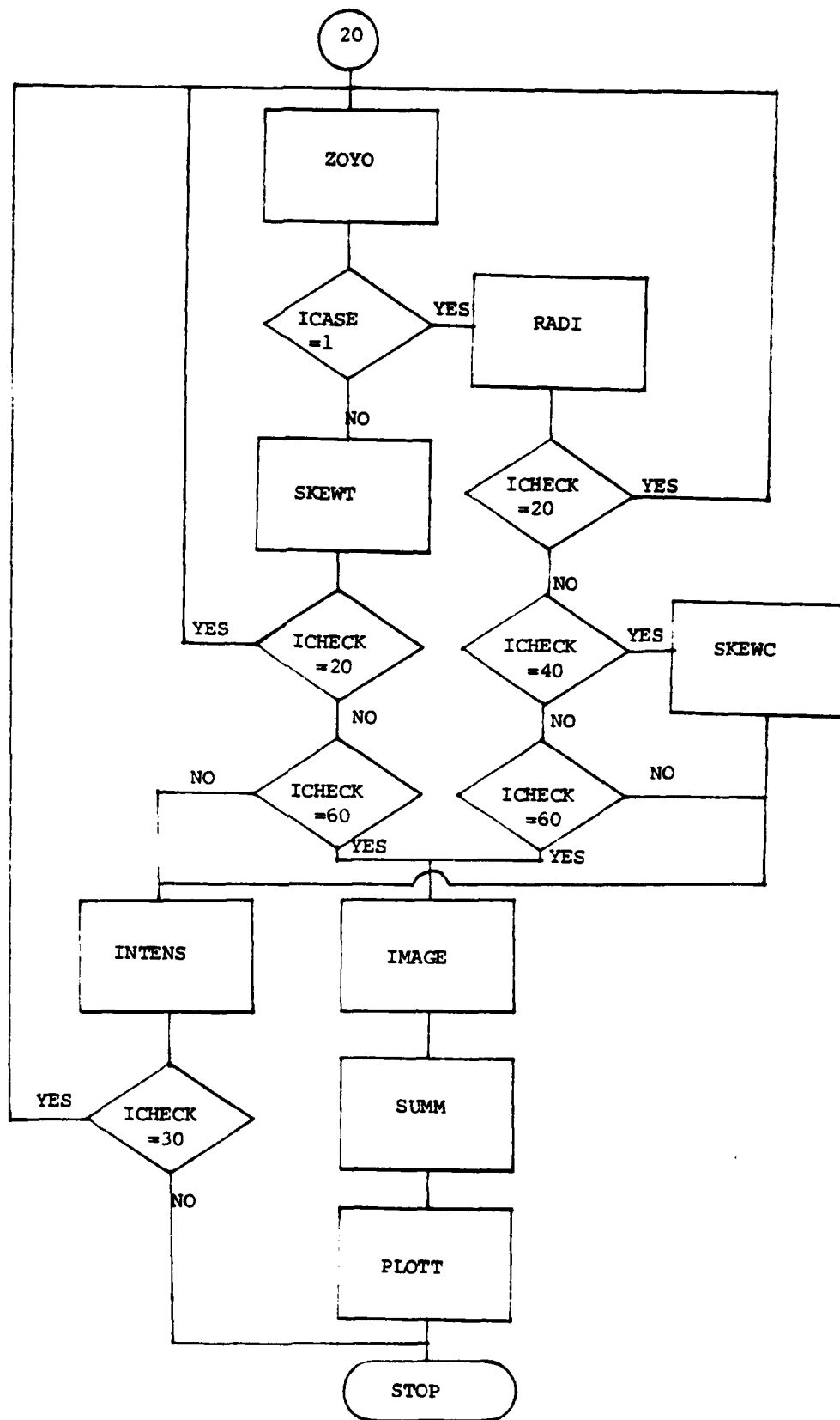
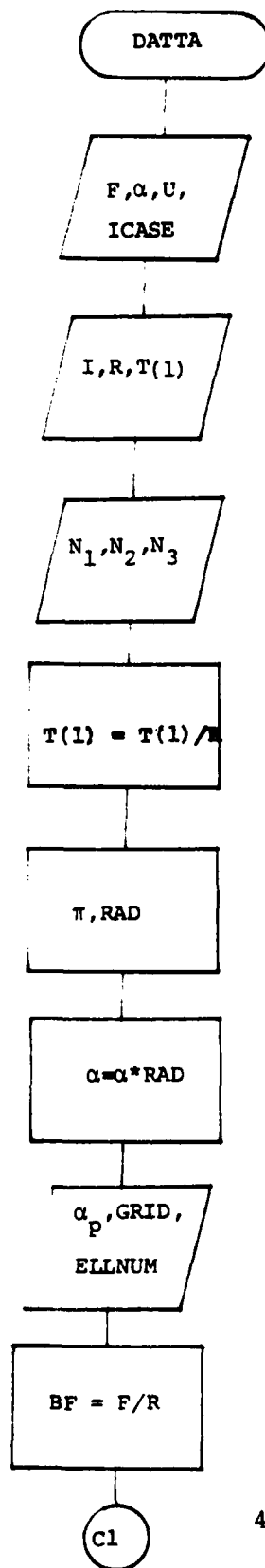


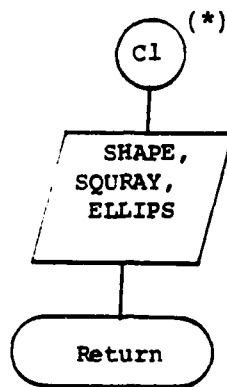
Figure 9. Illustration of the lens which has a circular cone on the inside surface.

Program LENS - Main

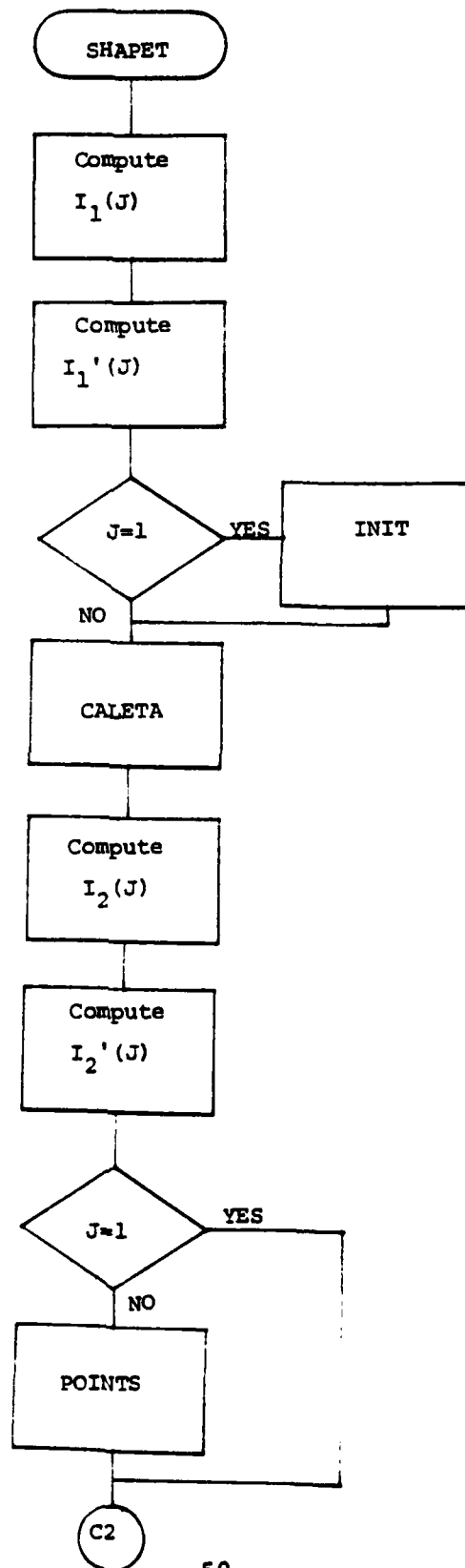


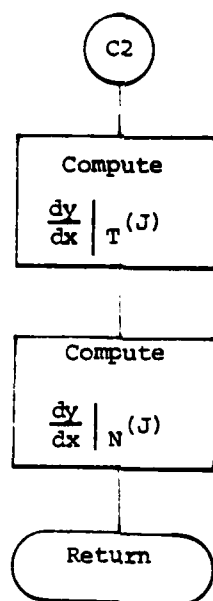


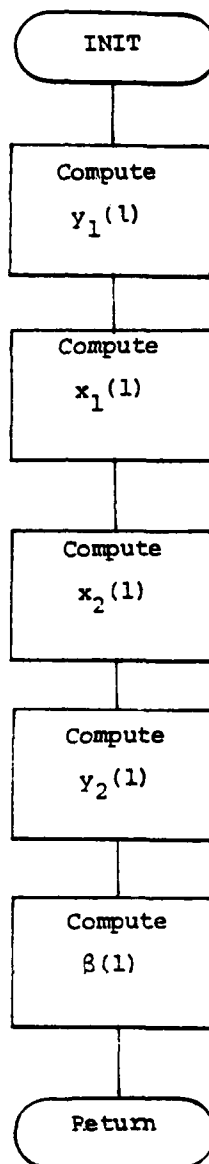


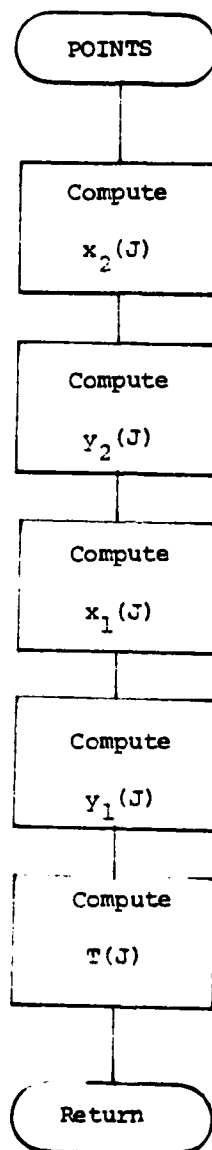


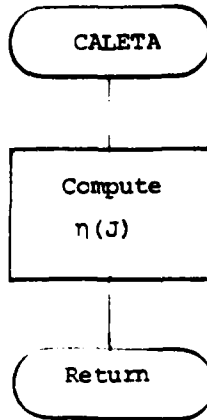
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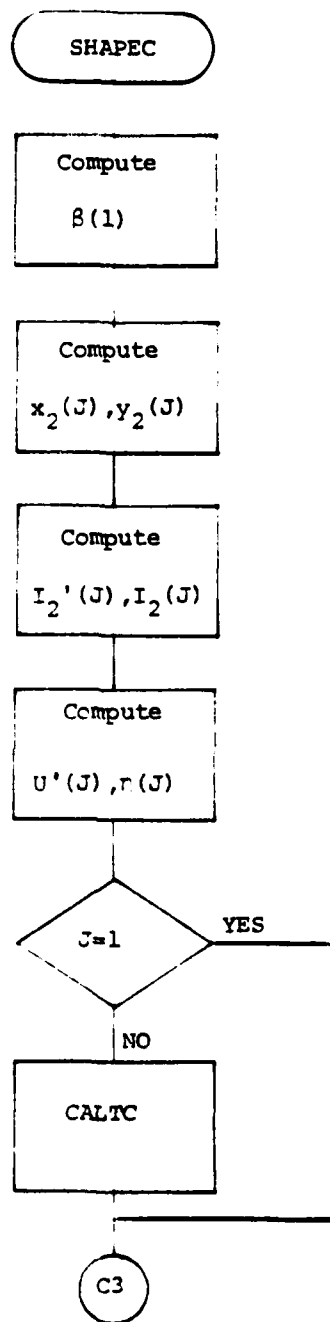


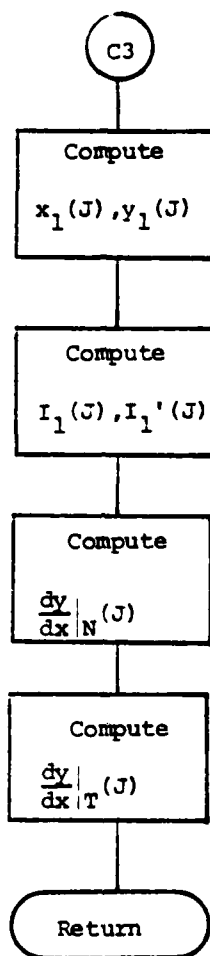


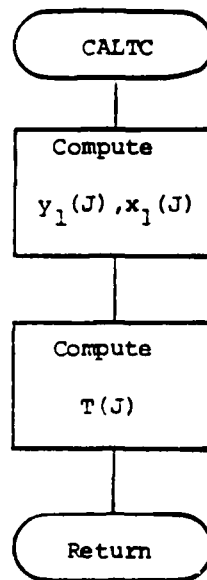


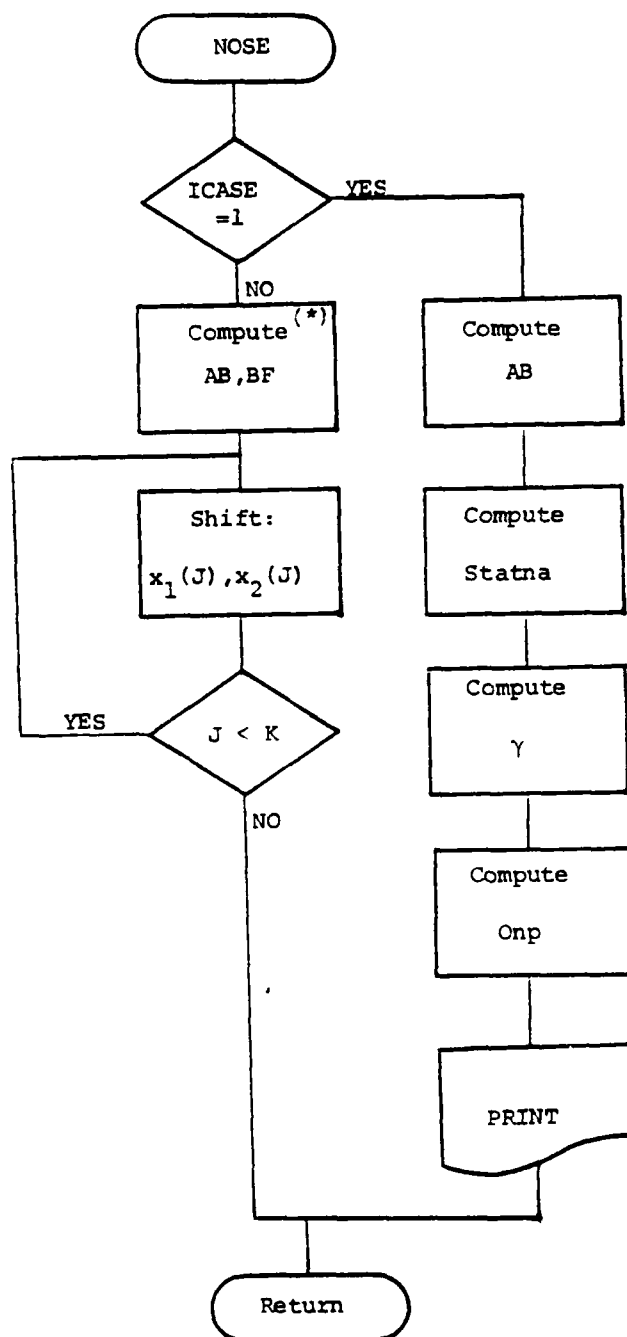




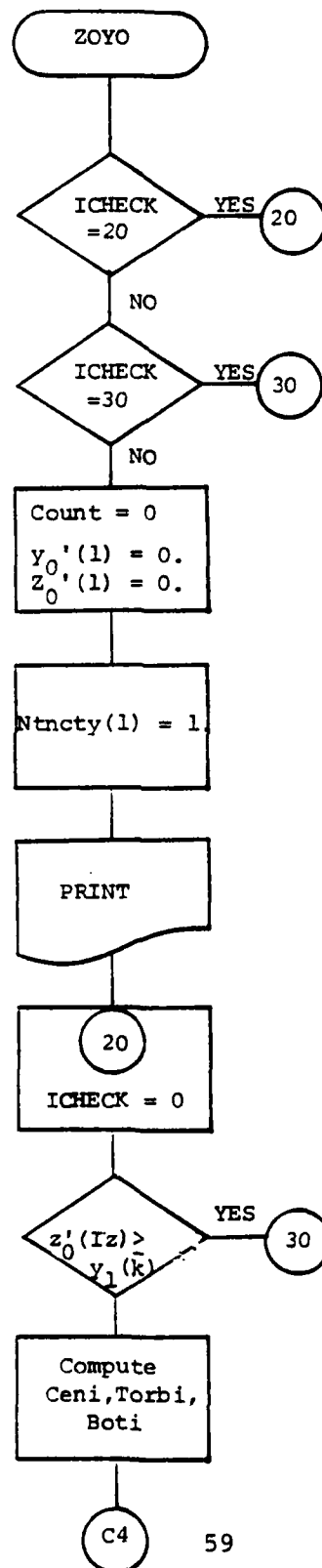


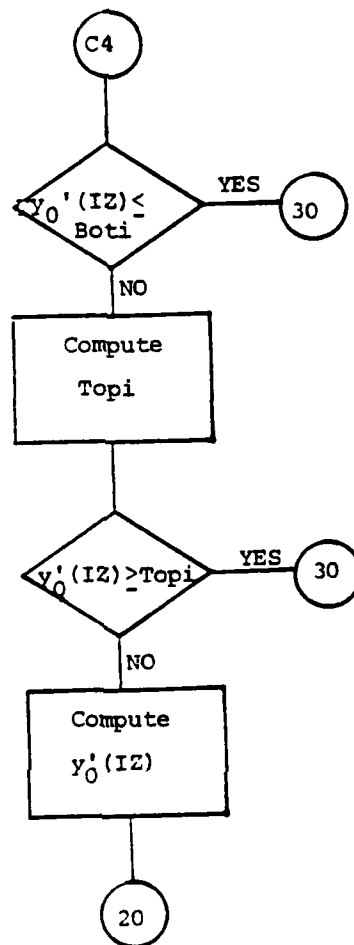


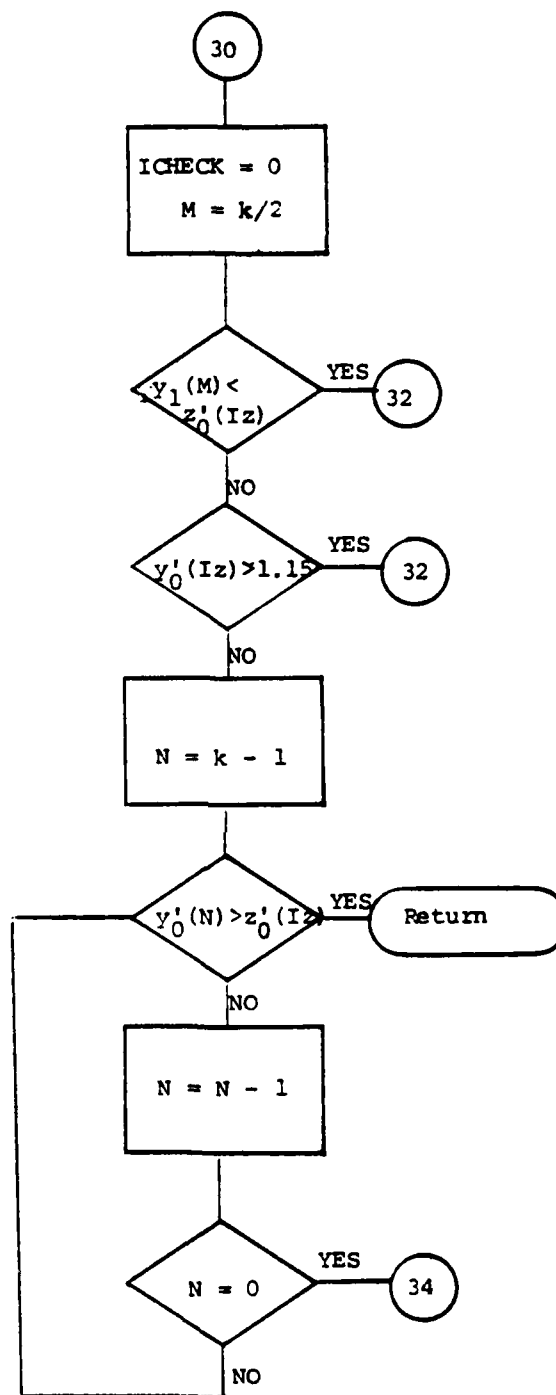


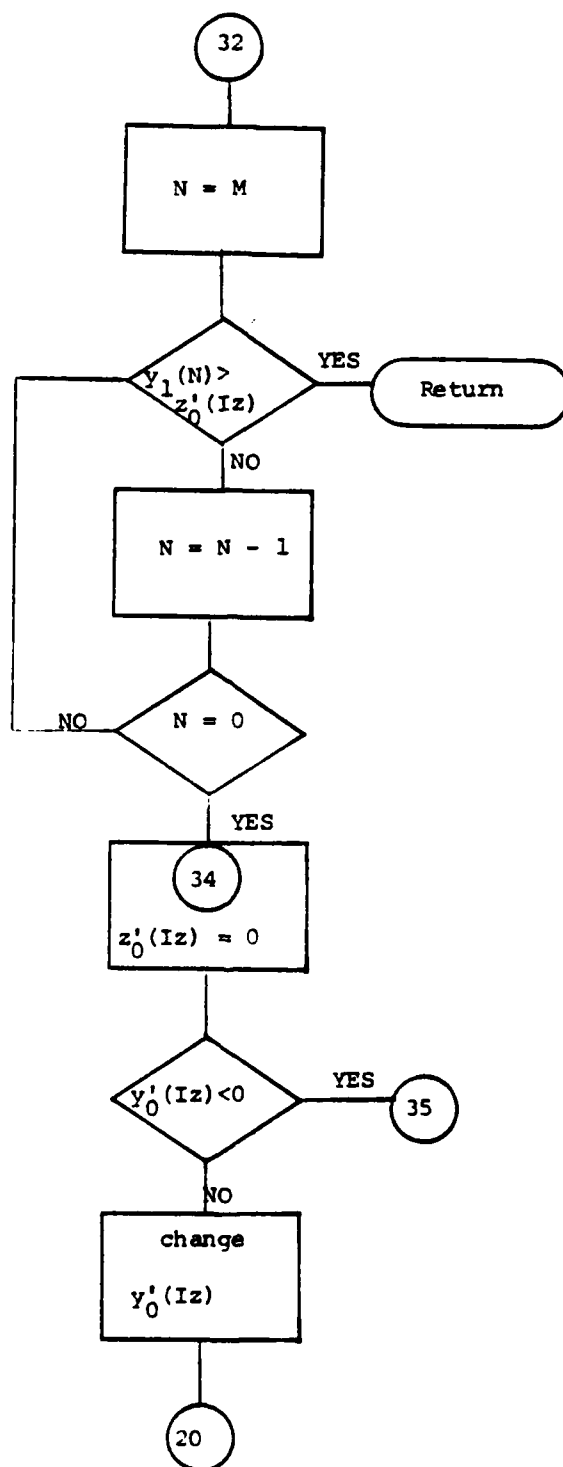


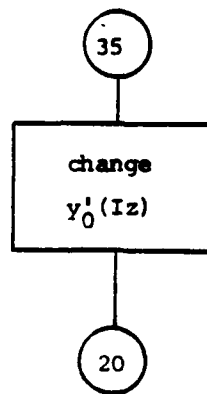
(*) In program GRIN, which uses the same subroutine, here, also xc is shifted.

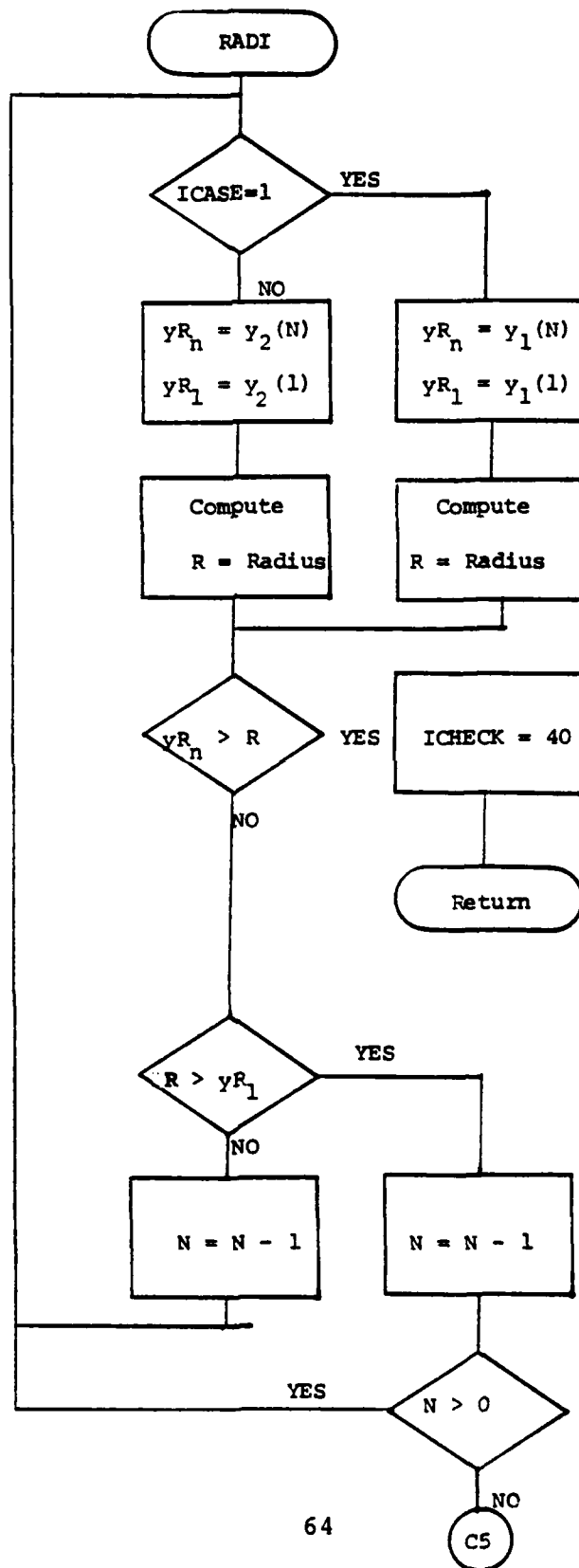


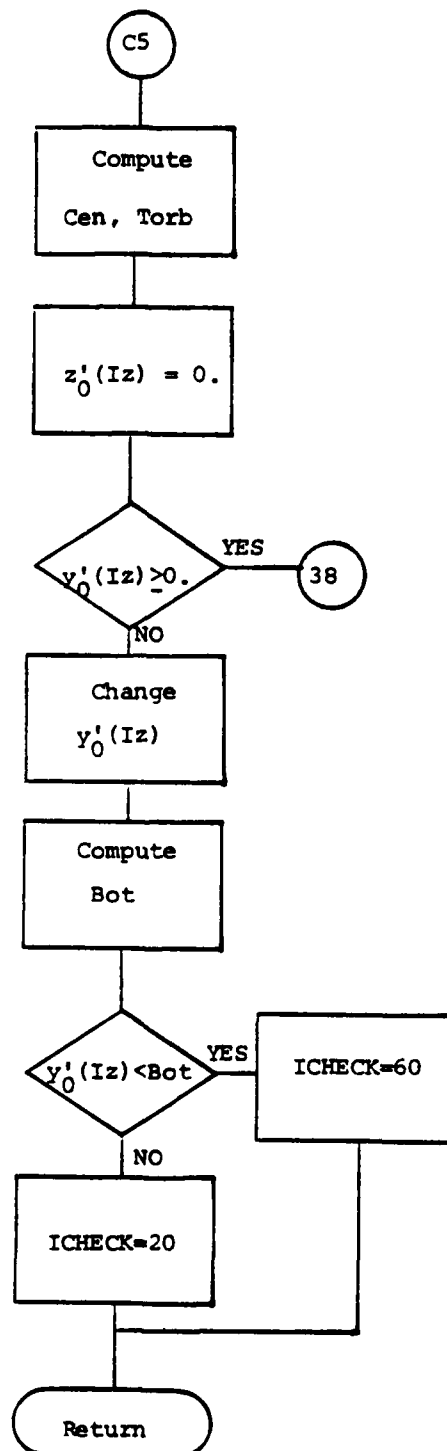


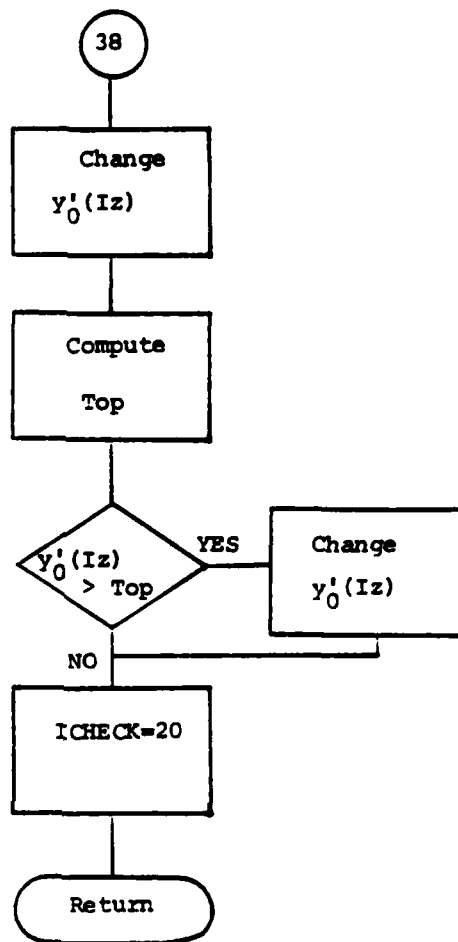


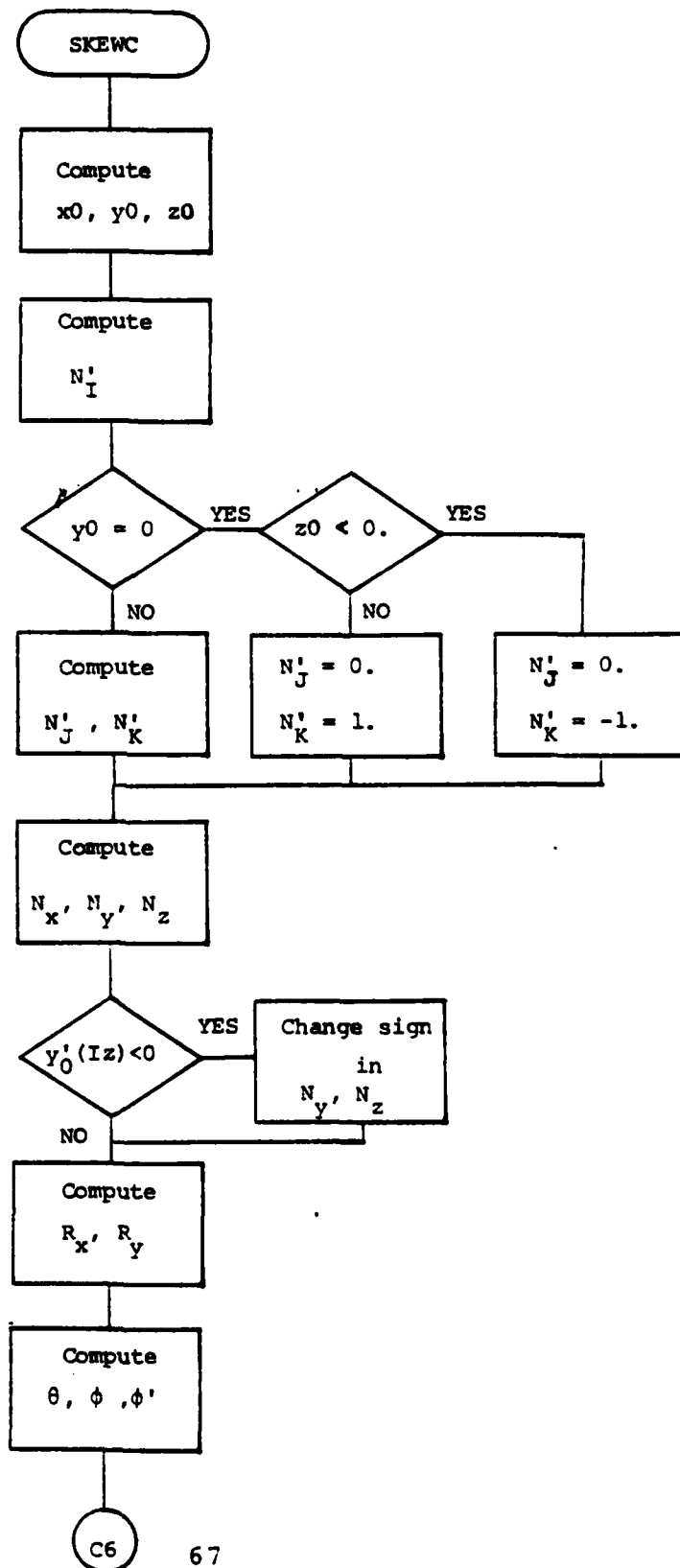


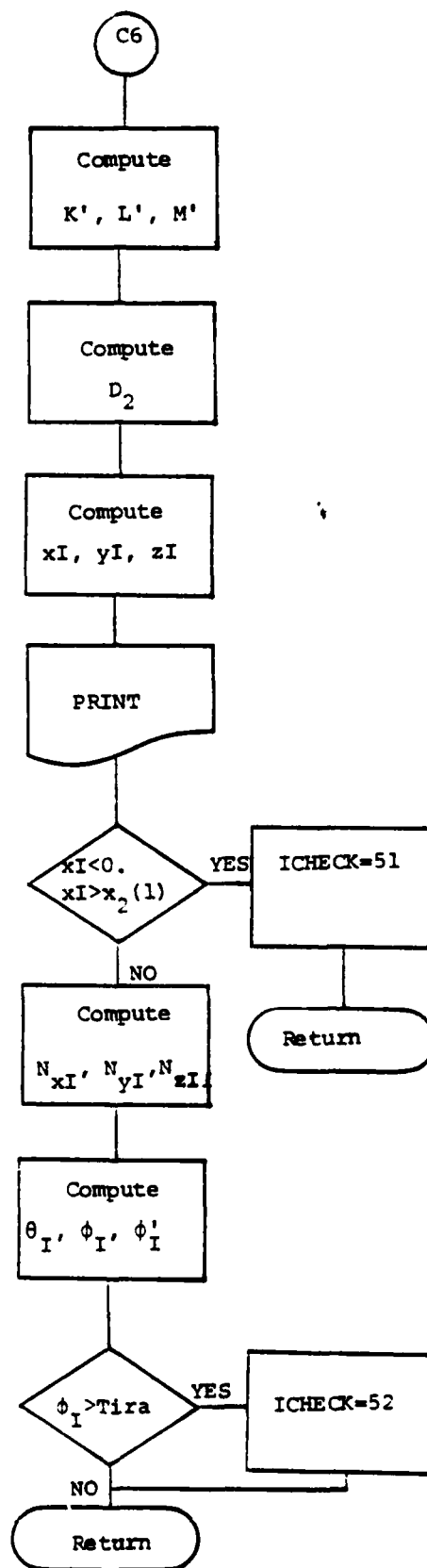


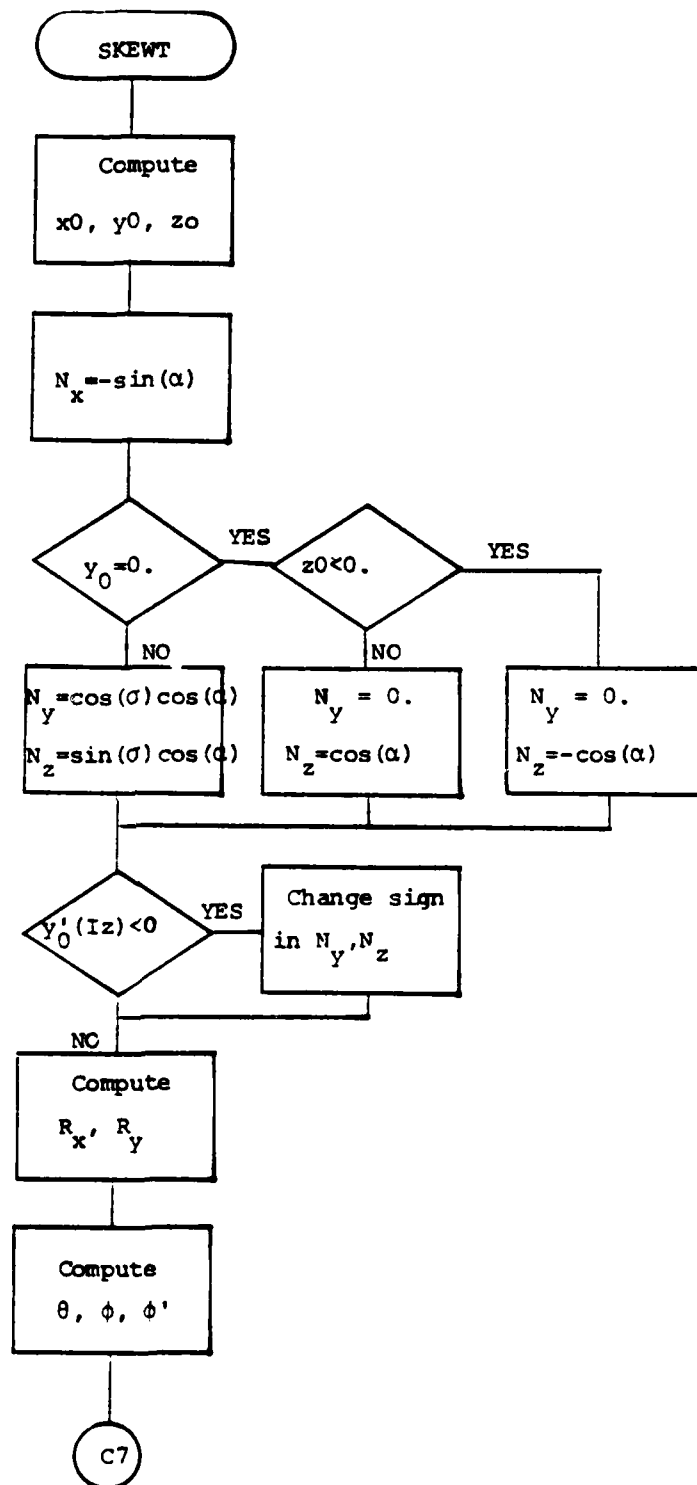


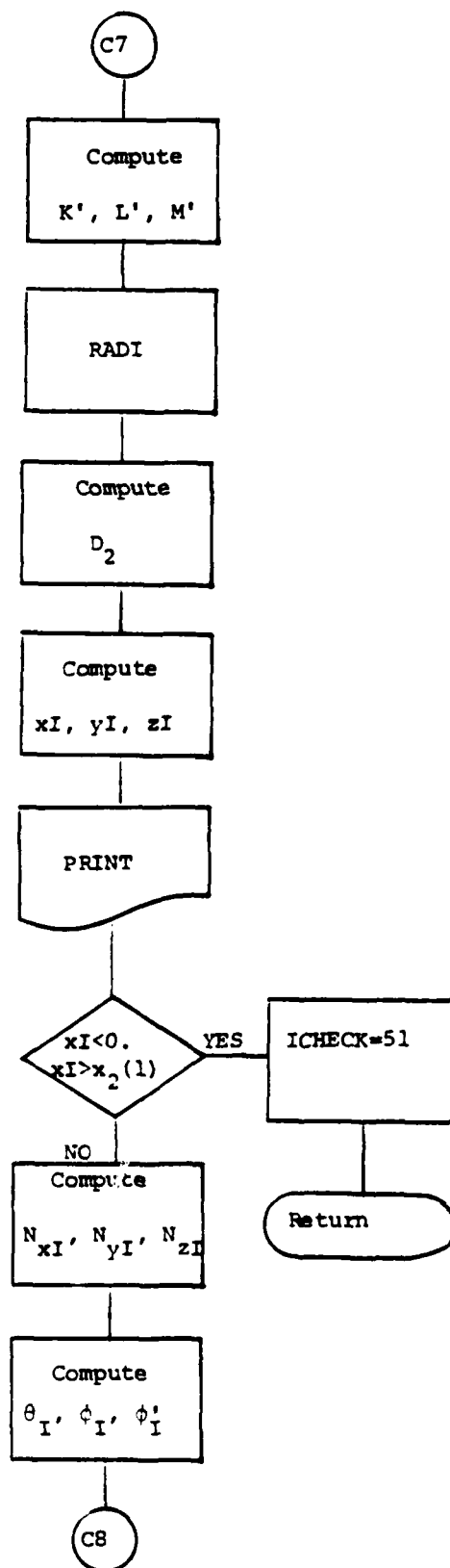


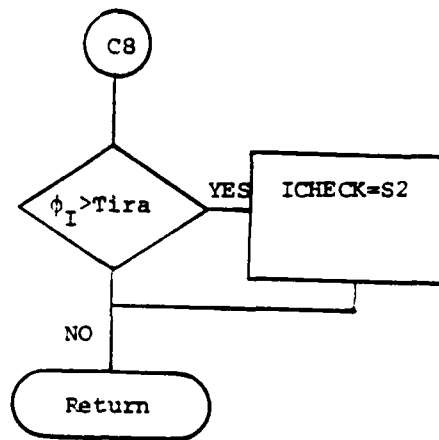


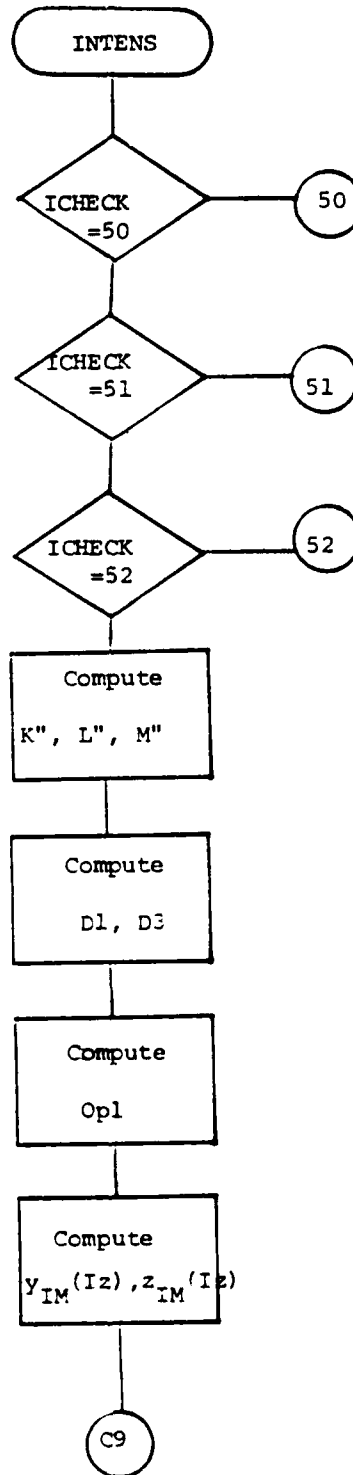


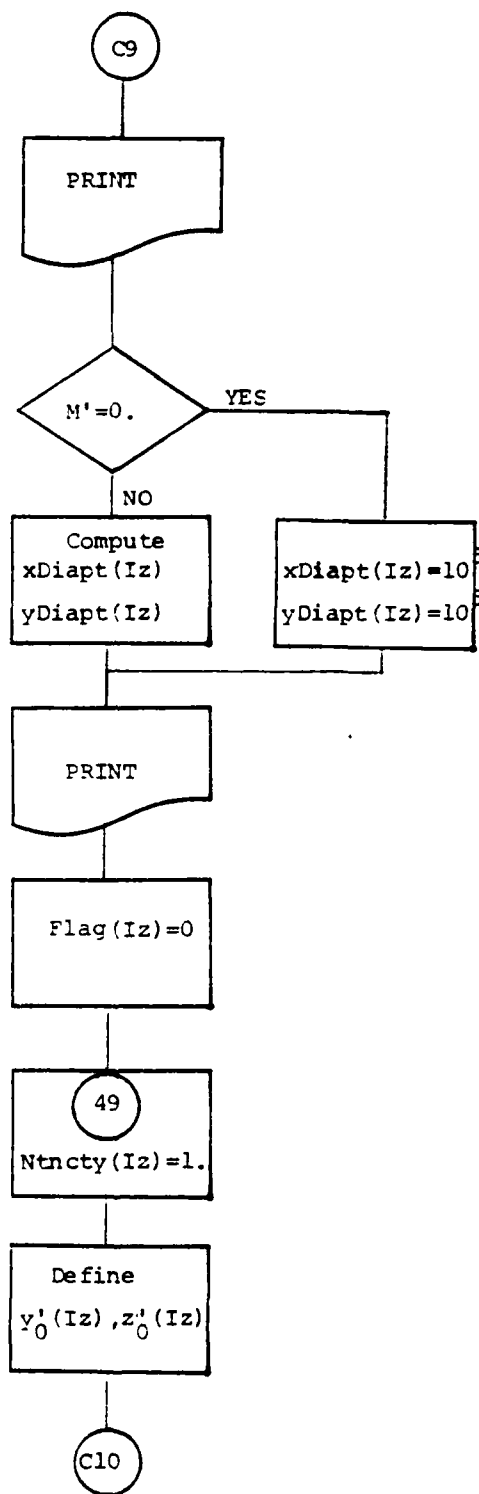


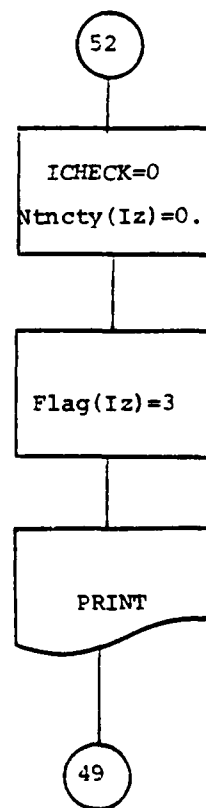
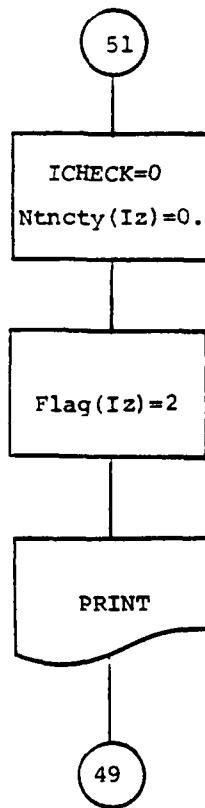
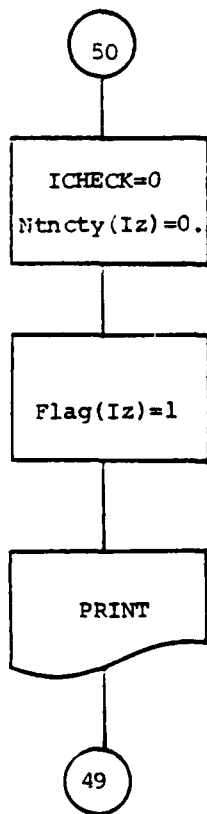
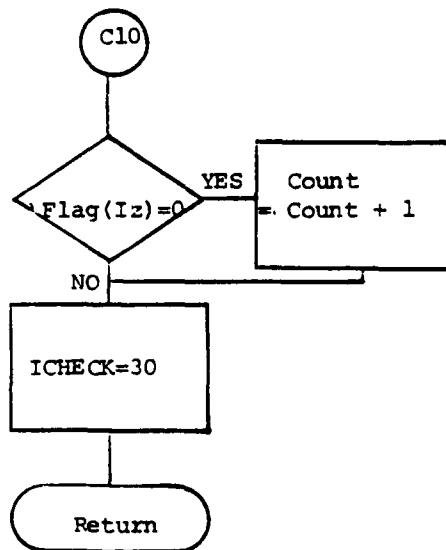


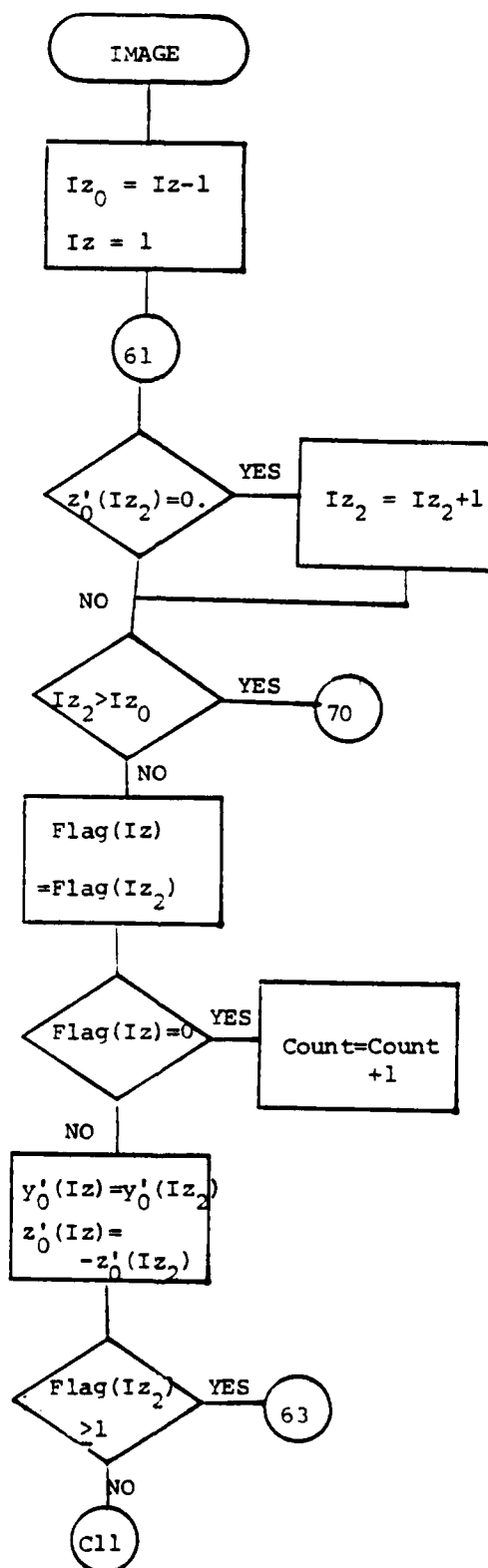


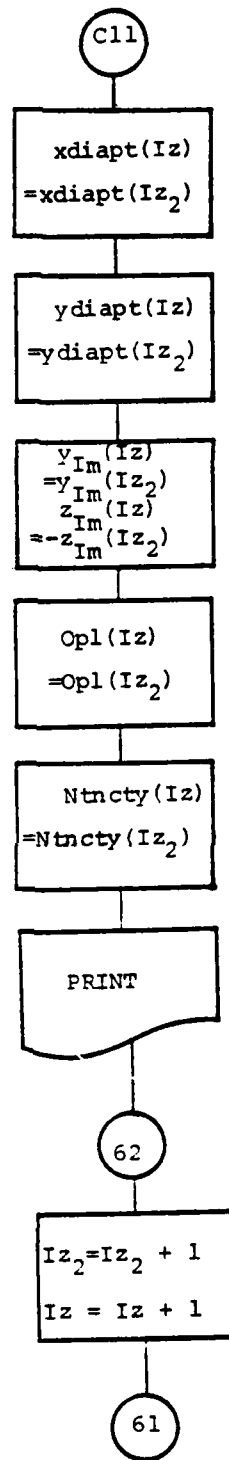


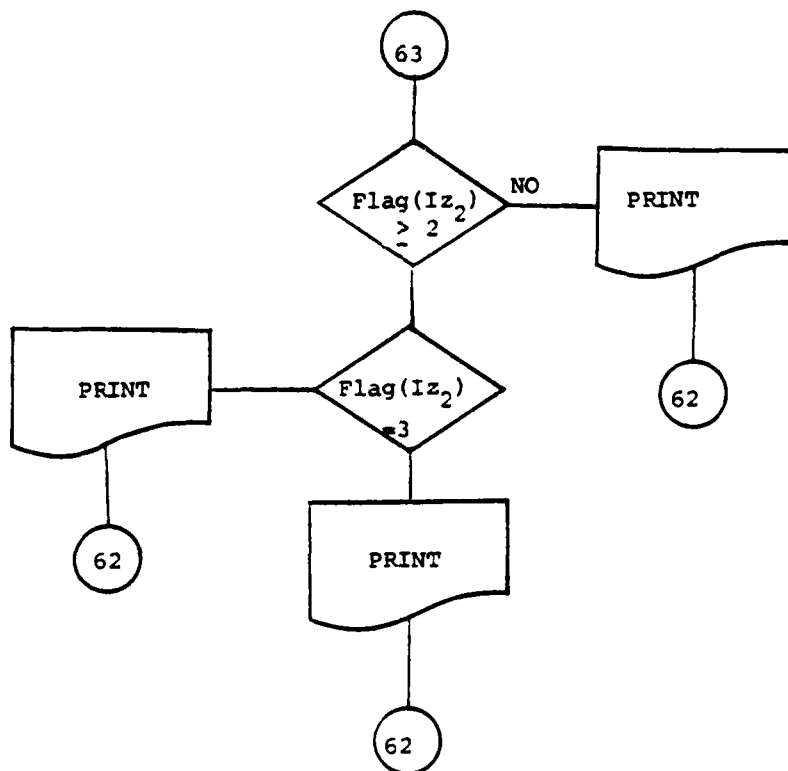


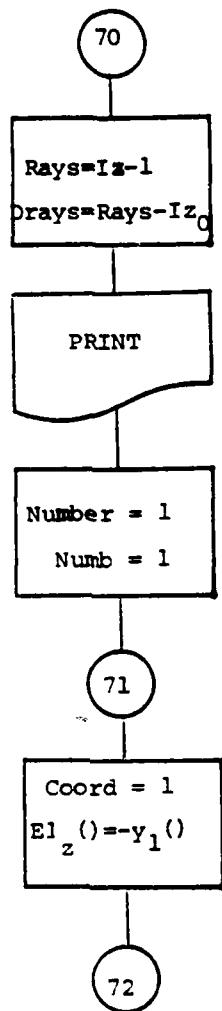


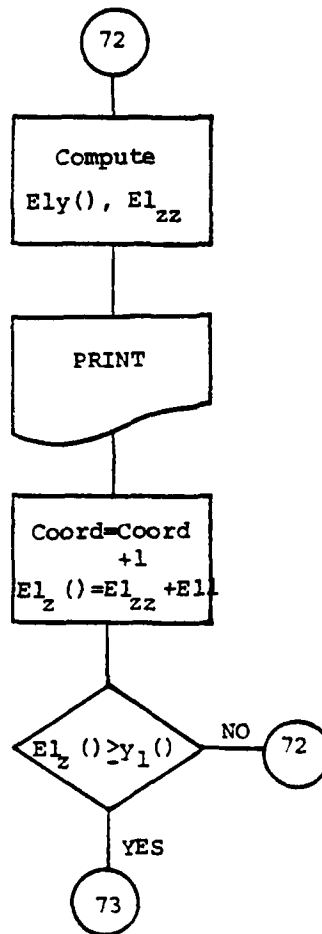


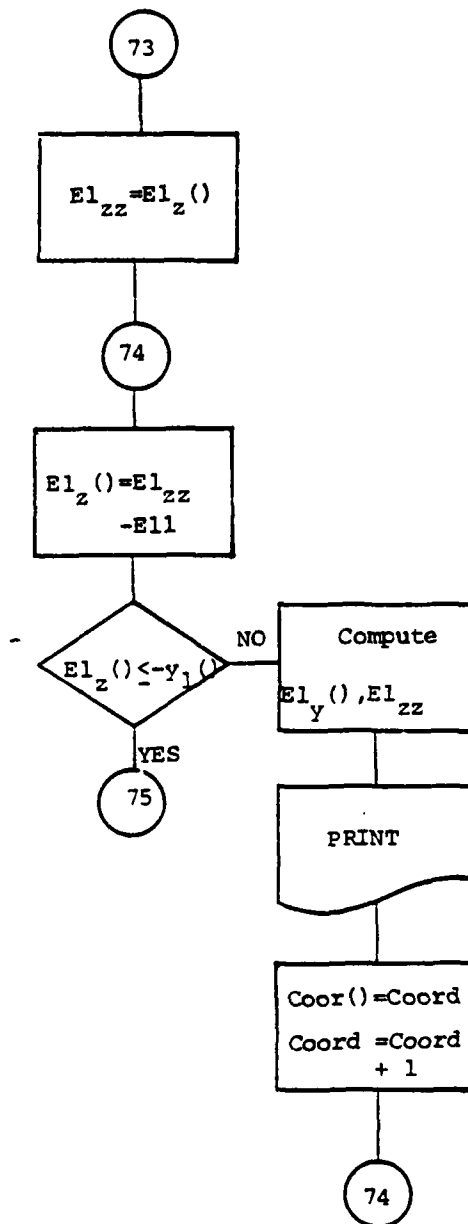


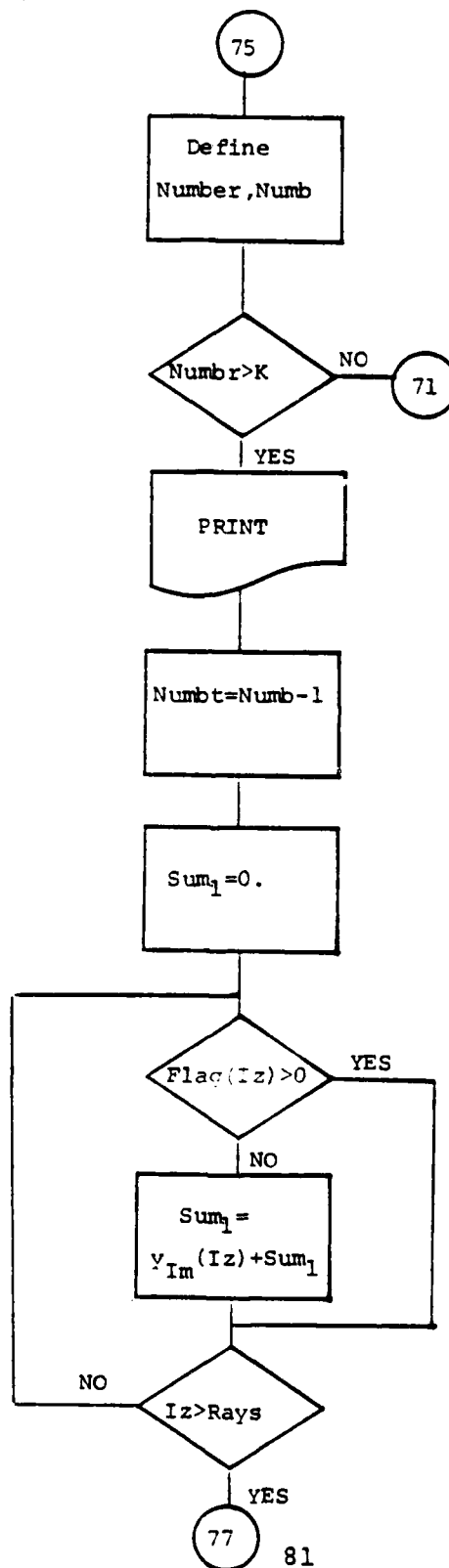


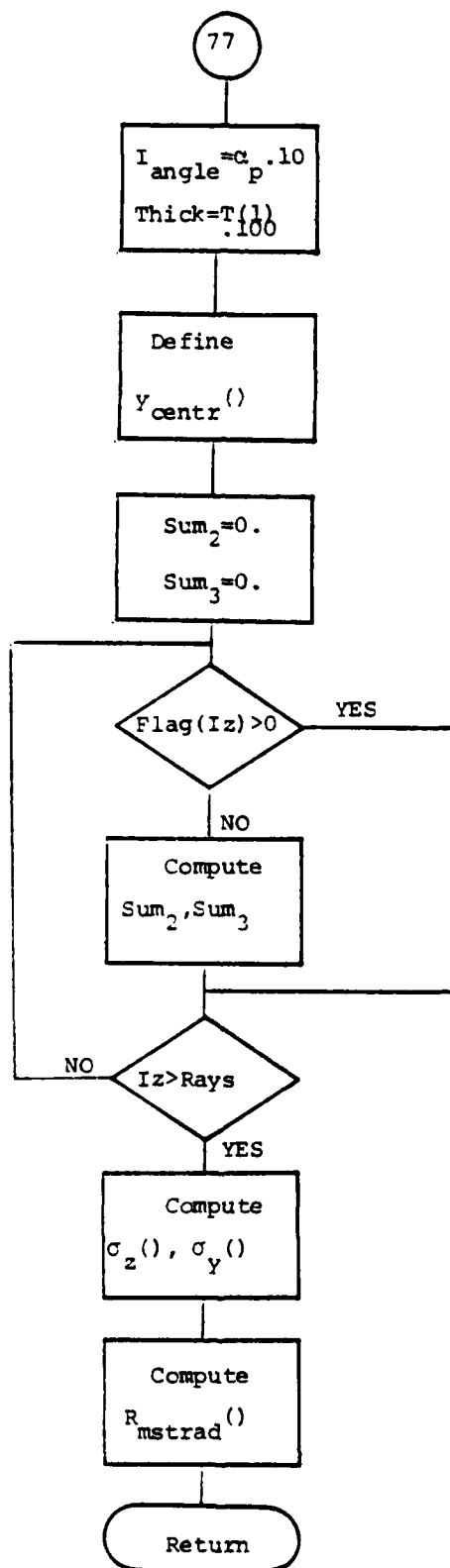


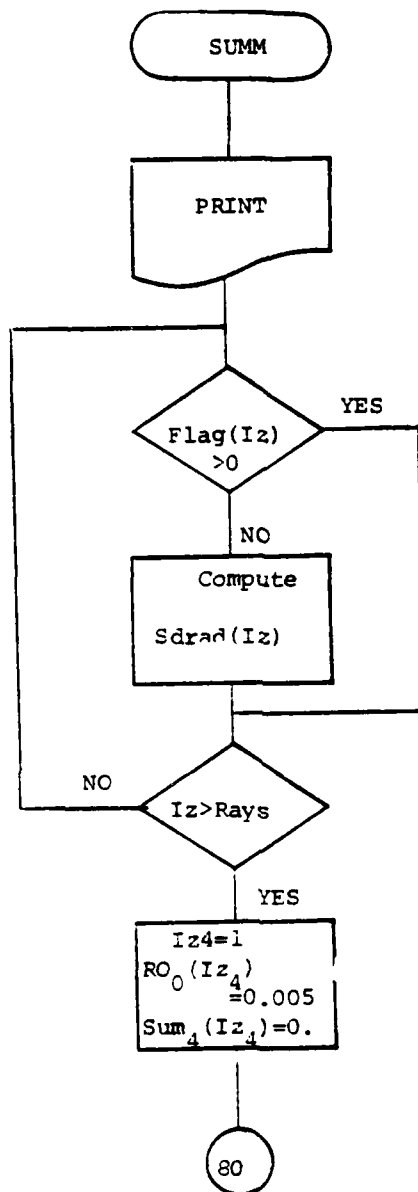


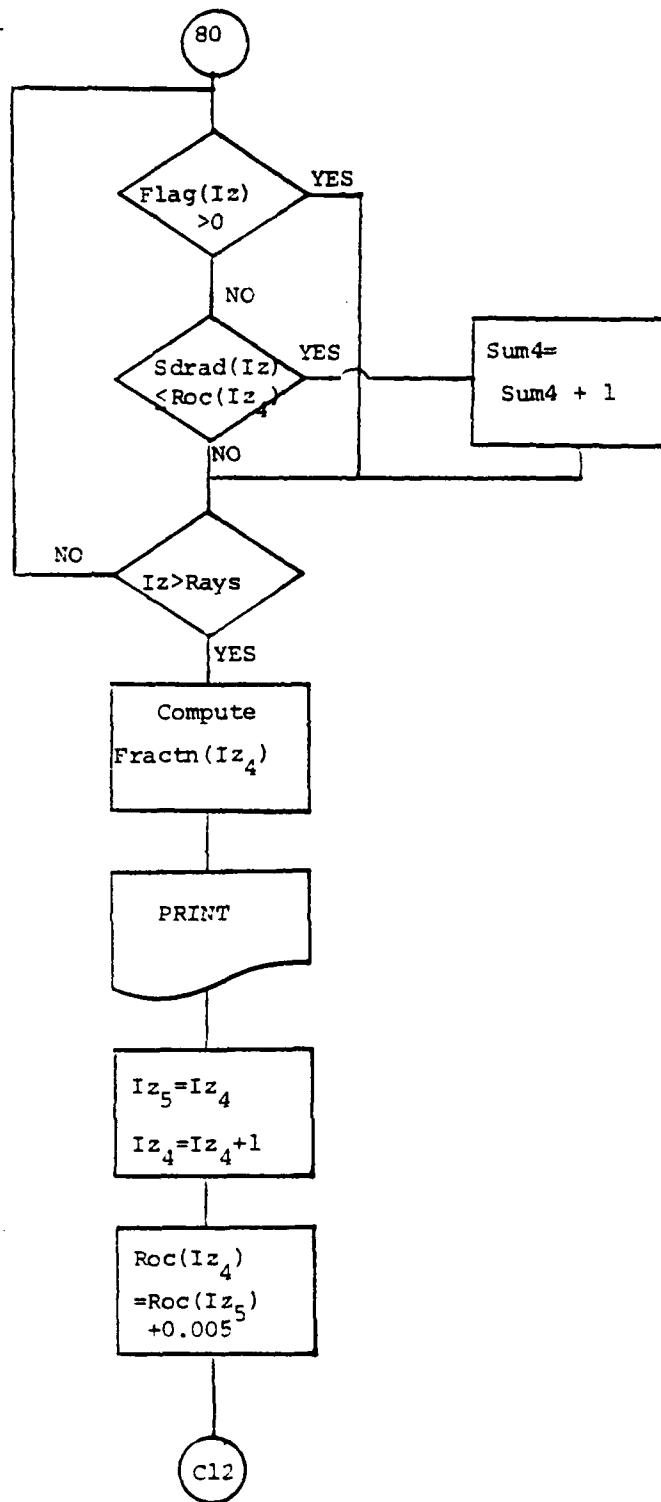


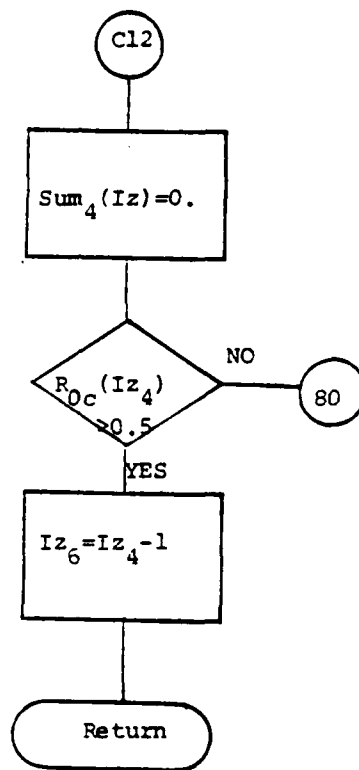


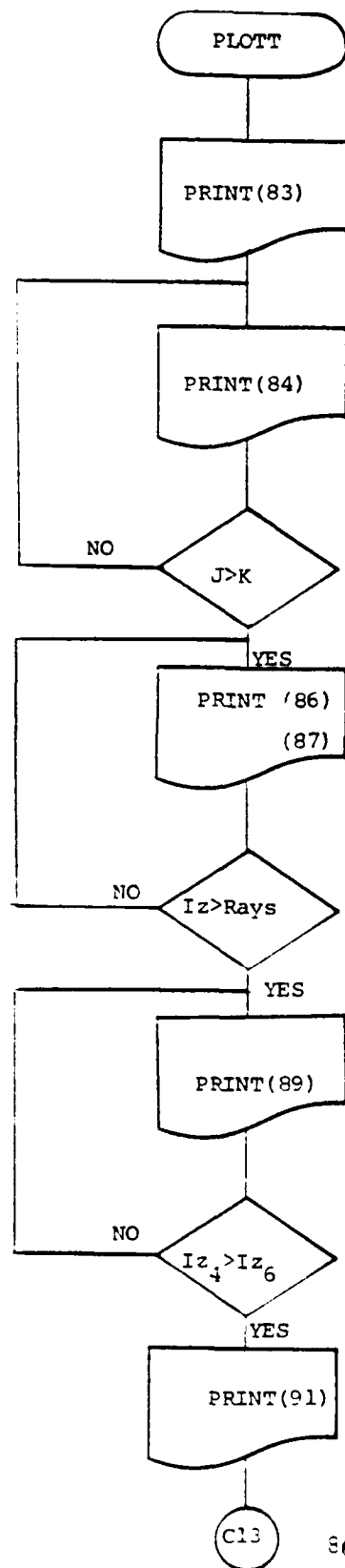


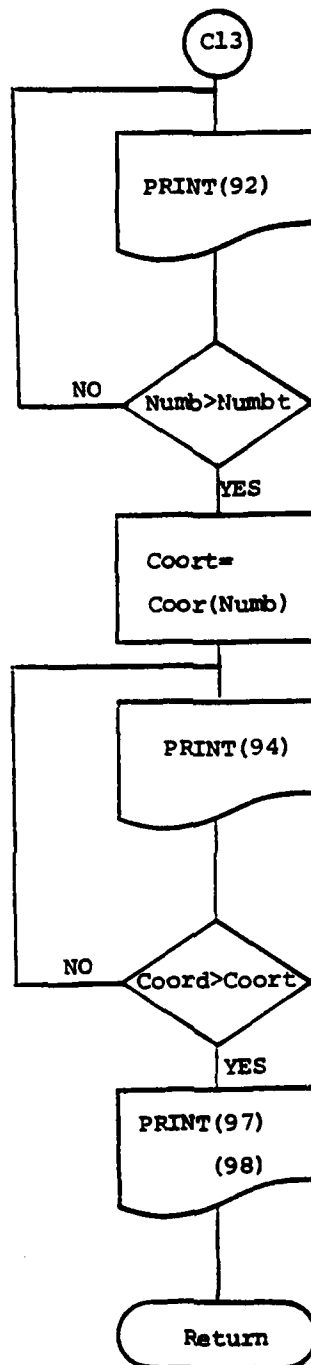










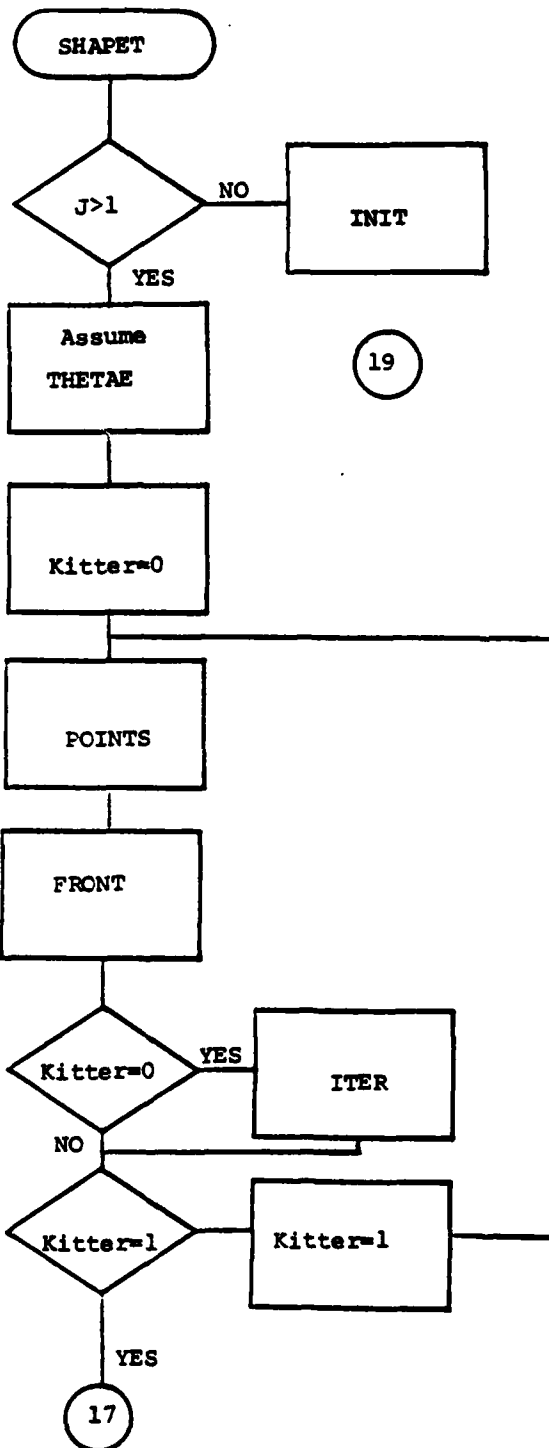


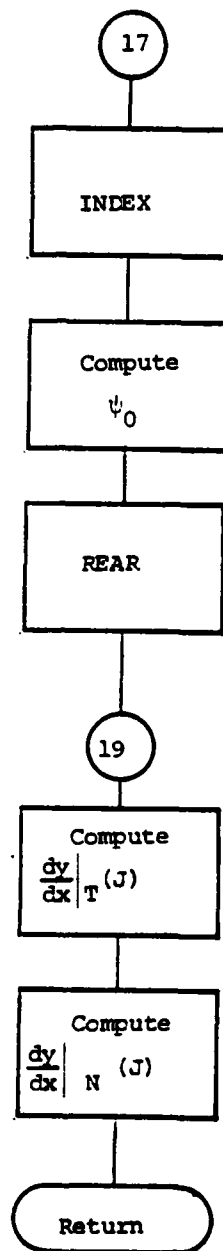
6. FLOW CHART OF PROGRAM GRIN

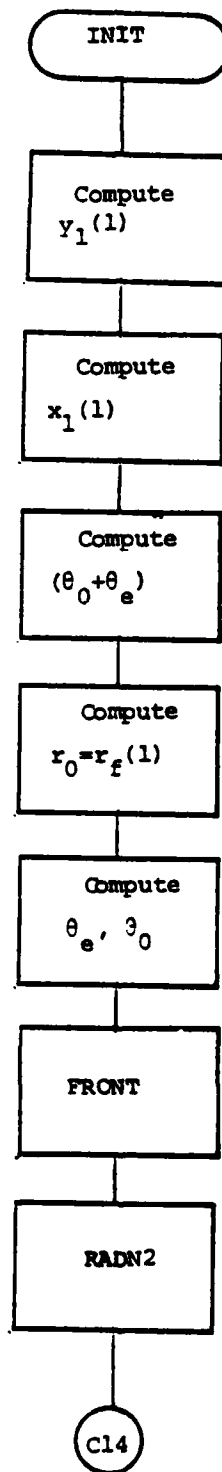
Note: Program GRIN is identical to program LENS (Section 5) except for subroutines:

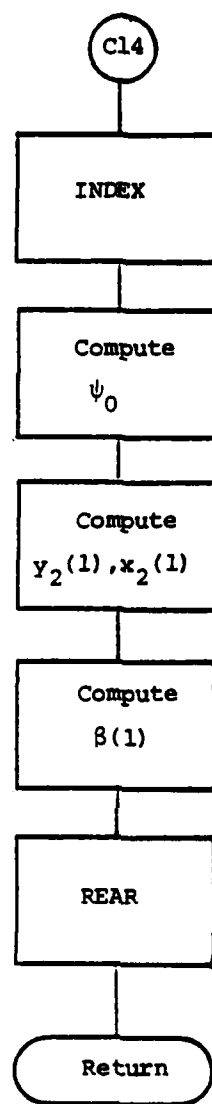
SHAPET, SKEWT, SHAPEC, SKEWC.

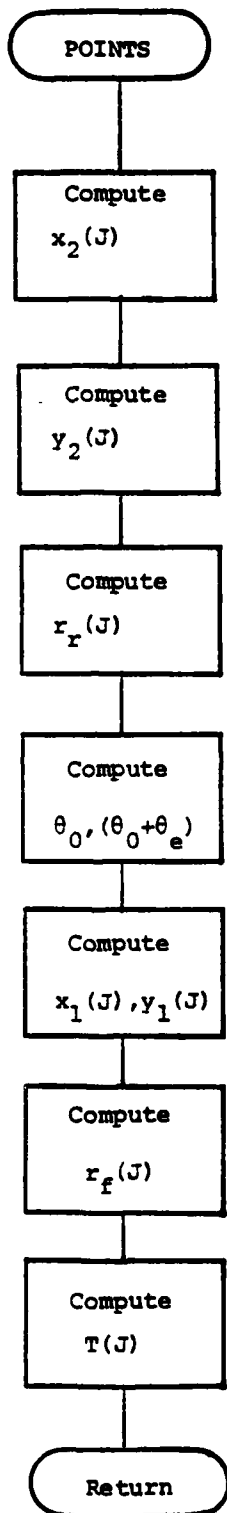
The flow chart for the first two is listed below. Subroutines SHAPEC, SKEWC are of a different design (fixed cone α_p for the rear surface). They are part of Captain Carr's thesis [15], and they will be described there.

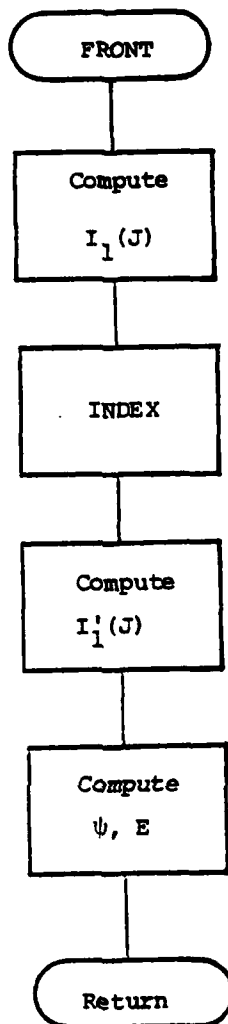


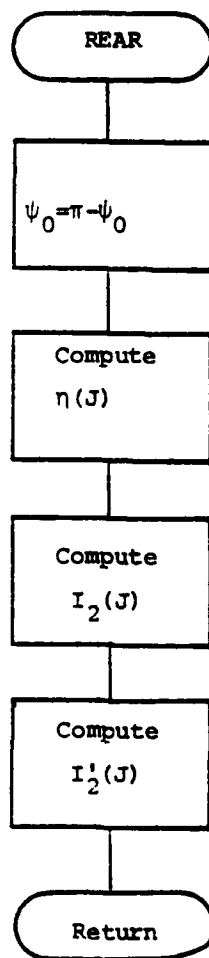


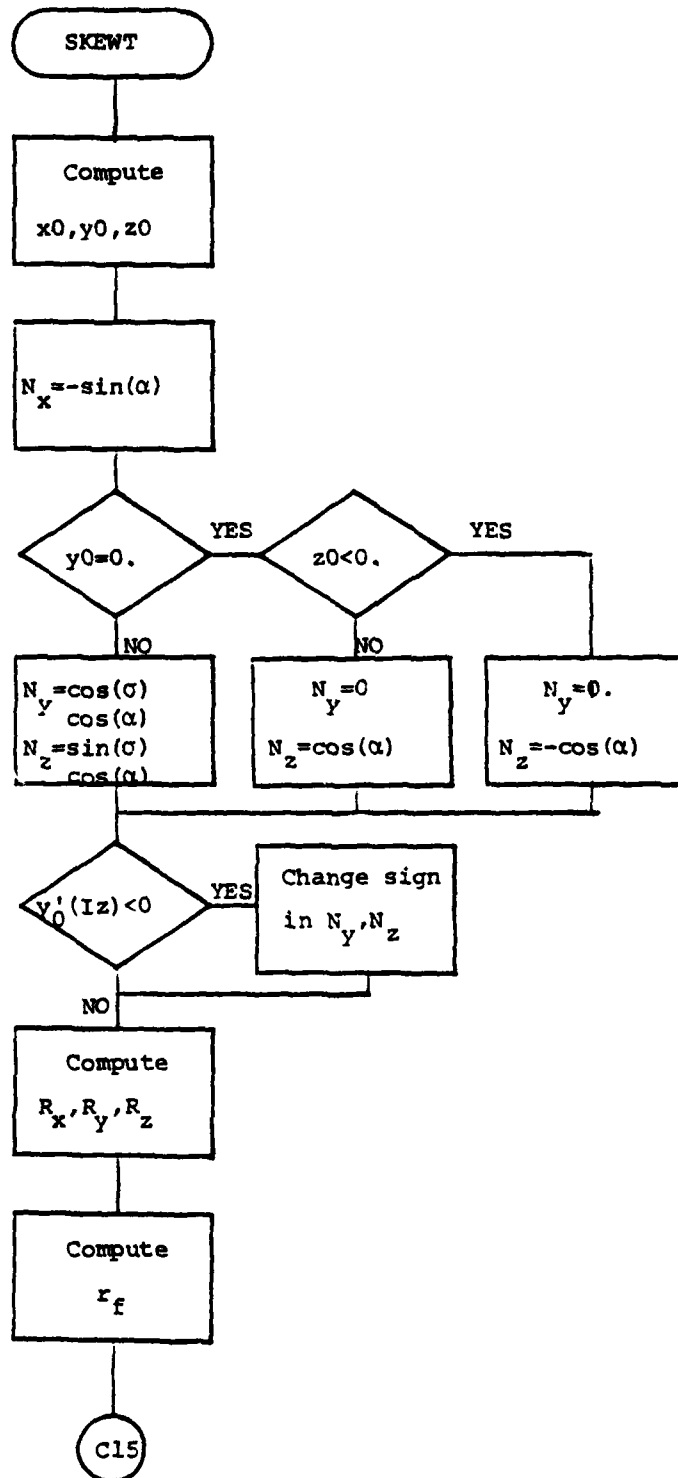


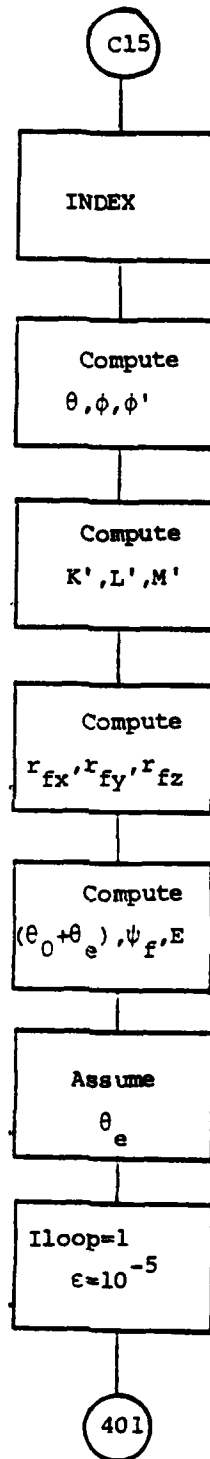


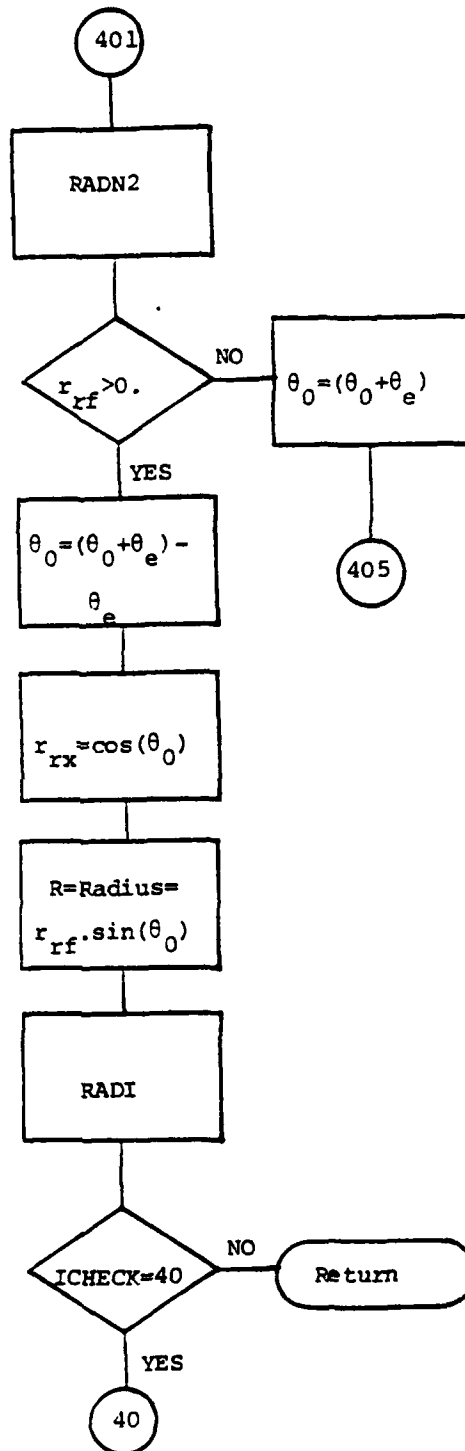


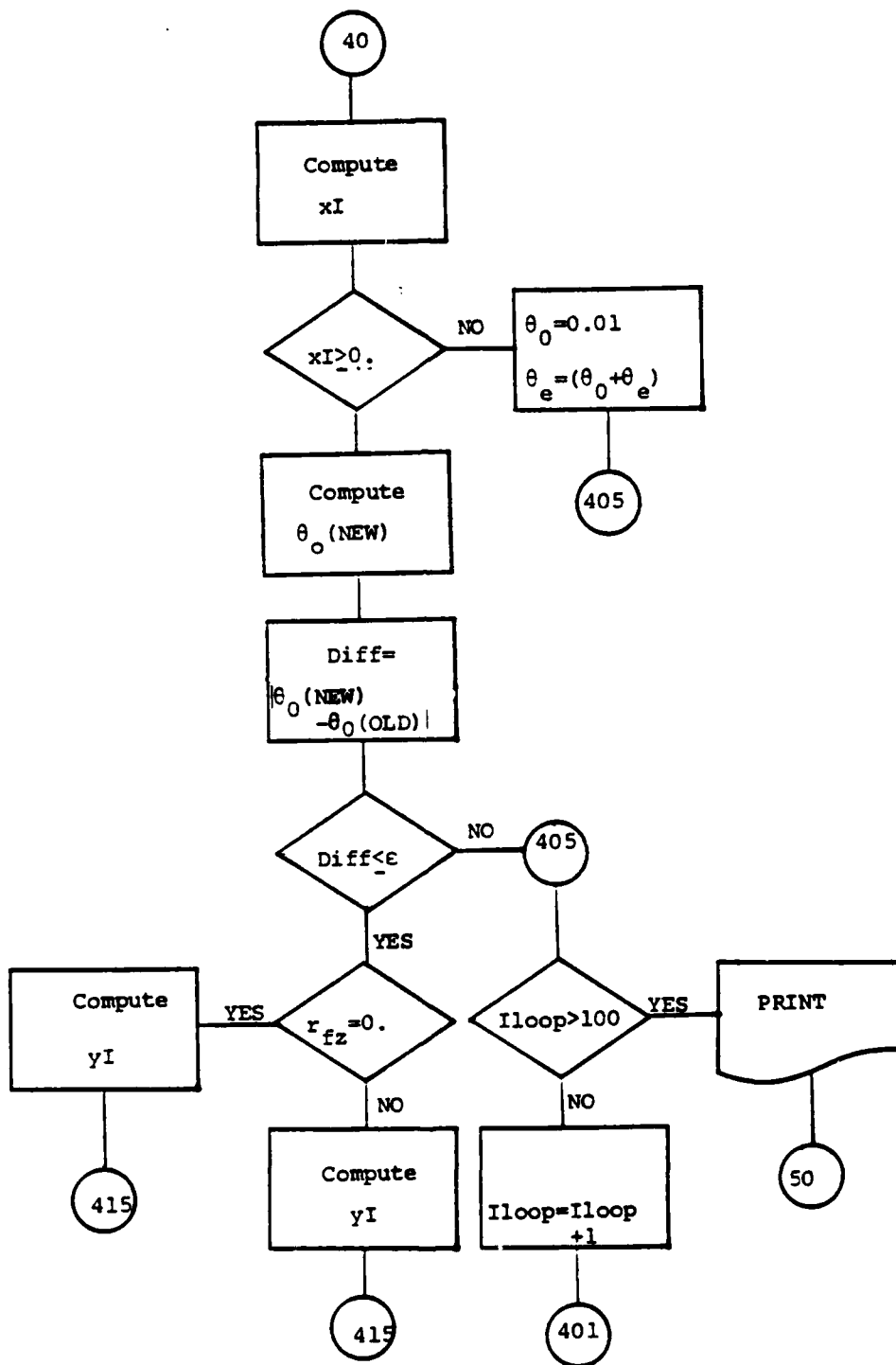


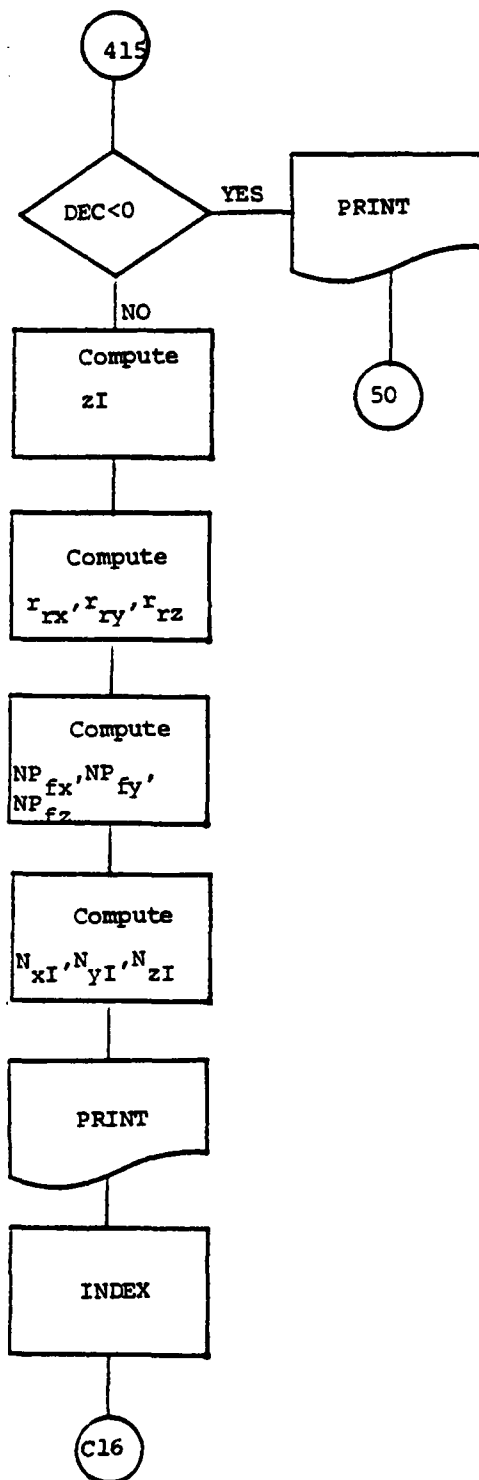


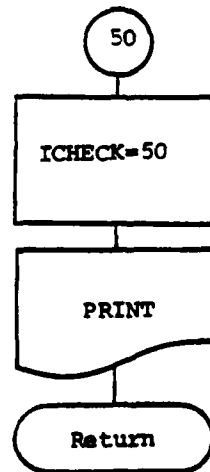
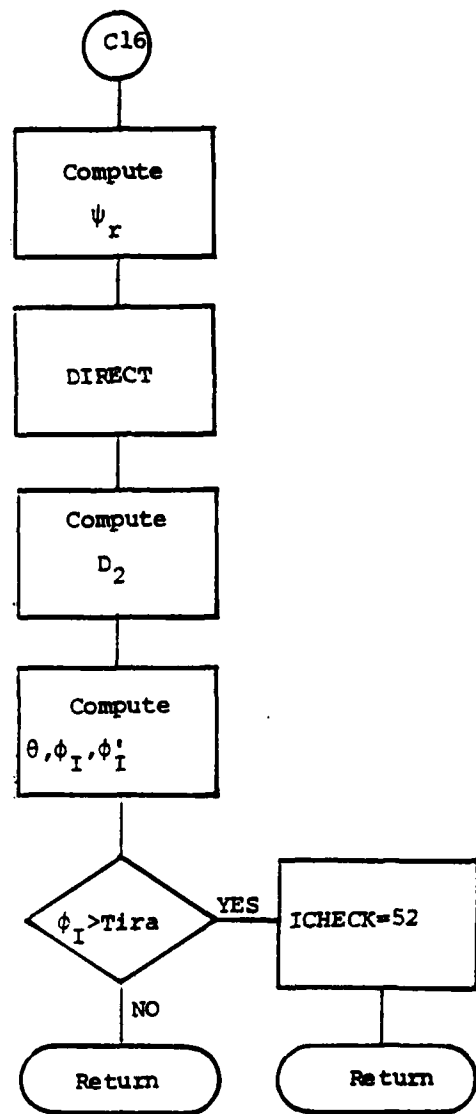


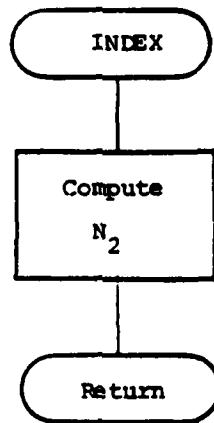


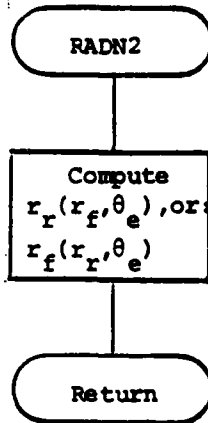


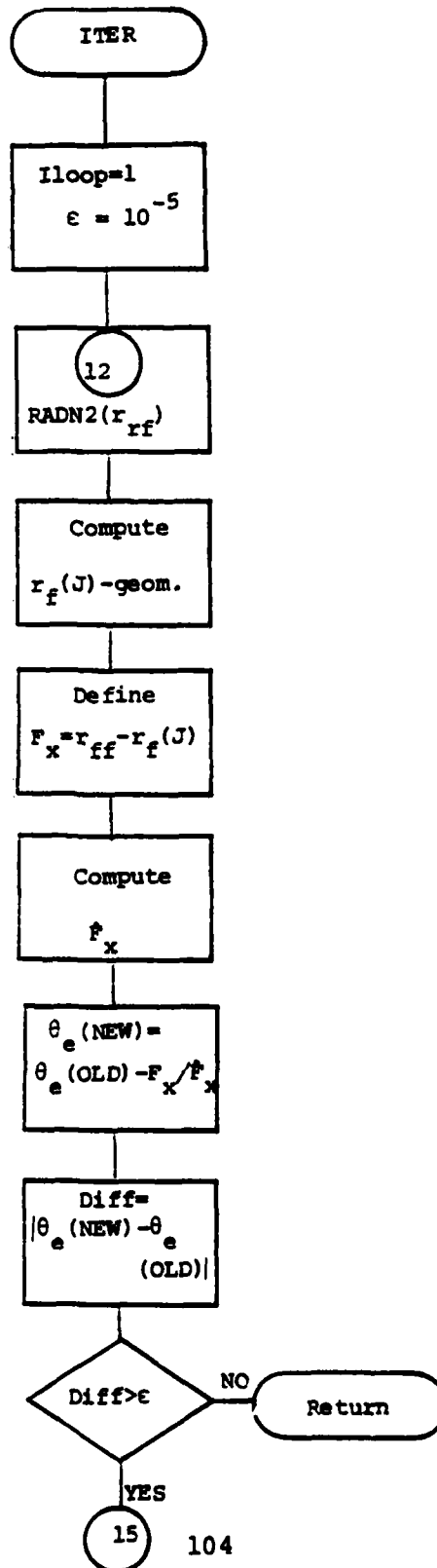


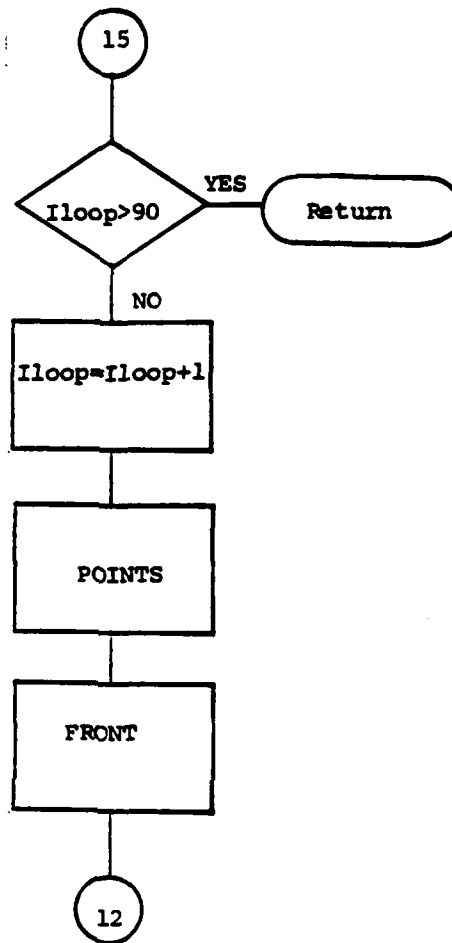


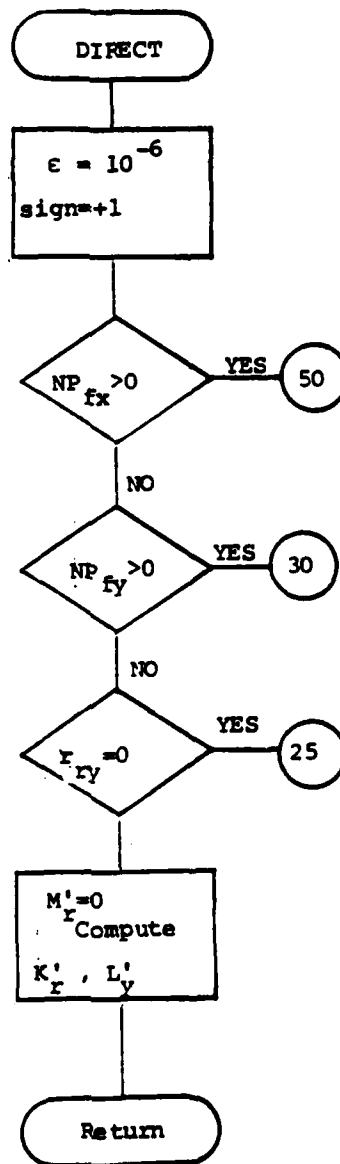


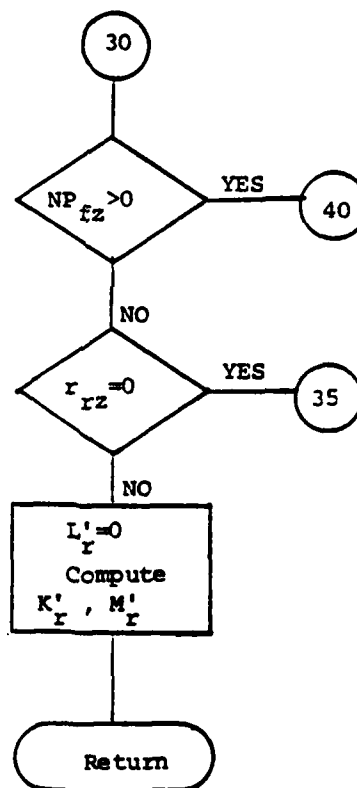
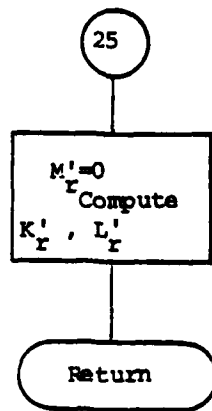


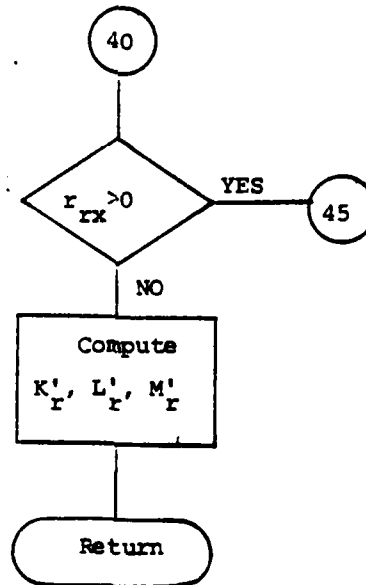
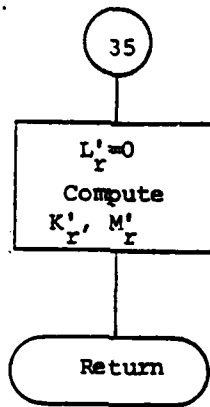


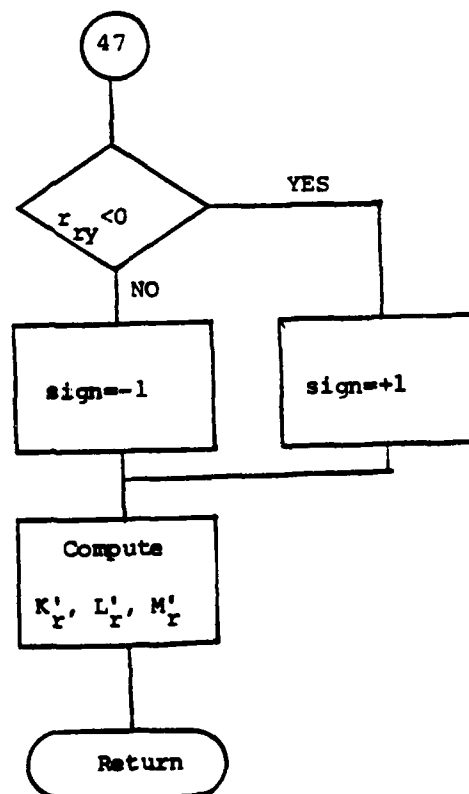
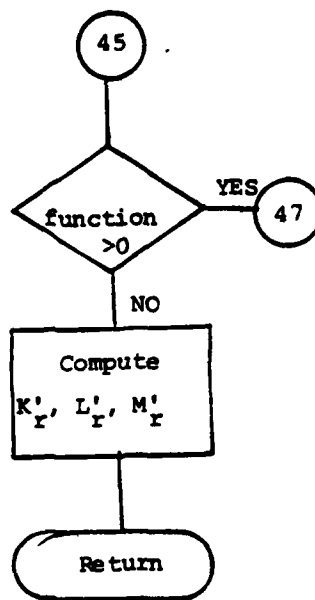


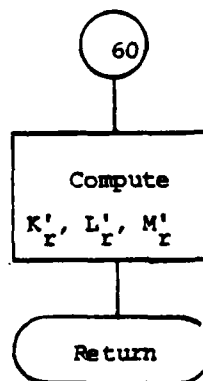
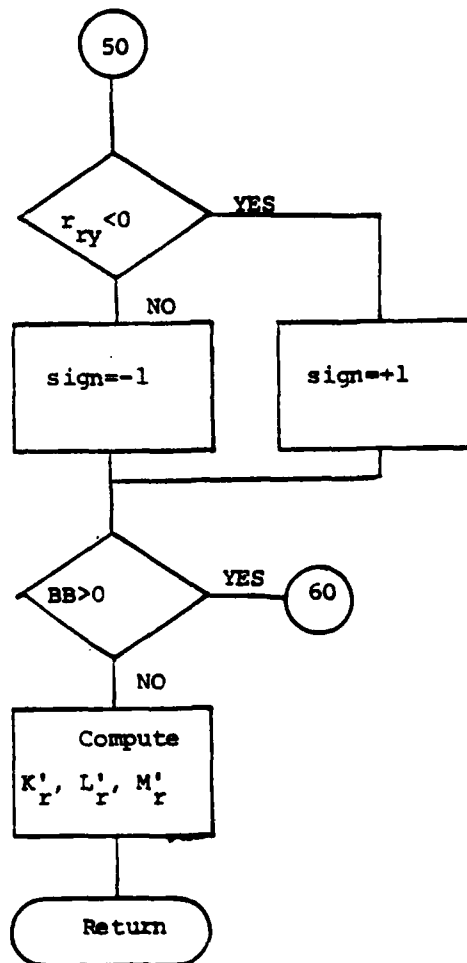












7. COMPUTER PROGRAMS USER'S GUIDE

7.1 Input Data

F, α , U, I_{case}

I, R, T(1)

N₁, N₂, N₃

α_p , Grid, Ellnum

X_C, Div

Shape, Squray, Ellips

7.2 Options

I_{case}=1 Rear surface is a fixed cone
(Capt. Carr's thesis, see ref. [15])

I_{case}=2 Front surface is a fixed cone
(This report).

7.3 Execution Commands

7.3.1 Opening Commands

LAXXXX (Write account no. instead of XXXX).

Password

GLOBAL TXTLIB FORTMOD2 MOD2EEH

7.3.2 Compilation

FORTGI LENS (or GRIN)

7.3.3 Run on Terminal (WORK⁽¹⁾)

FILEDEF 05 DISK DATA L

FILEDEF 06 DISK OUT D (RECFM F BLOCK 132 PERM

EXEC RUN LENS (or GRIN)

XEDIT OUT D

7.3.4 Hard Copy

FILE

PRINT OUT D

7.3.5 Get a Plot

LENSCOM PRINTER

7.3.6 Change in Plot Routine

XEDIT LENSLOT FORTRAN

7.3.7 Transfer Files to Another User

(a) The Transferer

CP SPOOL PUNCH CONT TO XXXXP⁽²⁾

PUNCH LENS FORTRAN⁽³⁾

(PUNCH GRIN FORTRAN⁽³⁾)

(PUNCH DATA L⁽³⁾)

CP SPOOL PUNCH CLOSE NOCONT

CP SPOOL PUNCH OFF

(b) The Receiver

READCARDA*Δ*

(c) Notes

(1) WORKG is the name of the file of the commands in this section.

(2) Account No. of the receiver.

(3) Optional.

8. COMPUTER PROGRAMS LIST OF SYMBOLS AND SUBROUTINES

8.1 Subroutines

DATTA	Initial data
SHAPET	Computes shape of lens in $I_{\text{case}}=2$
SHAPEC	Computes shape of lens in $I_{\text{case}}=1$
INIT	Computes behavior of first ray.
POINTS	Computes coordinates of rear and front surfaces.
FRONT	Computes $I_1(J)$, $I_1'(J)$, ψ , E at front surface.
REAR	Computes $n(J)$, $I_2(J)$, $I_2'(J)$ at rear surface.
CALTC	Computes thickness at each point for SHAPEC.
NOSE	Computes extrapolation of last points in $I_{\text{case}}=1$, or coordinates shift in $I_{\text{case}}=2$.
ZOYO	Computes $Z_0'(IZ)$, $y_0'(IZ)$ for skew rays calculation.
RADI	Computes intersection of the ray with the designed surface.
SKEWT	Skew rays calculation in $I_{\text{case}}=2$.
SKEWC	Skew rays calculation in $I_{\text{case}}=1$.
INTENS	Calculates transmitted intensity of the rays.
IMAGE	Calculates image plane spot diagram.
SUMM	Calculates spot diagram energy density.
PLOTT	Save output for plot routine.
INDEX	Computes index of refraction in the lens (N_2).
RADN2	Computes radius to rear (or front) surface from known radius to front (or rear) surface and θ_e .
ITER	Iteration routine to find correct θ_e in SHAPET.
DIRECT	Computes direction cosines of the ray at the rear surface.

8.2 Program Symbols

8.2.1 Data Symbols

F	Focal length.
α	The fixed surface cone half angle.
U	The incident ray offset angle.
I	Number of iterations.
R	Maximum radius of fixed surface cone.
T(l)	Thickness of lens at the edge.
N_1, N_2, N_3	Indices of refraction.
α_p	Inclination of object plane.
Grid	Size of grid increment.
Ellnum	Number of ellipses.
Ell	z - coordinate increment for ellipse plot.
X_C	Location of center symmetry in GRIN.
Div	The maximum change in the index of refraction (N_2)

8.2.2 Geometrical Symbols

$x_1(J), y_1(J)$	Coordinates on front surface.
$x_2(J), y_2(J)$	Coordinates on rear surface.
$r_f(J)$	Radius to front surface.
$r_r(J)$	Radius to rear surface.
XO, YO, ZO	Intercept of the ray with the front surface.
XI, YI, ZI	Intercept of the ray with the rear surface.
Y_{Im}, Z_{Im}	Intersection with the image plane.

8.2.3 Direction Cosines Symbols

N_x, N_y, N_z	Direction cosines of the front surface normal.
-----------------	--

N_{xI}, N_{yI}, N_{zI}	Direction cosines of the rear surface normal.
R_x, R_y, R_z	Direction of cosines of the ray.
K', L', M'	Direction cosines of the internal refracted ray.
r_{fx}, r_{fy}, r_{fz}	Direction cosines of the front radius.
$NP_{fx}, NP_{fy}, NP_{fz}$	Direction cosines of the normal to plane of the ray at front surface.
r_{rx}, r_{ry}, r_{rz}	Direction cosines of the rear radius.
K'', L'', M''	Direction cosines of the rear surface external refracted ray.

8.2.4 Angle Symbols

The angle symbols are defined in figures 3 and 8.

9. PROGRAM LENS - LISTING

[illegible]

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[illegible]

[illegible]

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C
2.ROCC(3001),SUM4(3000),FRACTIN(3001),SDRAD(119001),VCENTR(120,501)

INTEGER I,J,K,L,M,N,P,Q,R,S,T,U,V,W,X,Y,Z,NUM1,NUM2,NUM3,NUM4,NUM5,NUM6,NUM7,NUM8
REAL M1,M2,M3,M4,M5,M6,M7,M8,M9,M10,M11,M12,M13,M14,M15,M16,M17,M18,M19,M20
M21,M22,M23,M24,M25,M26,M27,M28,M29,M30,M31,M32,M33,M34,M35,M36,M37,M38,M39,M40
M41,M42,M43,M44,M45,M46,M47,M48,M49,M50,M51,M52,M53,M54,M55,M56,M57,M58,M59,M60
M61,M62,M63,M64,M65,M66,M67,M68,M69,M70,M71,M72,M73,M74,M75,M76,M77,M78,M79,M80
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M161,M162,M163,M164,M165,M166,M167,M168,M169,M170,M171,M172,M173,M174,M175,M176,M177,M178,M179,M180
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M201,M202,M203,M204,M205,M206,M207,M208,M209,M210,M211,M212,M213,M214,M215,M216,M217,M218,M219,M220
M221,M222,M223,M224,M225,M226,M227,M228,M229,M230,M231,M232,M233,M234,M235,M236,M237,M238,M239,M240
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M281,M282,M283,M284,M285,M286,M287,M288,M289,M290,M291,M292,M293,M294,M295,M296,M297,M298,M299,M300
M301,M302,M303,M304,M305,M306,M307,M308,M309,M310,M311,M312,M313,M314,M315,M316,M317,M318,M319,M320
M321,M322,M323,M324,M325,M326,M327,M328,M329,M330,M331,M332,M333,M334,M335,M336,M337,M338,M339,M340
M341,M342,M343,M344,M345,M346,M347,M348,M349,M350,M351,M352,M353,M354,M355,M356,M357,M358,M359,M360
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M1001,M1002,M1003,M1004,M1005,M1006,M1007,M1008,M1009,M1010,M101
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[illegible]

[illegible]

9.1 PLOT ROUTINES

[illegible]

FILE: LEASCOM EXEC A NAVAL POSTGRADUATE SCHOOL

PAGE 001

CCNIPCL F1RGA
C1F .61 EC .PRINTER ECCTO -PRINTER
C1F .61 EC .PLOTTER ECCTO -PLOTTER
C1YPT REFAIT. SPECIFY FINIFR OR PLOTTER.
C1YIT
-PRINTER ECCTO INUE
CNAME : LFASPLCT
ECCTO -C
-PLOTTER ECCTO INUE
CNAME : LNSGRF
-C
ECCTO INUE
COPY FILE NAME FRTIRAN A FILE FINIFR A PLOT FORTIRAN A (REPLACE
EXEC STEPIT PLOT FORTIRAN

10. PROGRAM GRIN - LISTING

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FILE: GRIN FURTH A NAVAL POSTGRADUATE SCHOOL

[illegible]

[illegible]

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COMMON/JN/ANZ,ENZ,XC,DIV,E,THEAE,RJ
COMMON/GN/PR1,10,10,REF1,10,1,THEY,1,OTE,PSI,PSIO
COMMON/RA/R1,R2,R3
REAL N1,R2,R3
1,RX,NV,K1,RX,RY,RZ,NXI,NVI,NZI,PHI1,PHI2,TIRA
C
11 CCP=1
EPS1=1.E-05
IF(J.EU,1)EPS1=-1.0
12 CALL RADZ2(RF,R1,R2)
13 CALL RADZ2(RF,R1,R2)
14 CALL RADZ2(RF,R1,R2)
15 CALL RADZ2(RF,R1,R2)
16 CALL RADZ2(RF,R1,R2)
17 CALL RADZ2(RF,R1,R2)
18 CALL RADZ2(RF,R1,R2)
19 CALL RADZ2(RF,R1,R2)
20 CALL RADZ2(RF,R1,R2)
21 CALL RADZ2(RF,R1,R2)
22 CALL RADZ2(RF,R1,R2)
23 CALL RADZ2(RF,R1,R2)
24 CALL RADZ2(RF,R1,R2)
25 CALL RADZ2(RF,R1,R2)
26 CALL RADZ2(RF,R1,R2)
27 CALL RADZ2(RF,R1,R2)
28 CALL RADZ2(RF,R1,R2)
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98 CALL RADZ2(RF,R1,R2)
99 CALL RADZ2(RF,R1,R2)
100 CALL RADZ2(RF,R1,R2)

```

```
45 IF (ABS(IPRY-NPFY/NPFZ*RRZ)).GT.EPSIGD TO 47
    RETURN
    CKP=SIGN(SQRT(1.0-CKP**2)/(1.0*(NPFY/NPFZ)**2))
    CLP=NPFY/NPFZ*CLP
    RETURN
47 SIGN=-1.0
    IF (IPRY-LT.0.0) SIGN=+1.0
    APP=(IPRY-NPFY/NPFZ*RRZ)/(RRX**2+1.0)*(NPFY/NPFZ)**2
    BPP=2.0*(COS(PSIR)/(RRX**2)*(IPRY-NPFY/NPFZ*RRZ)
    CFP=(COS(PSIR)/(RRX**2-1.0)
    CLP=BPP/(2.0*(APP)+SIGN(SQRT(BPP**2-4.0*(APP*CFP)/(2.0*(APP)
    CKP=(NPFY/NPFZ*CLP
    CKP=(COS(PSIR)-(IPRY-NPFY/NPFZ*RRZ)*(CLP)/RPX
    RETURN
50 SIGN=-1.0
    IF (IPRY-LT.0.0) SIGN=+1.0
    AA=NPFY*IPRY-NPFY*RRX
    BB=NPFY*RRZ-NPFZ*RRX
    CC=NPFY*CCF(PSIR)
    IF (ABS(CF(PSIR)).GT.EPSIGD TO 60
    CLP=CC/AA
    BPP=(NPFY/NPFZ*APP**2+1.0)*CLP**2-1.0
    CFP=(NPFY/NPFZ*APP**2+1.0)*CLP**2-1.0
    CKP=-EP/APP+SIGN(SQRT(BPP**2-APP*CFP)/APP
    CKP=1-APP*CLF-NPFZ*CFP)/NPFY
    RETURN
60 AF=(NPFY/NPFZ)*2+1.0
    BP=(NPFZ/NPFX)*2+1.0
    CP=2.0*(AF*NPFF/NPFZ/NPFX**2
    APP=AB+NF+IAA/PAI**2-CP*AA/BB
    BPP=2.0*(AA*CC*PP/RR**2-CP*CC/RR
    CFP=BB*(CC/BB)**2-1.0
    CLP=BPP/(2.0*(APP)+SIGN(SQRT(BPP**2-4.0*(APP*CFP)/(2.0*(APP)
    CKP=CC/BB-AA/BB*CLP
    CKP=1-APP*CLP-NPFZ*CFP)/NPFY
    RETURN
END
```

GR11 3970
GR11 3980
GR11 3990
GR11 4000
GR11 4010
GR11 4020
GR11 4030
GR11 4040
GR11 4050
GR11 4060
GR11 4070
GR11 4080
GR11 4090
GR11 4100
GR11 4110
GR11 4120
GR11 4130
GR11 4140
GR11 4150
GR11 4160
GR11 4170
GR11 4180
GR11 4190
GR11 4200
GR11 4210
GR11 4220
GR11 4230
GR11 4240
GR11 4250
GR11 4260
GR11 4270
GR11 4280
GR11 4290
GR11 4300
GR11 4310
GR11 4320
GR11 4330
GR11 4340
GR11 4350

11. PRELIMINARY RESULTS

Table 1. Comparison of RMS Spot size for a homogeneous lens with the RMS Spot size for a GRIN lens.

α_p \ DIV	0	+0.05	-0.05
0.	0.0057336	0.0069021	0.005286
0.1	0.027424	0.027646	0.027327
0.2	0.06277	0.06288	0.06304
0.3	0.113431	0.11216	0.113245
0.4	0.18265	0.18287	0.18277

Note: DIV is the fractional variation of refractive index. α_p is the angle of incoming parallel rays relative to lens axis; α_p has dimensions of radians. The center of symmetry X_C was at -0.07 measured from the apex of the outer surface. The minus sign indicates that X_C is external to lens.

RESULTS FROM LENS

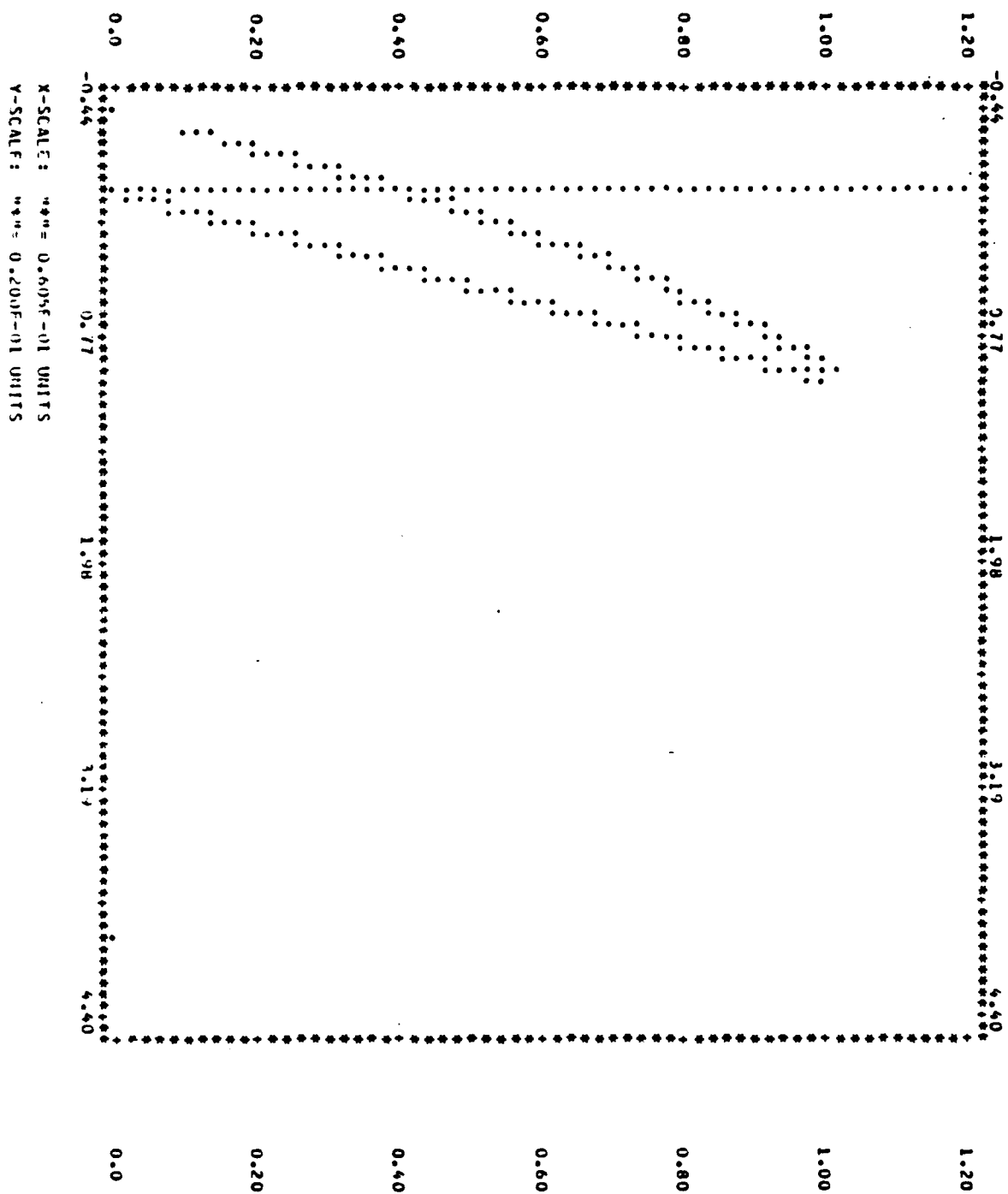
(ICASE = 1)

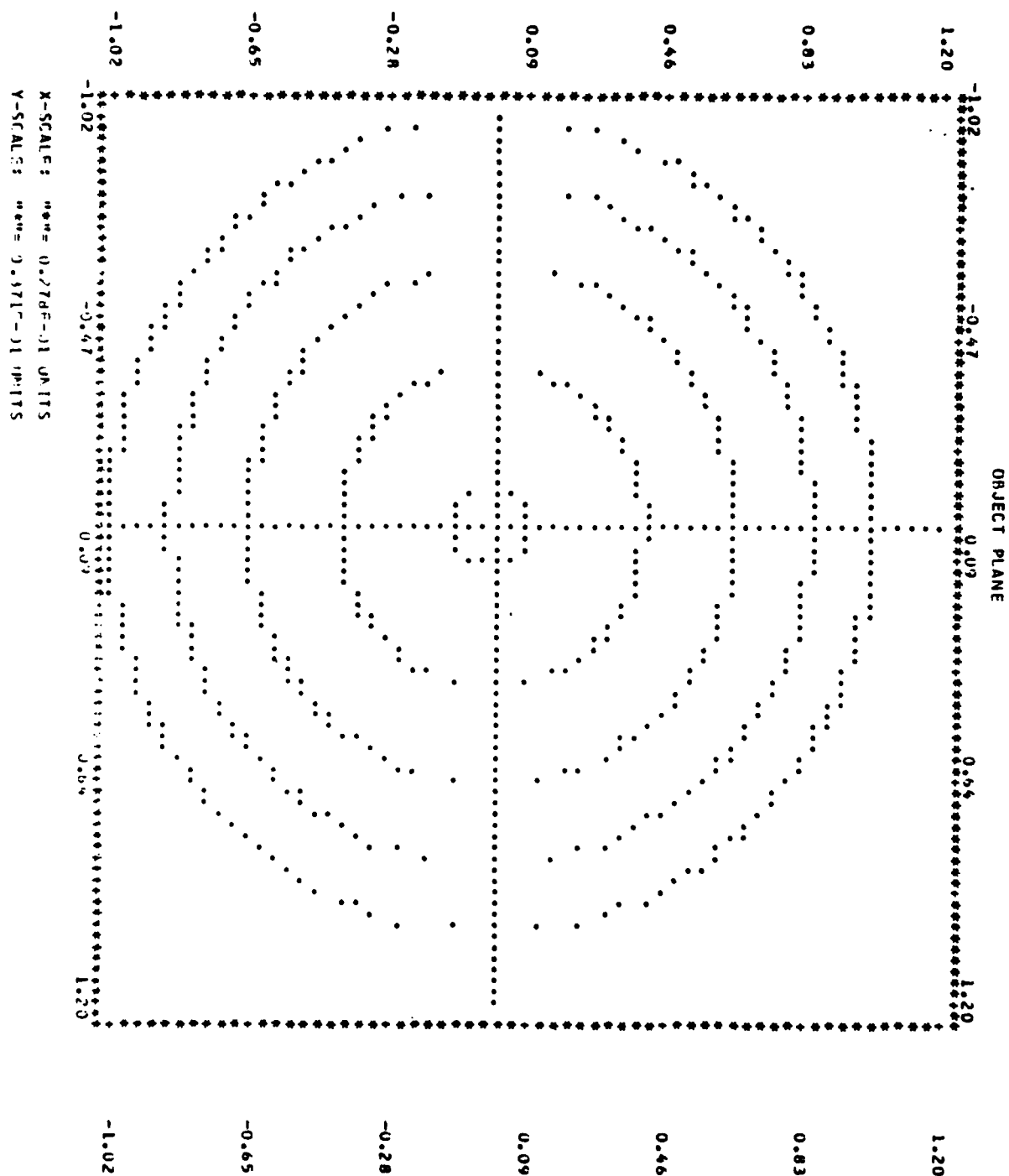
Input: $\alpha_p = 0.0, 0.2, 0.4$

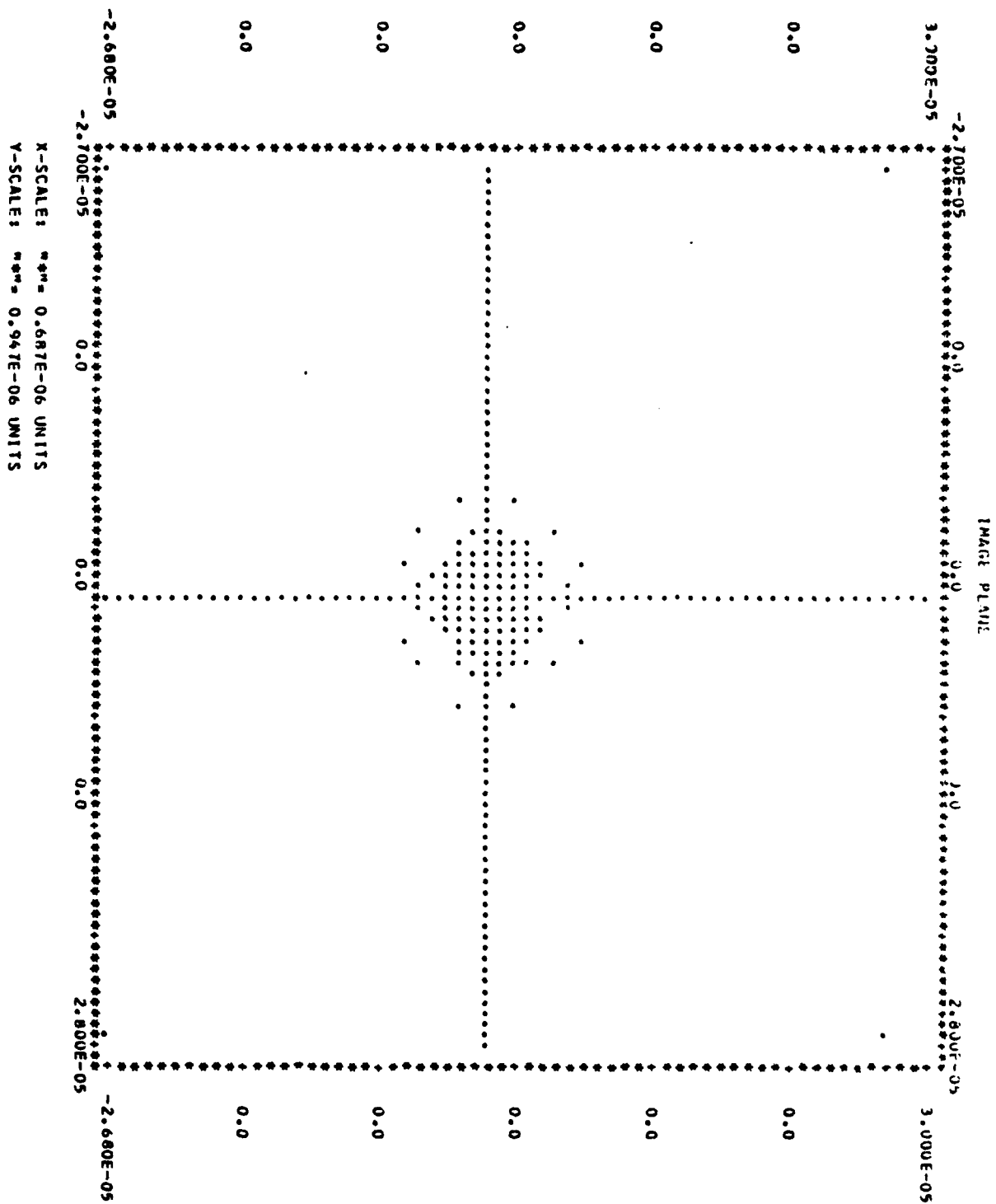
SUMMARY OF RESULTS

FOCAL LENGTH = 4.0000000 ALPHA = 0.7853979 U = 0.0 I = 1008
R = 1.0000000 T = 0.0500000 INDICES OF REFRACTION ARE: N1 = 1.0000000 N2 = 1.5000000 N3 = 1.0000000
ALFAP = 0.0 GRID = 0.1000000 STATNA = -0.44171 GAMMA = 0.7850314 XC=0.0 DIV=0.0
RAVS = 328 COUNT = 328 YCENTR = 0.0 SIGMAV = 0.0 SIGMAZ = 0.0
RMSRAD = 0.0000052

GLM LENS SHAPE



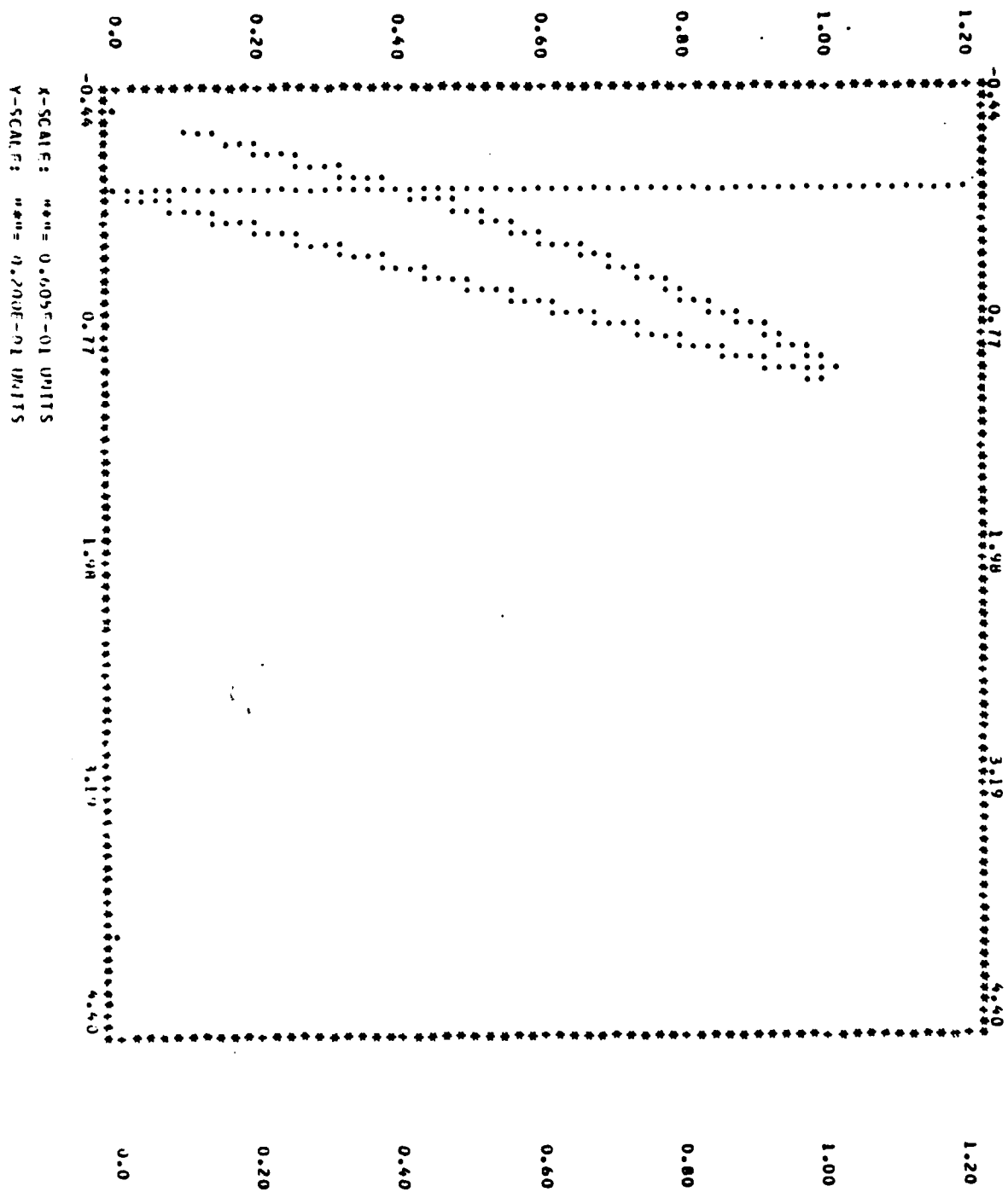


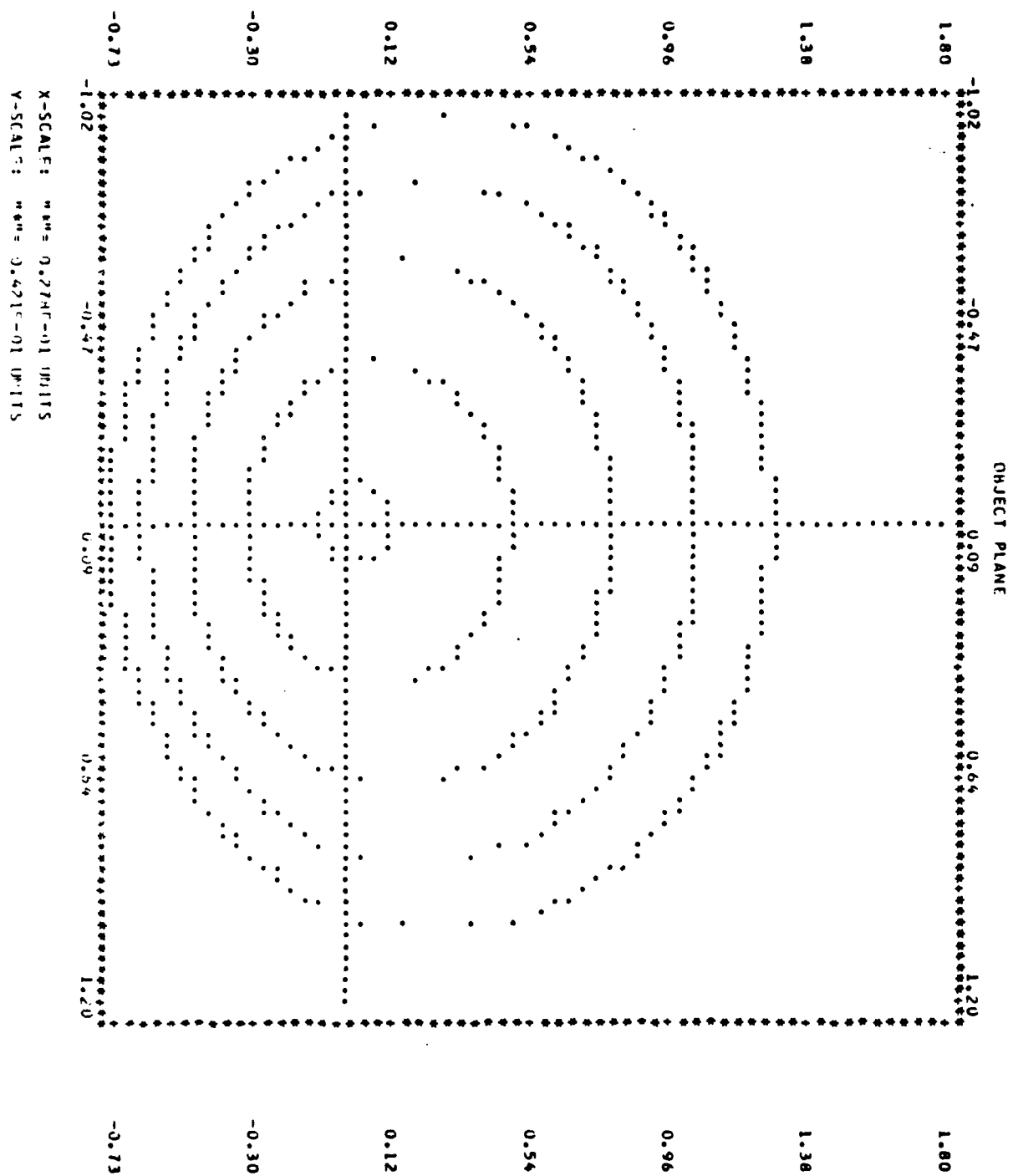


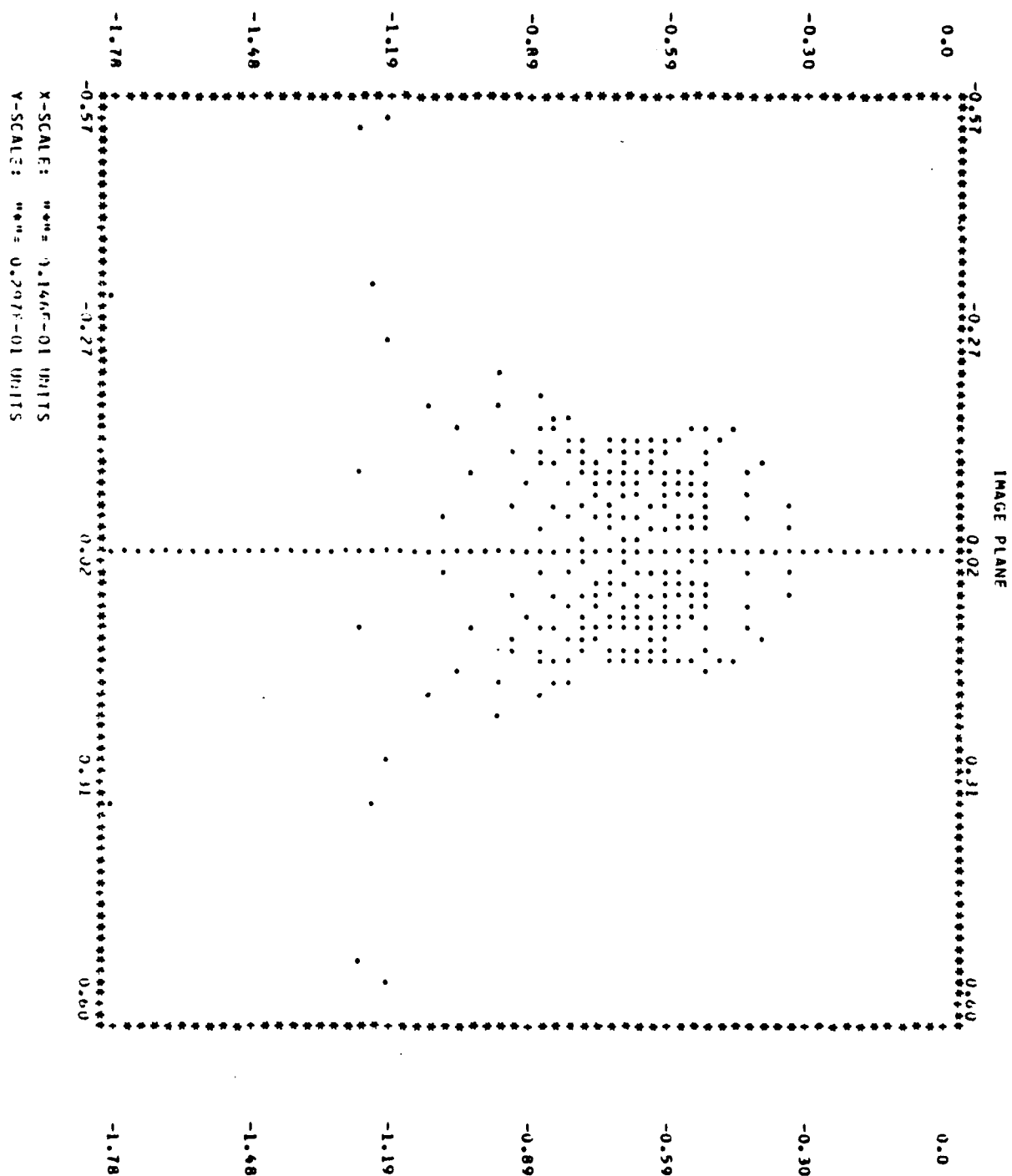
SUMMARY OF RESULTS

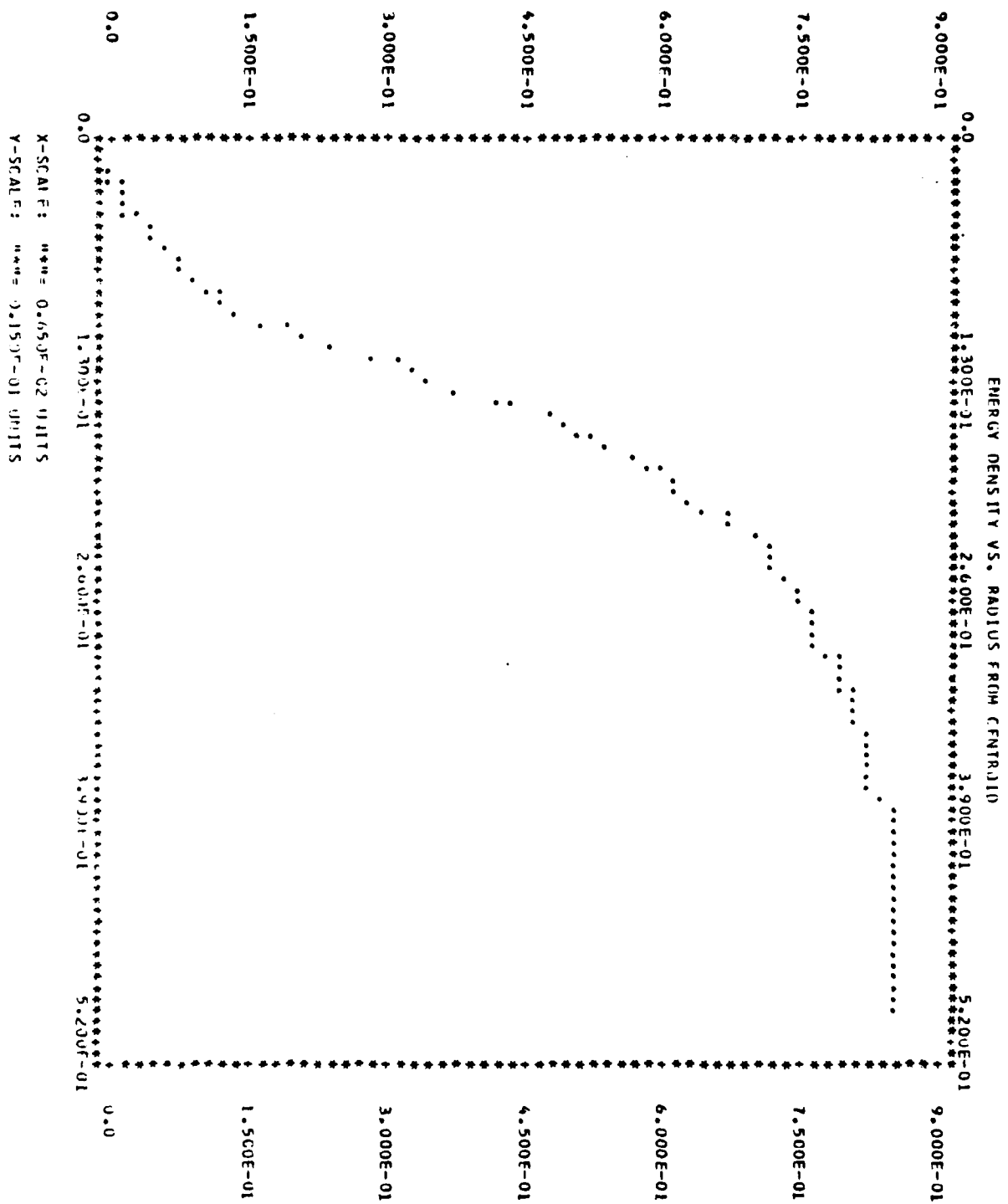
FOCAL LENGTH = 4.0000000 ALPHA = 0.7853979 U = 0.0 I = 100R
R = 1.0000000 T = 0.0500000 INDICES OF REFRACTION ARE: N1 = 1.0000000 N2 = 1.5000000 N3 = 1.0000000
ALFAP = 0.2000000 GRID = 0.1000000 STATNA = -0.44171 GAMMA = 0.7850314 XC=0.0 DIV=0.0
RAVS = 320 COUNT = 286 YCENTR = -0.6992106 SIGMAY = 0.0386393 SIGMAZ = 0.0164104
PMSRAD = 0.2346267

CIM LENS SHAPE



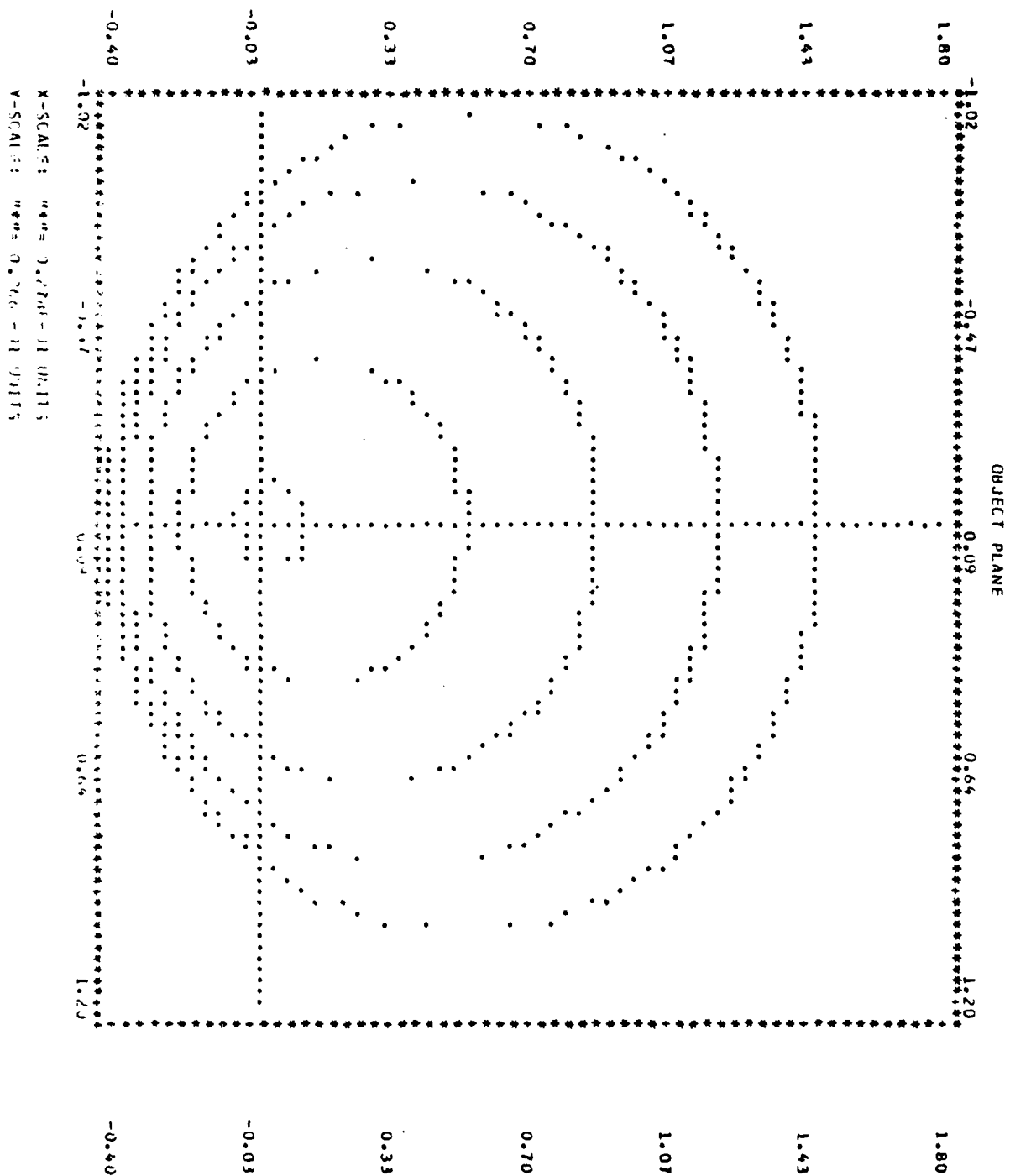


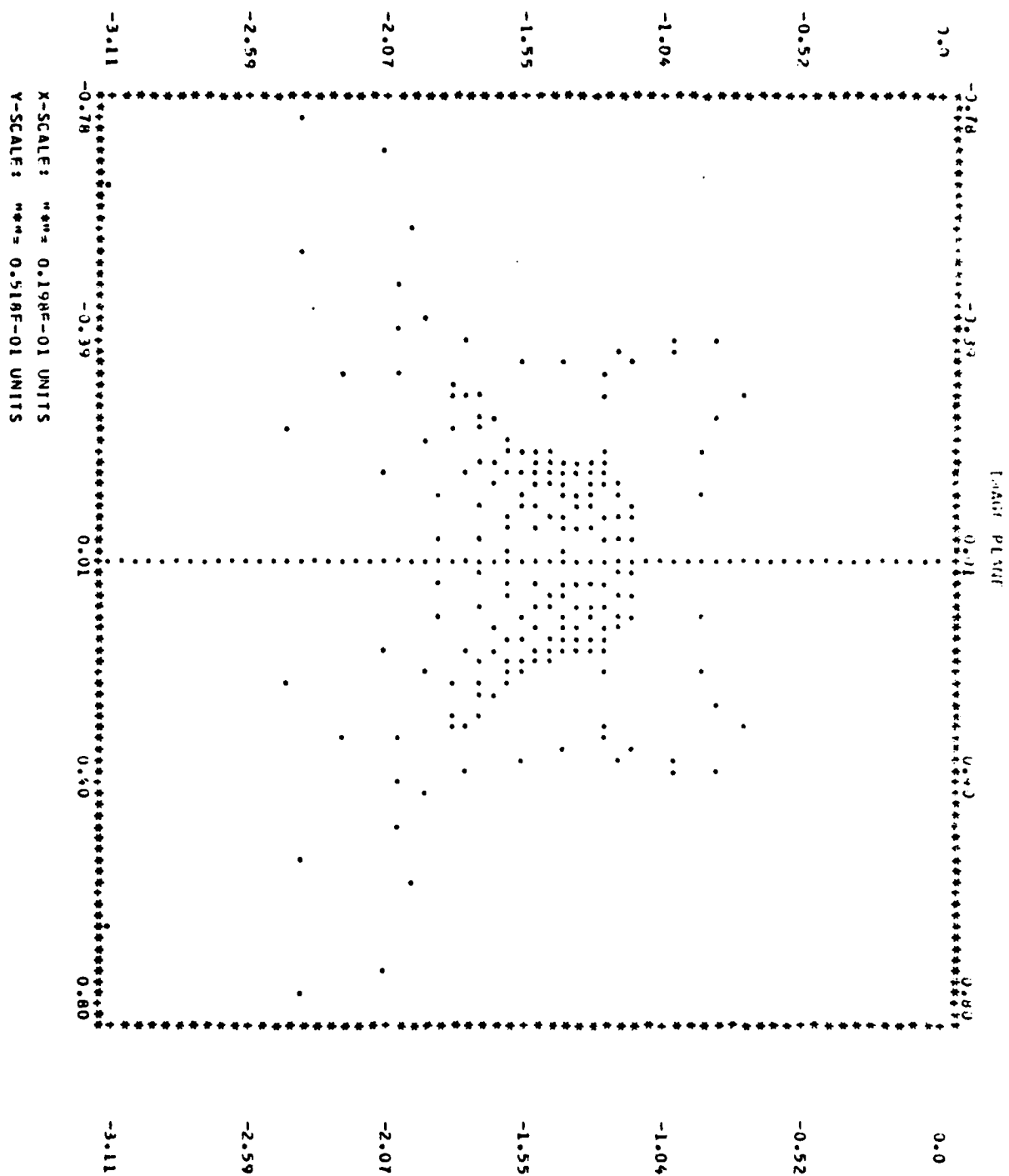




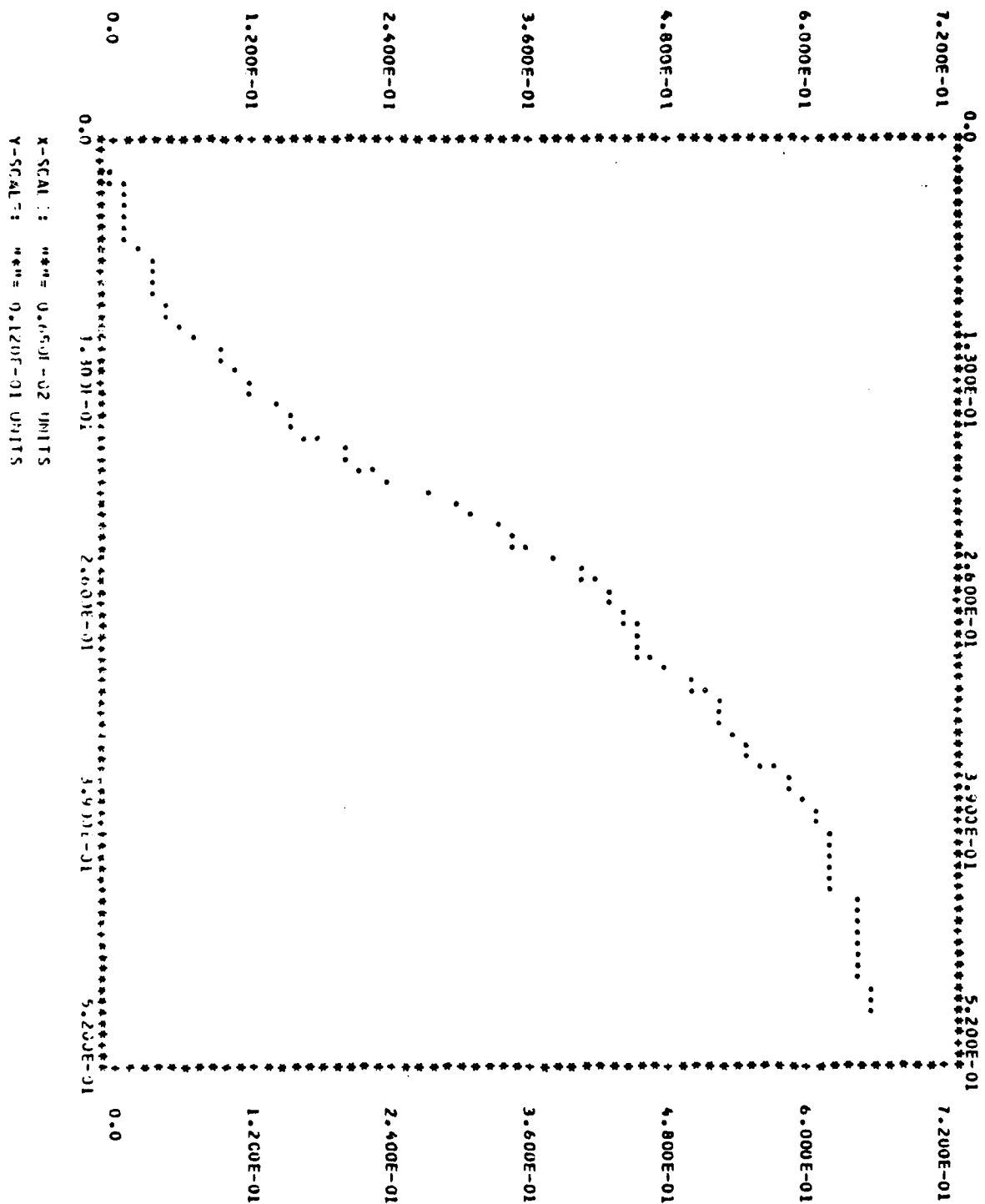
SUMMARY OF RESULTS

FOCAL LENGTH = 4.0000000 ALPHA = 0.7853979 U = 0.0 I = 1008
 R = 1.0000000 T = 0.0500000 INDICES OF REFRACTION ARE: N1 = 1.0000000 N2 = 1.5000000 N3 = 1.0000000
 ALFAP = 0.4000000 GRID = 0.1000000 STAINA = -0.44171 GAMMA = 0.7850314 XC=0.0 DIV=0.0
 RAYS = 302 COUNT = 241 VCENTR = -1.4999914 SIGMAV = 0.1186211 SIGMAZ = 0.0549298
 RMSRAD = 0.4165944





ENERGY DENSITY VS. RADIUS FROM CENTROID



RESULTS FROM GRIN

(ICASE = 2)

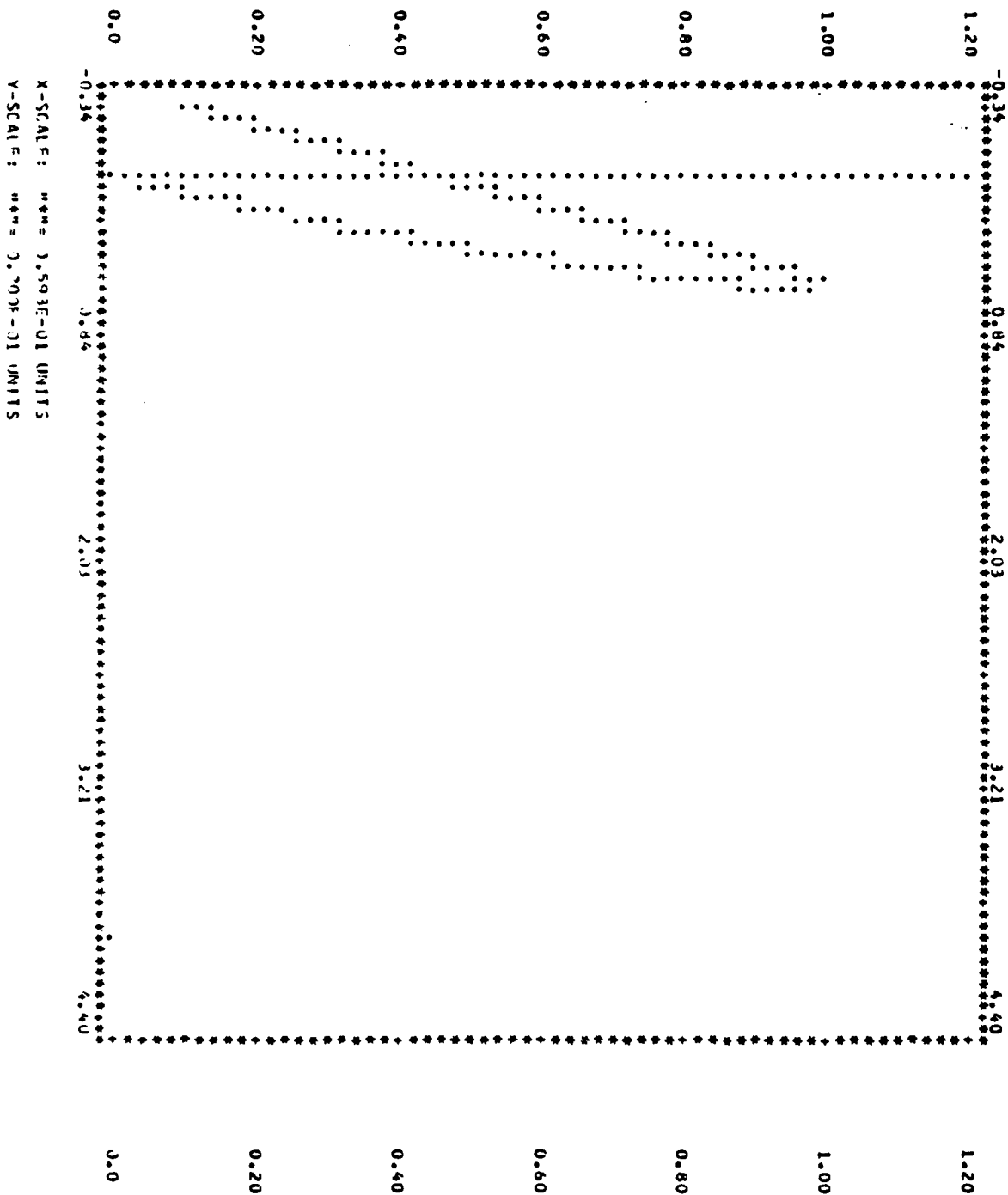
Input: $x_c = -0.07$, DIV = +0.05

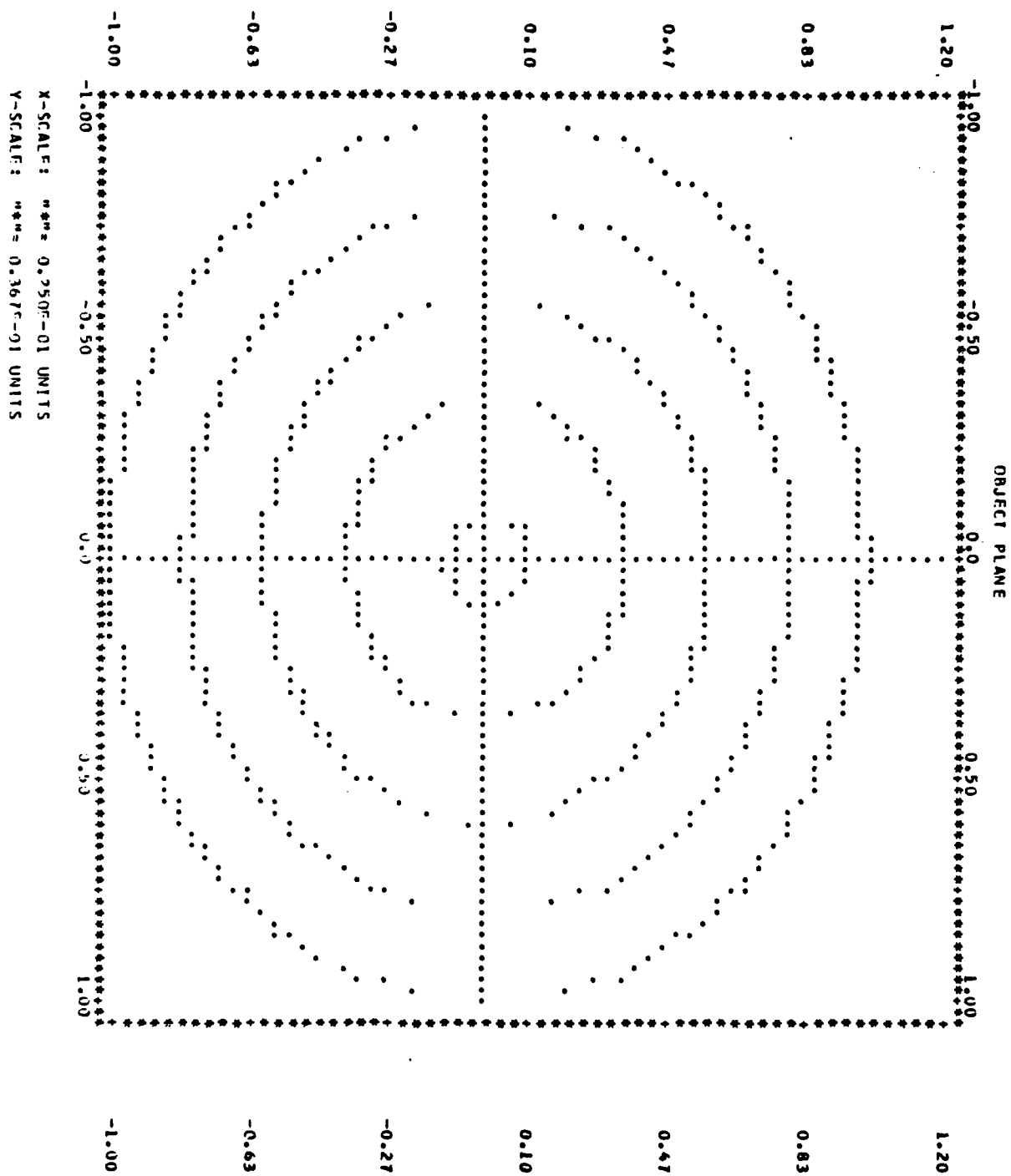
$\alpha_p = 0.0, \quad 0.1$

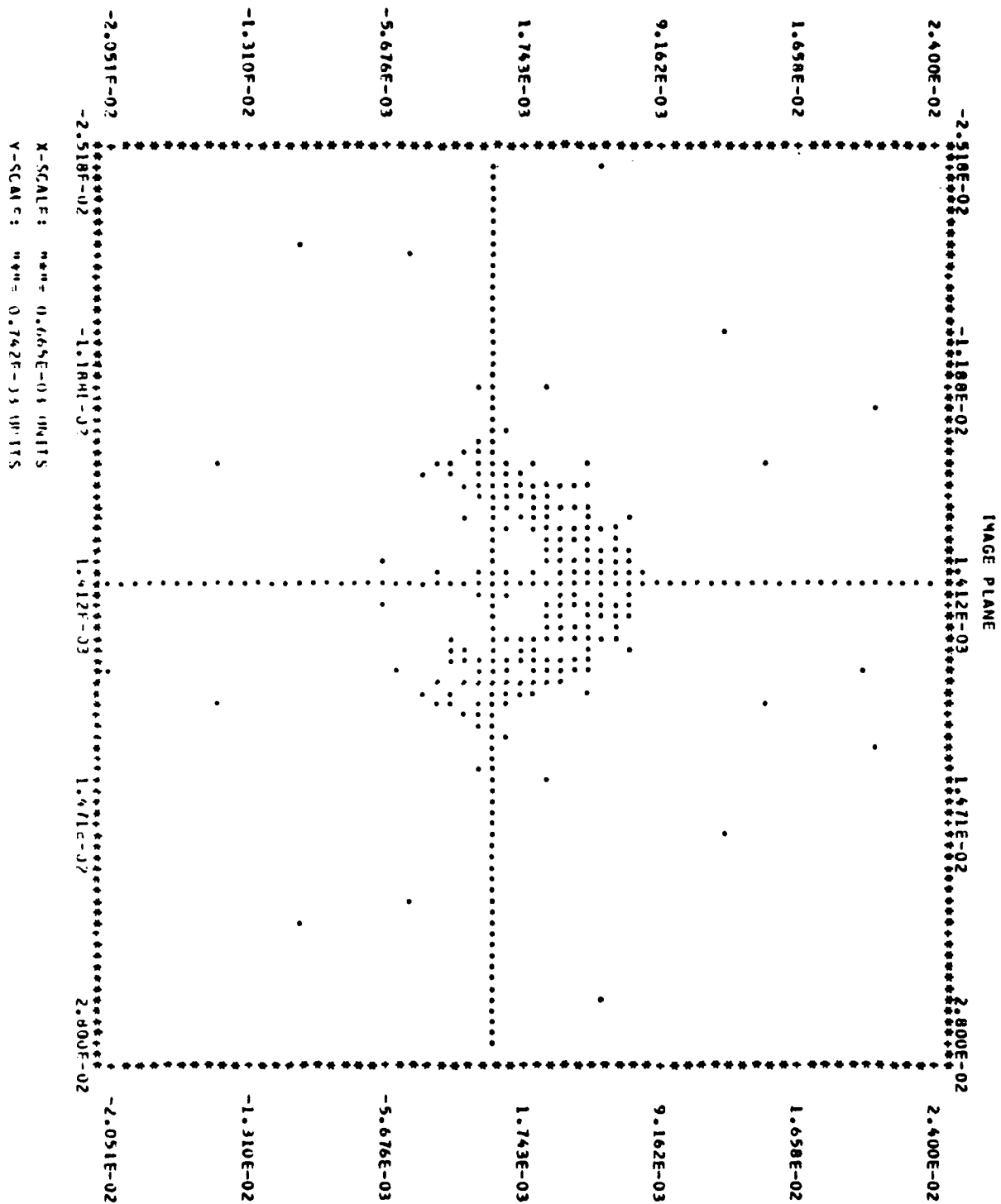
SUMMARY OF RESULTS

FOCAL LENGTH = 4.0000000 ALPHA = 0.7853979 U = 0.0 I = 1008
 R = 1.0000000 T = 0.0500000 INDICES OF REFRACTION ARE: N1 = 1.0000000 N2 = 1.5757046 N3 = 1.0000000
 ALFAP = 0.0 GRID = 0.1000000 STATNA = 0.0 GAMMA = 0.0 XC = -0.51737 DIV = 0.05000
 RAYS = 310 COUNT = 310 VCENR = 0.0030477 SIGMA = 0.0000180 SIGMAZ = 0.0000297
 RMSRAD = 0.0069021

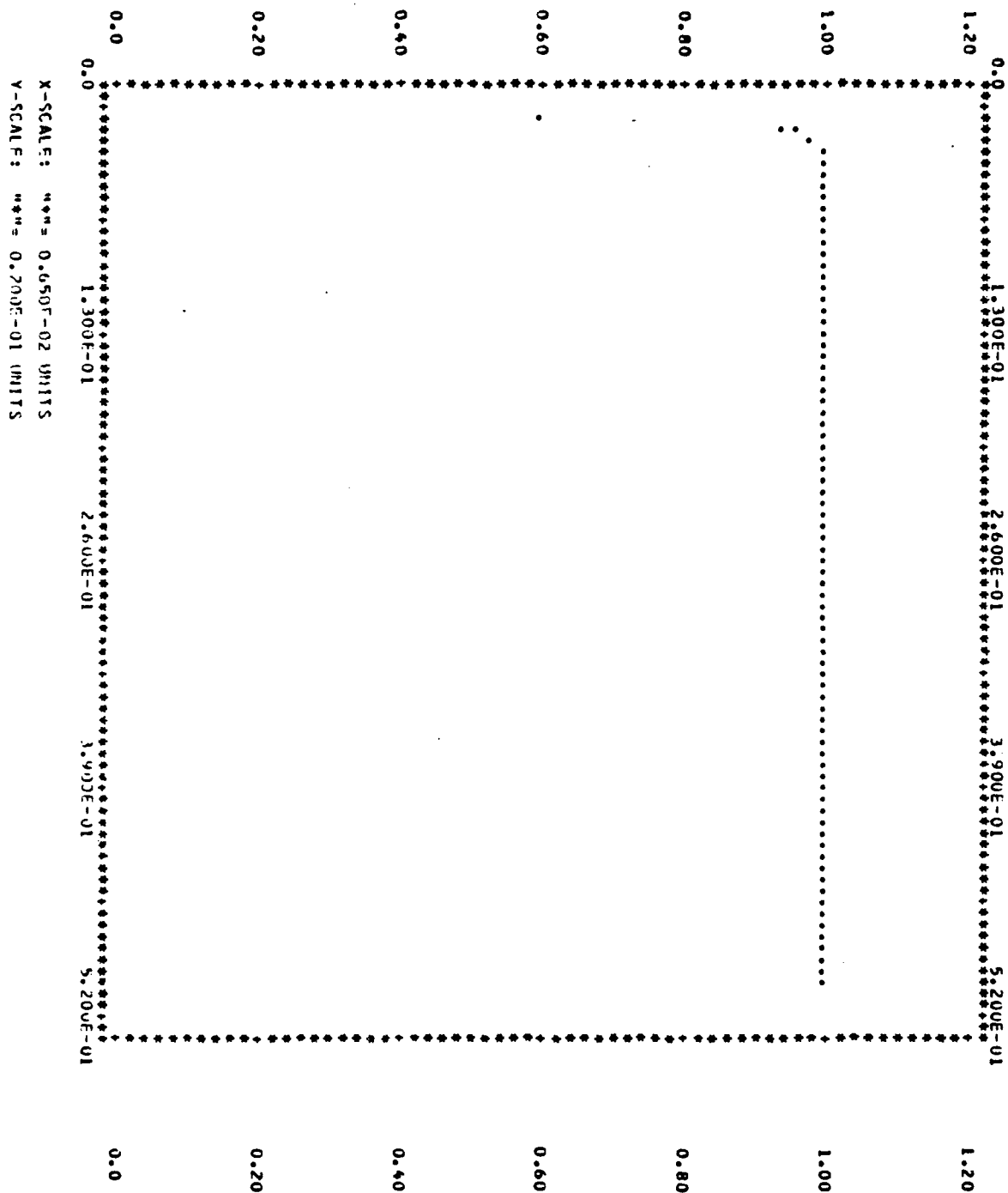
GLM LENS SHAPE





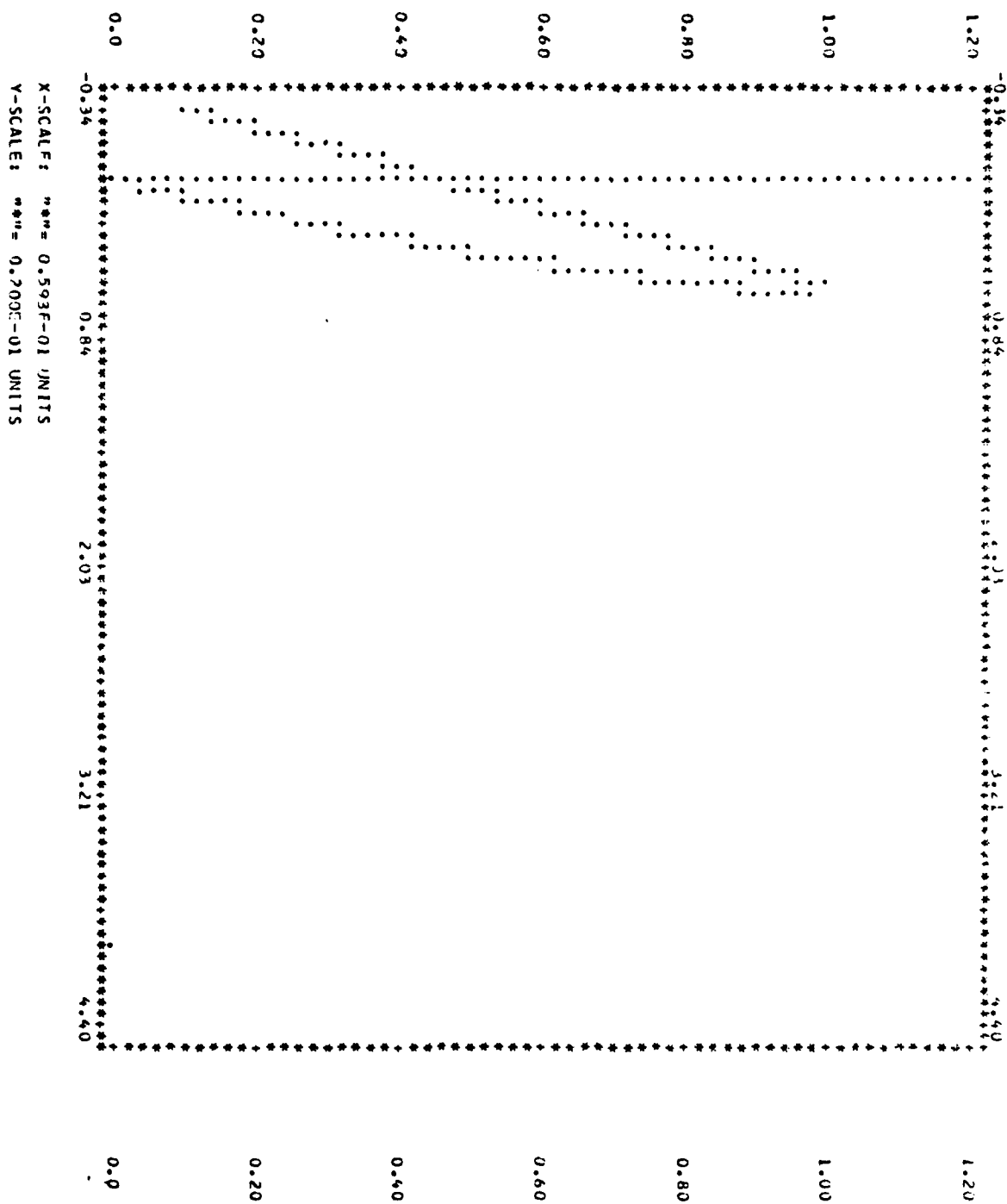


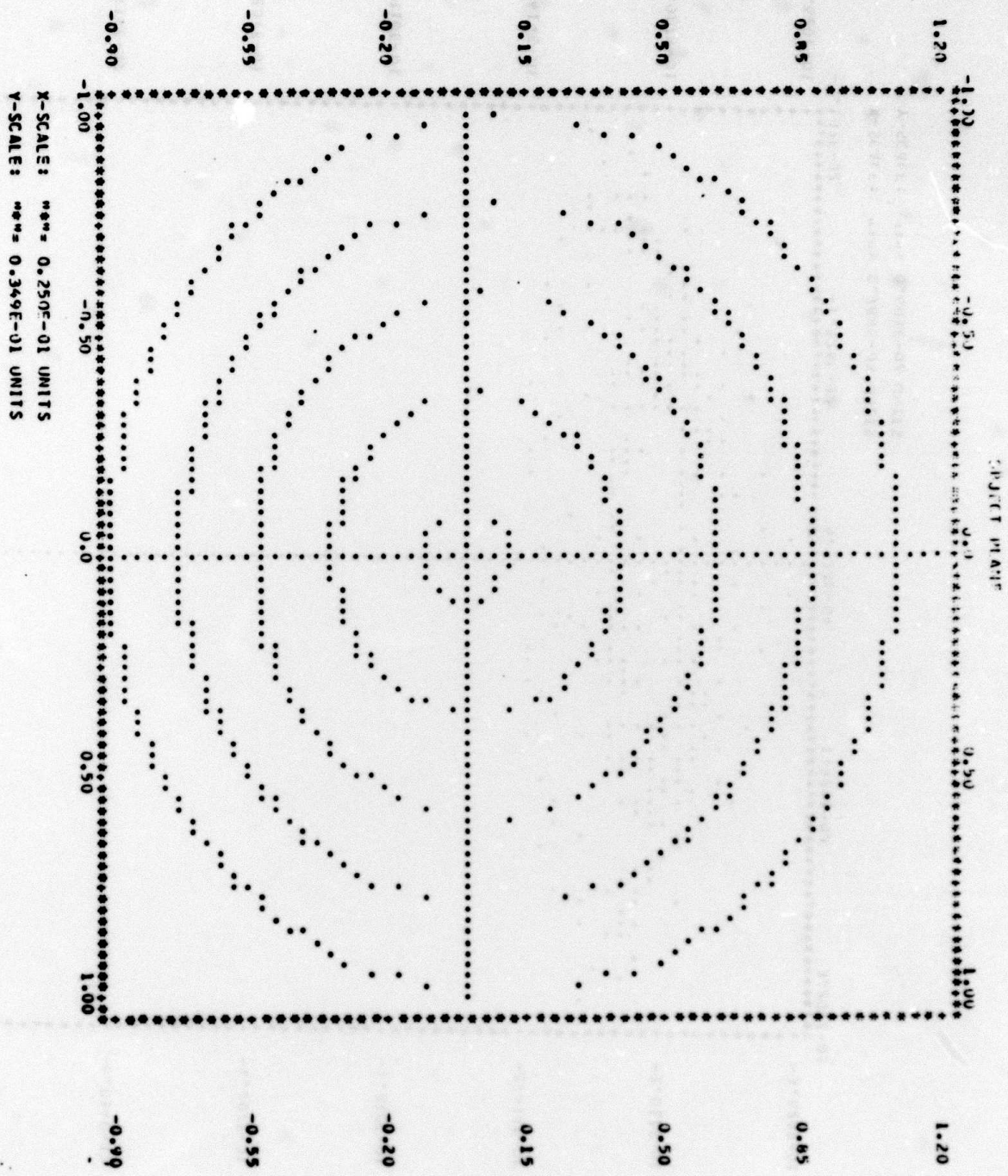
ENERGY DENSITY VS. RADIUS FROM CENTROID

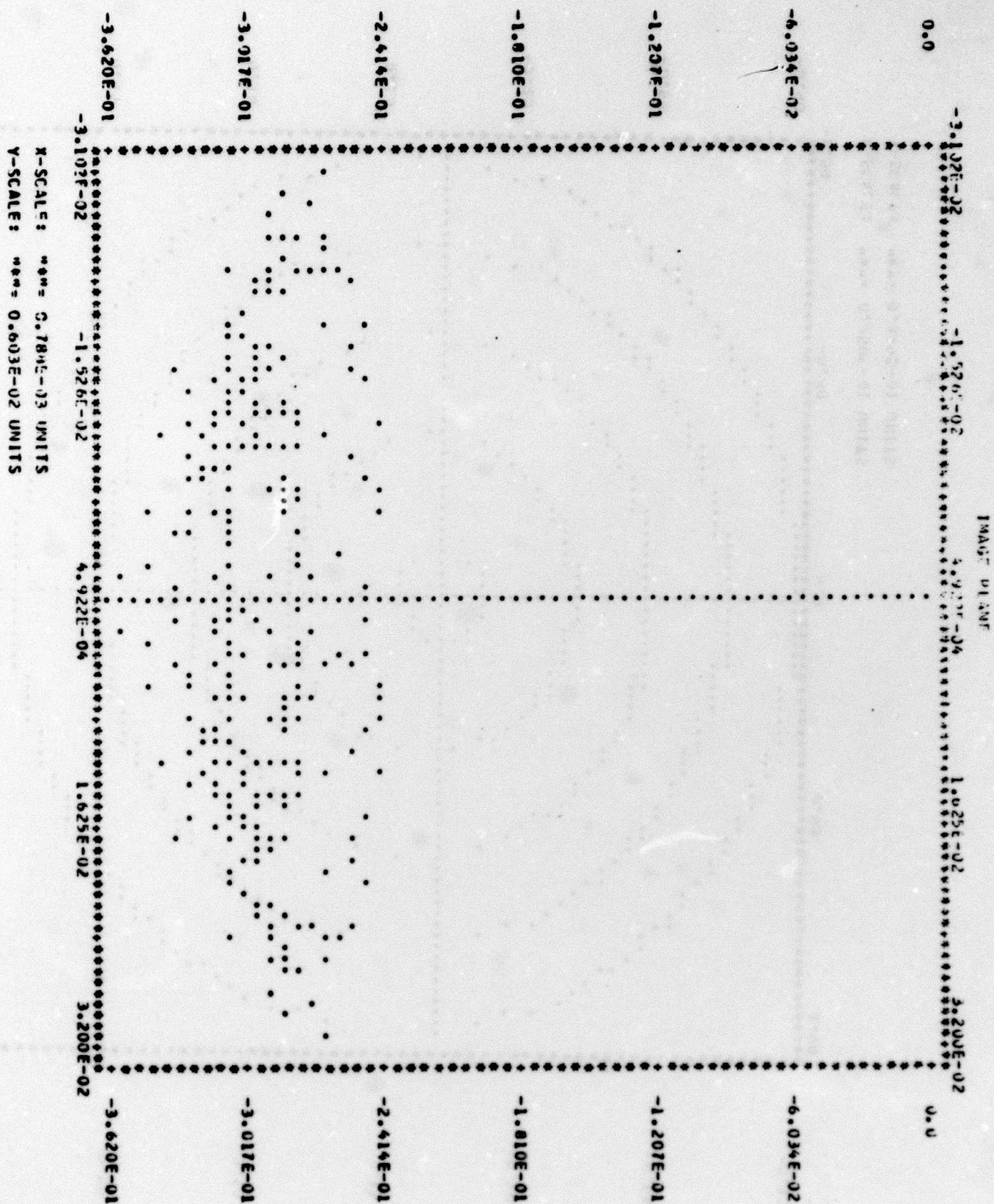


SUMMARY OF RESULTS

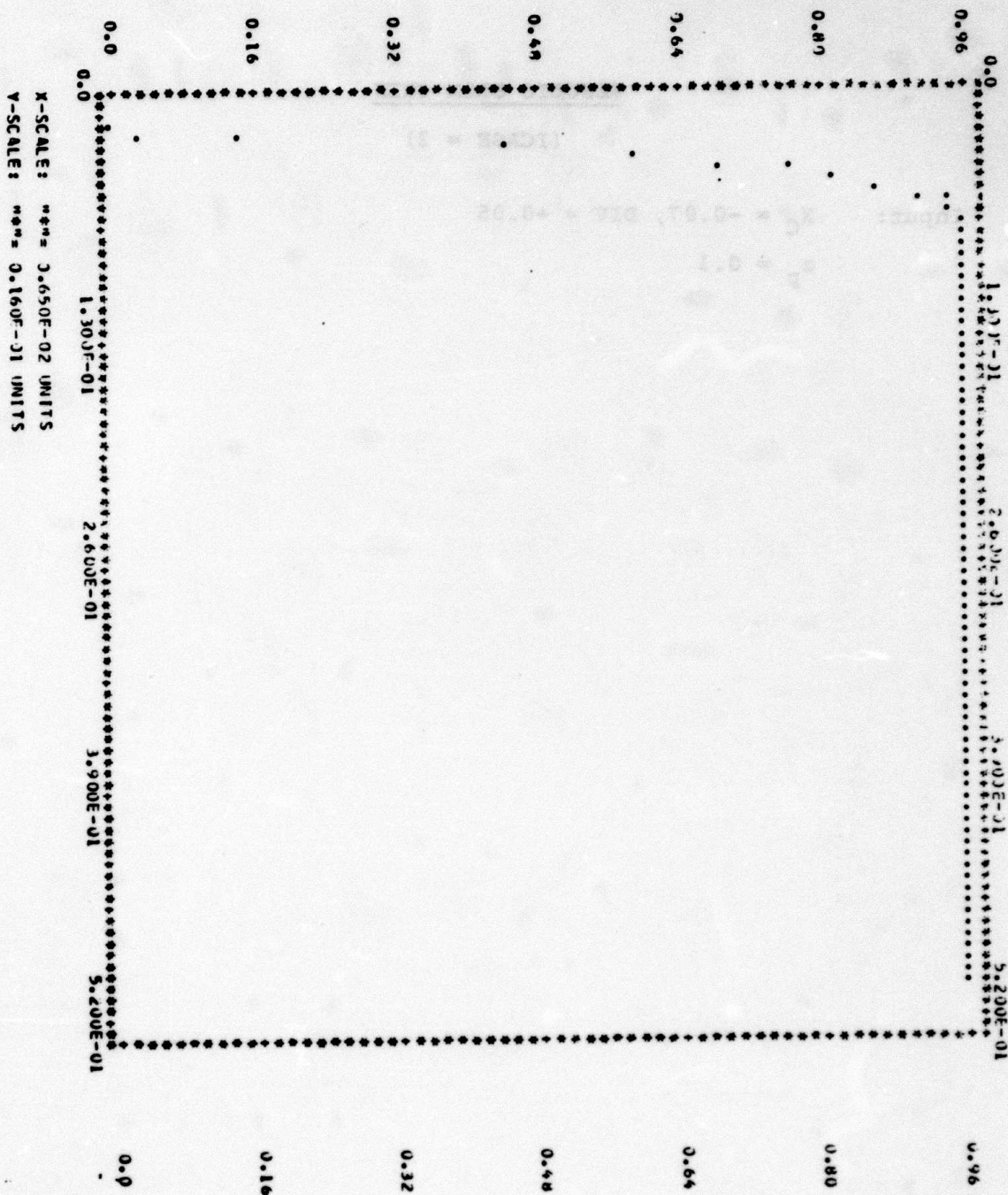
FOCAL LENGTH = 4.10000000 XPR.A = 7.683479 U = 0.0 I = 1.00H
 R = 1.00000000 T = 0.05000000 EFFICIENCY OF REFLECTION ARE: H1 = 1.00000000 A2 = 1.0002507 H3 = 1.00000000
 ALFAP = 0.10000000 G910 = 0.10000000 STATUA = 0.0 G940A = 0.0 AC = -0.01737 DIV = 0.05000
 RAYS = 297 CUBIT = 286 YCENTR = -0.2932486 SIGMAV = 0.0005436 SIGMAZ = 0.0002209
 RMSRAD = 0.0276461







ENERGY DENSITY VS. FACTOR FROM GPHOTOID



RESULTS FROM GRIN

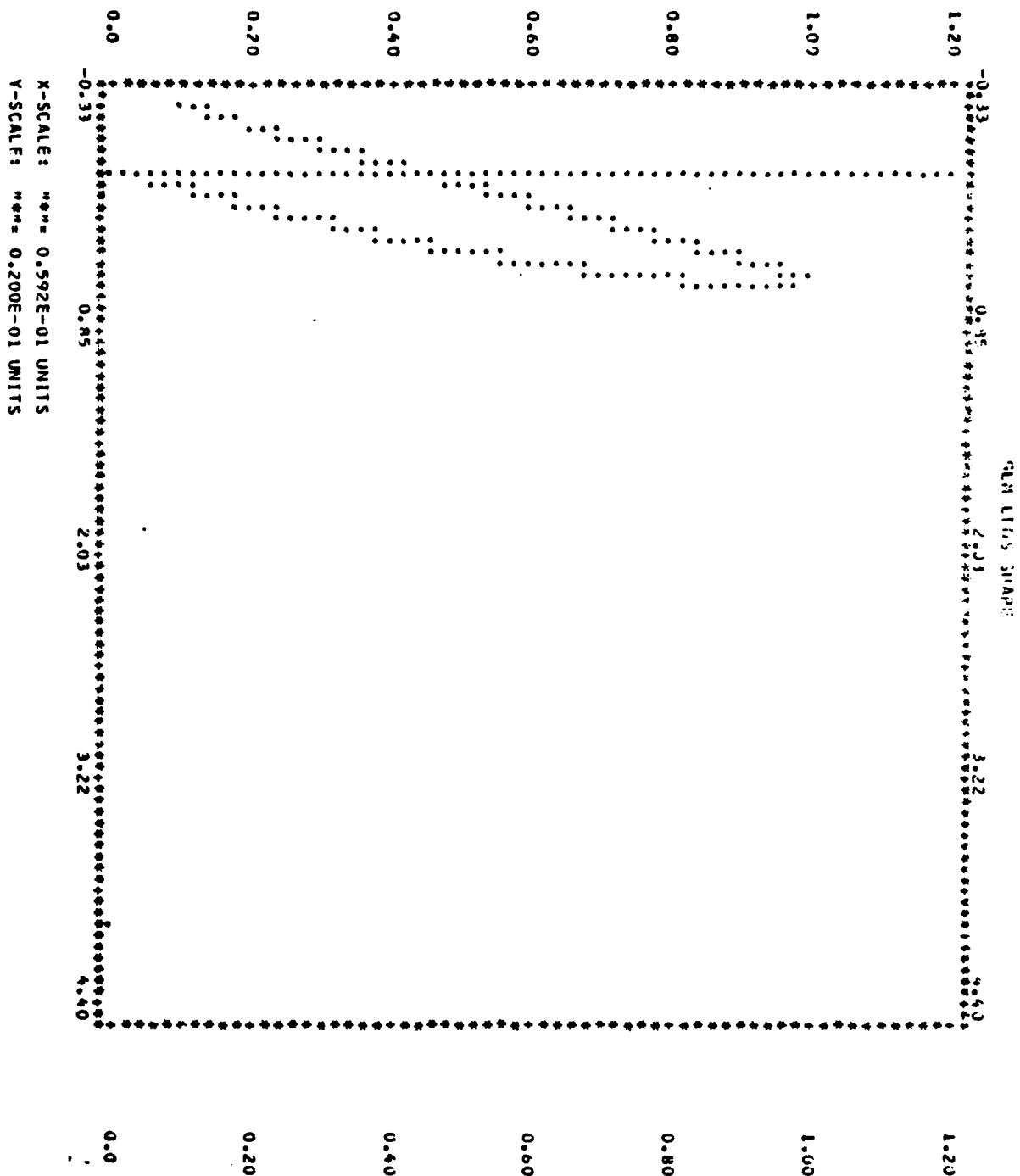
(ICASE = 2)

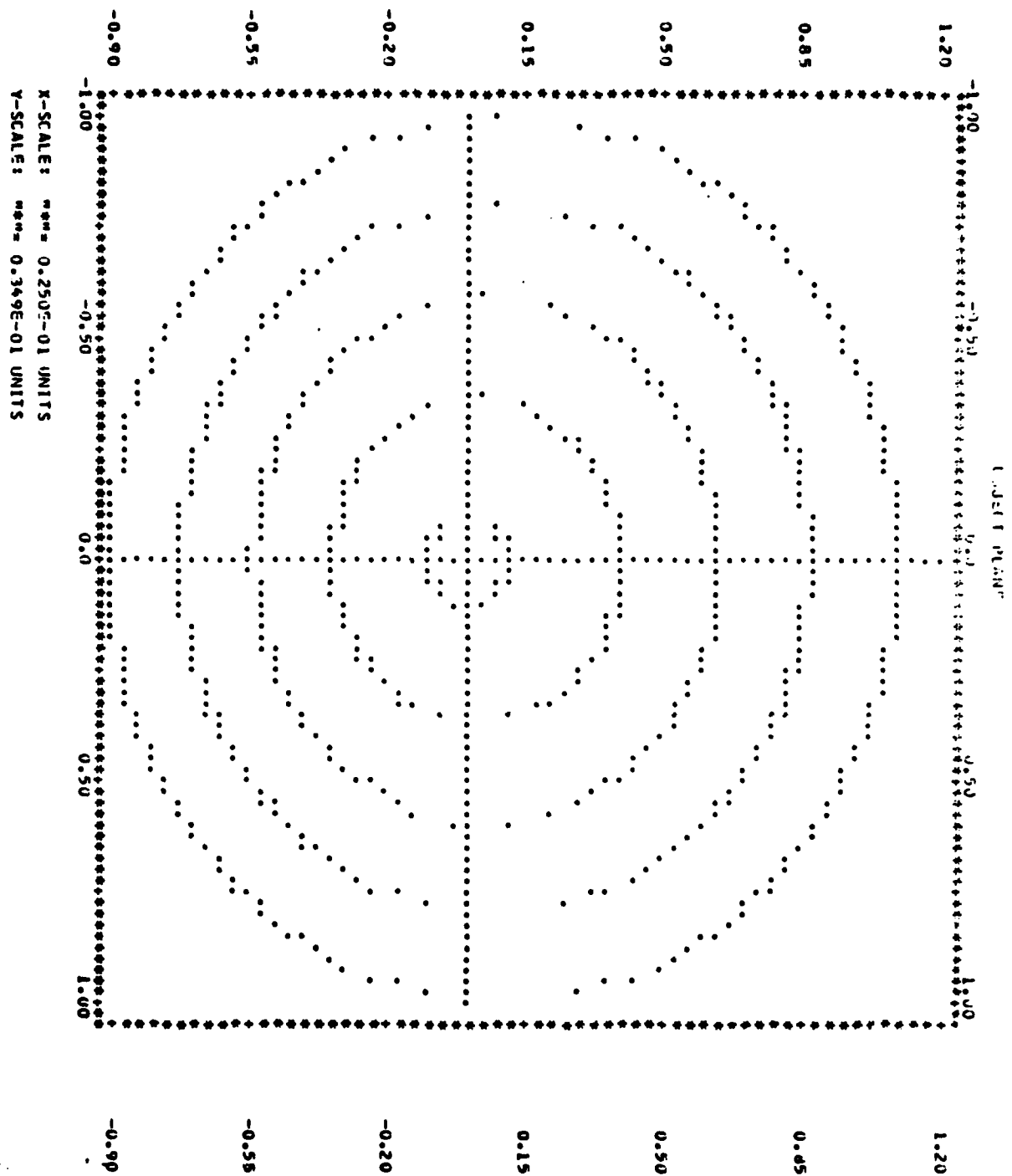
Input: $x_c = -0.07$, DIV = +0.05

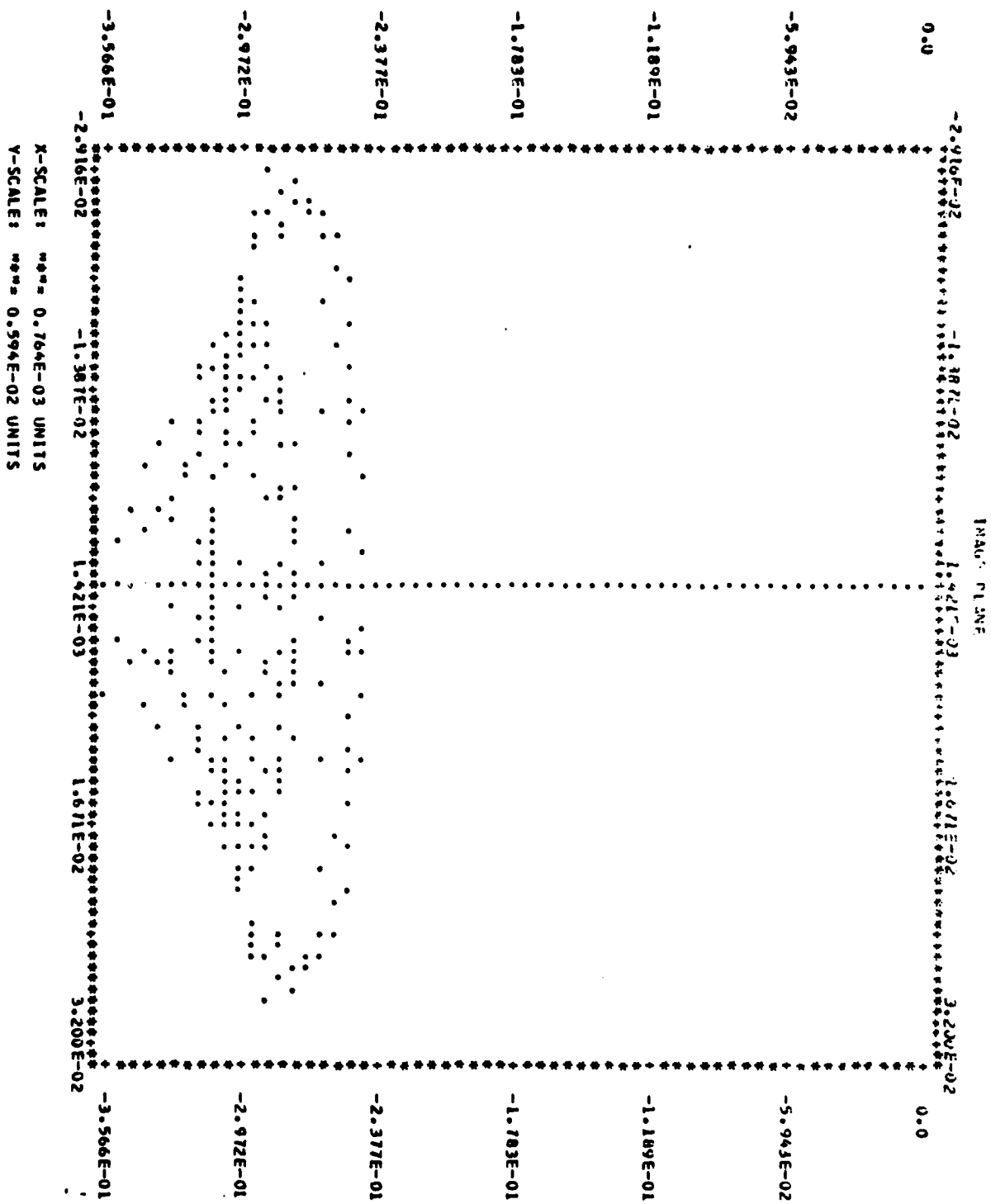
$\alpha_p = 0.1$

SUMMARY OF RESULTS

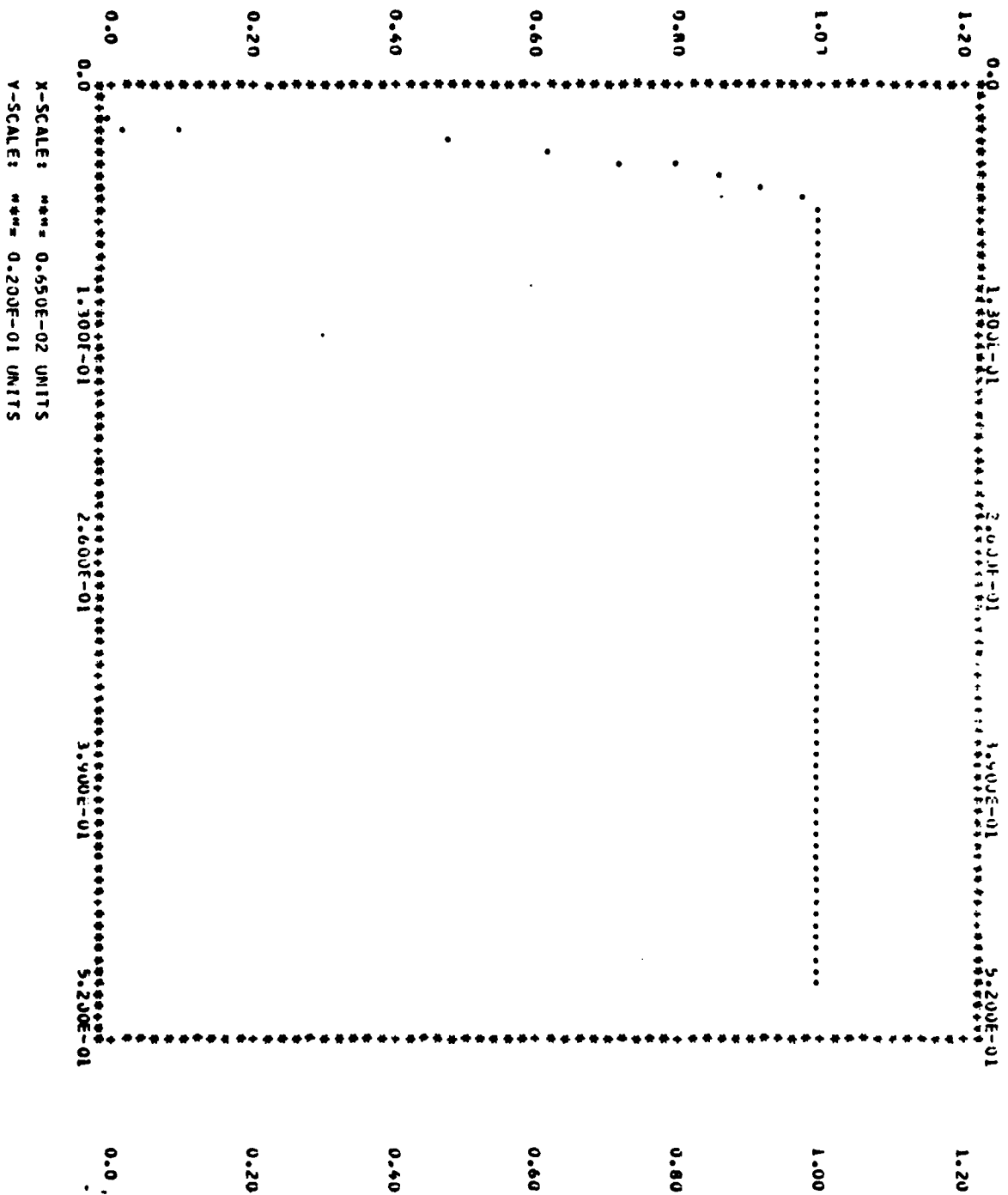
FOCAL LENGTH = 4.0110000 ALPMA = 0.7853779 U = 0.0 I = 1.000
 R = 1.0000000 T = 0.0500000 INDICES OF REFRACTION AET: M1 = 1.0010000 M2 = 1.4194584 M3 = 1.0000000
 ALFAP = 0.1000000 GCID = 0.1000000 STATMA = 0.0 GAMMA = 0.0 XC = -.50610 MIV = -.05000
 RAWS = 265 COUNT = 284 VCENTR = -0.2919591 SIGMAV = 0.0005272 SIGMAZ = 0.0002196
 RMSRAD = 0.0213276







ENERGY DEPOSIT VS. RADIUS OF CRYSTAL



X-SCALE: *** 0.650E-02 UNITS
Y-SCALE: *** 0.200E-01 UNITS

RESULTS FROM GRIN

1. Checkup for the homogeneous case.

GRIN PARAMETERS:

ALPHA = 0.7853979 BETA = 0.3222679 RADIUS = 1.00000 INCIDENT ANGLE = 0.0 ITERATIONS = 1000
 EDGE THICKNESS = 0.050000 INDICES OF REFRACTION: N1 = 1.00000 N2 = 1.50000 N3 = 1.00000
 FOCAL LENGTH FROM STATION ZERO = 4.00000 DELTA BETA = 0.00032
 CENTER OF SYMMETRY = 0.07000 CHANGE IN N2(1) = 0.0 ALFAP = 0.0
 NOTE: COORDINATES HAS BEEN SHIFTED IN CASE=2 BY X2(1);Y(0),X2(1)-0.0 ETC.

J E X1 Y1 X2 Y2 PSI BETA RR 12P RF 12 ETA T 11P 11 DWDXT
 0.44158 0.61444 3.55802 -0.51198
 ISKEW RAY TRACE PARAMETERS:

ALFAP = 0.0 GRID = 0.100000 SEE LENS PARAMETERS ABOVE.

RAY	RAY	RAY	X0	Y0	X1	Y1	Z1	DPL	YIN	ZIN	NTACTY	XDIAPY	YDIAPY
PT-11	PT-11	PT-11	CRP	CLP	CRP	CLP	D3	D1	NUM6	NUM7	NUM8		
1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

16	0.1733	0.2616	0.9768	-0.0281	-0.2022	3.1372	0.4420	0.7071	0.1090	-0.5116	1.00000	0.431E+00	0.361E-02
17	0.1000	0.0000	0.3642	-0.1000	0.5341	3.1964	0.7468	3.7813	0.0052	-0.0028	1.00000	0.445E+00	0.609E-02
18	0.0214	0.0320	0.4636	-0.1000	0.5824	3.0996	0.8637	3.6986	0.0061	0.0007	1.00000	0.445E+00	0.609E-02
19	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
20	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
21	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
22	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
23	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
24	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
25	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
26	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
27	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
28	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
29	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
30	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
31	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
32	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
33	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
34	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
35	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
36	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
37	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
38	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
39	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06
40	0.2000	0.0000	0.2418	-0.0330	0.0000	3.4653	4.2467	0.0155	0.0000	0.0000	1.00000	0.100E+06	0.100E+06

08-0.4716	C.7497	0.9999	0.0116	-0.0116	3.5203	0.4420	0.1414	-0.1091	-0.6944										
08-0.10000	C.20000	-0.21037	-0.10000	0.11679	0.03453	0.10906	4.23378	0.00747	-0.01495	1.00000	0.271E-01	-0.230E-05							
08-0.4413	C.6958	0.9992	0.0183	-0.0366	3.4441	0.4420	1.2236	-0.1704	-0.5886										
08-0.10000	C.31000	-0.12515	-0.10000	0.20659	0.06825	0.20624	4.17058	0.00535	-0.00620	1.00000	0.344E+00	0.324E-02							
08-0.4055	C.6331	0.9976	0.0219	-0.0631	3.3649	0.4421	0.3162	-0.1033	-0.5722										
90-0.10000	C.40000	-0.02967	-0.10000	0.28181	0.02655	0.30847	4.09841	0.00271	-0.00057	1.00000	0.436E+00	0.256E-02							
90-0.3611	C.5505	0.9953	0.0241	-0.0393	3.2939	0.4420	0.4123	-0.0049	-0.5552										
91-0.10000	C.50000	0.06392	-0.10000	0.35751	0.09155	0.41409	4.02145	0.00419	0.00068	1.00000	0.447E+00	0.424E-02							
91-0.3608	C.4702	0.9914	0.0265	-0.03281	3.2282	0.4421	3.5099	-0.1031	-0.5385										
92-0.10000	C.60000	0.16630	-0.10000	0.42446	0.09439	0.52260	3.94361	0.00722	-0.00055	1.00000	0.436E+00	C.706E-02							
92-0.3633	C.3697	0.9859	0.0288	-0.01645	3.1117	0.4420	0.6083	-0.1030	-0.5234										
93-0.10000	C.70000	0.26513	-0.10000	0.48726	0.08819	0.62362	3.86242	0.00522	-0.00145	1.00000	0.433E+00	C.495E-02							
93-0.1733	C.2616	0.9788	0.0288	-0.02126	3.1372	0.4420	0.7071	-0.1030	-0.5116										
94-0.10000	C.80000	0.36424	-0.10000	0.53941	0.09033	0.74766	3.78137	0.00580	-0.00145	1.00000	0.436E+00	C.561E-02							
94-0.0981	C.1475	0.9701	0.0309	-0.02407	3.1117	0.4420	0.8162	-0.1030	-0.5036										
95-0.10000	C.90000	0.46356	-0.10000	0.58247	0.09215	0.86458	3.69886	0.00594	0.00208	1.00000	0.449E+00	C.610E-02							
95-0.0214	C.0321	0.9650	0.0316	-0.02783	3.0996	0.4420	0.9055	-0.1030	-0.5002										
96-0.20000	C.0	-0.2419E-01	-0.20000	0.09460	0.09790	0.0	4.24767	0.0165E-01	0.0	1.00000	0.100E+06	C.100E+06							
96-0.4578	C.7123	0.9555	0.0333	0.0	3.4653	0.4420	0.2000	-0.2000	-0.5933										
97-0.20000	C.10000	-0.21837	-0.20000	0.11672	0.10917	0.05454	4.23355	0.02036	-0.00484	1.00000	0.162E+00	-0.296E-05							
97-0.4437	C.6997	0.9995	0.0345	-0.03172	3.4438	0.4420	1.2235	-0.2036	-0.5897										
98-0.20000	C.20000	-0.15914	-0.20000	0.17099	0.12885	0.12954	4.19425	0.0040E-01	0.0145	1.00000	0.481E+00	0.563E-02							
98-0.4327	C.6628	0.9995	0.0352	-0.03177	3.3521	0.4420	0.2828	-0.2000	-0.5797										
99-0.30000	C.30000	-0.08163	-0.20000	0.23886	0.14577	0.21939	4.13099	0.00407	-0.00201	1.00000	0.412E+00	0.264E-02							
99-0.3661	C.6702	0.9968	0.0459	-0.0665	3.3299	0.4421	1.3608	-0.2010	-0.5644										
100-0.30000	C.40000	0.00523	-0.20000	0.30970	0.15752	0.31799	4.07124	0.00545	0.00053	1.00000	0.452E+00	C.593E-02							
100-0.3421	C.5273	0.9949	0.0459	-0.0970	3.2678	0.4420	1.4412	-0.2000	-0.5489										
101-0.20000	C.50000	0.09654	-0.20000	0.37842	0.16685	0.42117	3.99871	0.00471	0.00052	1.00000	0.446E+00	0.499E-02							
101-0.2888	C.4414	0.9859	0.0534	-0.1311	3.2119	0.4420	1.5385	-0.2000	-0.5337										
102-0.20000	C.60000	-0.19047	-0.20000	0.44235	0.17419	0.52819	3.92363	0.00434	0.0156	1.00000	0.451E+00	0.487E-02							
102-0.2280	C.3460	0.9844	0.0564	-0.1664	3.1652	0.4420	0.6325	-0.2000	-0.5204										
103-0.20000	C.70000	0.28503	-0.20000	0.49904	0.17972	0.63854	3.84469	0.00461	0.00203	1.00000	0.452E+00	0.520E-02							
103-0.1597	C.2409	0.9773	0.0550	-0.2034	3.1299	0.4420	0.7280	-0.2000	-0.5098										
104-0.20000	C.80000	0.38264	-0.20000	0.54807	0.18437	0.75218	3.76554	0.00622	0.00079	1.00000	0.445E+00	0.642E-02							
104-0.6845	C.1270	0.9688	0.0613	-0.02417	3.1882	0.4420	1.8246	-0.2000	-0.5927										
105-0.20000	C.90000	0.47997	-0.20000	0.58862	0.19115	0.86843	3.68655	0.00471	-0.00152	1.00000	0.435E+00	0.428E-02							
105-0.6855	C.0083	0.9577	0.0629	-0.2867	3.1035	0.4420	1.9228	-0.2000	-0.5000										
106-0.30000	C.0	-0.14198	-0.30000	0.18429	0.20743	0.00038	4.18222	0.00435	0.00275	1.00000	-0.346E+01	-0.233E+00							
106-0.4141	C.6480	0.9982	0.0606	-0.03179	3.3179	0.4420	0.3300	-0.2000	-0.5754										
107-0.30000	C.10000	-0.12515	-0.30000	0.20099	0.27579	0.76899	4.17998	0.00785	-0.00043	1.00000	0.421E+00	0.651E-02							
107-0.4054	C.6331	0.9953	0.0636	-0.03281	3.3649	0.4420	1.3162	-0.2000	-0.5722										
108-0.30000	C.20000	-0.09143	-0.30000	0.23886	0.21891	0.14648	4.13909	0.00461	-0.00011	1.00000	0.440E+00	0.444E-02							
108-0.3661	C.6002	0.9958	0.0671	-0.0344	3.1299	0.4420	1.3476	-0.2000	-0.5624										
109-0.30000	C.30000	-0.01772	-0.30000	0.29172	0.23339	0.23426	4.09832	0.00461	0.00043	1.00000	0.448E+00	0.506E-02							
109-0.3539	C.5467	0.9958	0.0724	-0.03712	3.2835	0.4420	0.4243	-0.2000	-0.5428										
110-0.30000	C.40000	0.03802	-0.30000	0.35919	0.24591	0.32977	4.02951	0.00391	0.00115	1.00000	0.454E+00	C.461E-02							
110-0.3121	C.4786	0.9918	0.0777	-0.03116	3.2141	0.4420	1.5000	-0.2000	-0.5399										
111-0.30000	C.50000	0.14111	-0.30000	0.47954	0.25678	0.43098	3.96288	0.00445	0.00066	1.00000	0.448E+00	0.501E-02							

112-0.34000	C.3963	0.9875	0.0819	-0.1349	3.1884	0.4420	1.5831	-0.3077	-0.5270	0.443E+00	0.527E-02
113-0.34000	C.3023	0.3816	0.0061	-0.1457	3.1500	0.4420	3.6518	-0.3077	-0.5153	0.443E+00	0.527E-02
114-0.34000	C.2001	0.3743	0.0897	-0.2668	3.1213	0.4420	3.0177	0.0066	0.0092	0.446E+00	0.706E-02
115-0.34000	C.0919	0.4134	0.3000	0.5415	0.7826	0.7585	3.7414	0.0075	0.0098	0.446E+00	0.393E-02
116-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
117-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
118-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
119-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
120-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
121-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
122-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
123-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
124-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
125-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
126-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
127-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
128-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
129-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
130-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
131-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
132-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
133-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
134-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02
135-0.34000	C.0252	0.5057	0.3000	0.5908	0.7886	0.8745	3.6684	0.0057	0.0262	0.433E+00	0.416E-02

0.2487	0.3782	0.9864	0.1643	0.0712	3.1803	0.4420	0.6000	-0.6000	-0.5245
136-0.60000	0.10000	0.16630	0.60000	0.43445	0.52216	0.08705	3.94261	0.00205	0.00029
0.4433	0.9859	0.1650	-0.0255	3.1763	0.4420	0.6063	-0.6000	-0.5234	
137-0.60000	0.20000	0.19947	0.60000	0.44206	0.52882	0.17821	3.92362	0.00183	0.00583
0.4288	0.98460	0.1670	-0.0035	3.1652	0.4420	0.60325	-0.6000	-0.5204	
138-0.60000	0.30000	0.22884	0.60000	0.46598	0.53444	0.27034	3.89188	0.00485	0.00472
0.1998	0.3323	0.9816	0.1712	-0.0843	3.1500	0.4420	0.6000	-0.5155	
139-0.60000	0.40000	0.2713	0.60000	0.49315	0.54448	0.34515	3.85083	0.00351	0.01215
0.1634	0.2465	0.9717	0.1749	-0.1139	3.1326	0.4420	0.6000	-0.5103	
140-0.60000	0.50000	0.33914	0.60000	0.52499	0.55494	0.46532	3.80144	0.00222	0.00297
0.1191	0.1792	0.9727	0.1788	-0.1481	3.1163	0.4420	0.6000	-0.5054	
141-0.60000	0.60000	0.40655	0.60000	0.55550	0.57619	0.56894	3.76619	0.00284	0.00261
0.0660	0.0990	0.9660	0.1831	-0.1634	3.1046	0.4420	0.6000	-0.5016	
142-0.60000	0.70000	0.47997	0.60000	0.58863	0.57619	0.67708	3.68655	0.00560	0.00099
0.0055	0.0083	0.9517	0.1876	-0.2181	3.1004	0.4420	0.6000	-0.5000	
143-0.60000	0.80000	0.55802	0.60000	0.61444	0.58974	0.78631	3.62175	0.00123	0.00165
0.0567	0.0851	0.9483	0.1904	-0.2539	3.1040	0.4420	1.0000	-0.6000	-0.5012
144-0.70000	0.0	0.35802	0.70000	0.48311	0.63170	0.00199	3.86773	0.00024	0.00429
0.1799	0.2717	0.9795	0.2013	0.0001	3.1391	0.4420	0.7000	-0.5125	
145-0.70000	0.10000	0.29513	0.70000	0.48125	0.63298	0.09266	3.86242	0.00322	0.00429
0.1733	0.2616	0.9788	0.2028	-0.0882	3.1375	0.4420	0.7000	-0.5116	
146-0.70000	0.20000	0.28603	0.70000	0.49103	0.63758	0.18328	3.84469	0.00006	0.00232
0.1329	0.2409	0.9773	0.2037	-0.0573	3.1299	0.4420	0.7280	-0.7000	-0.5067
147-0.70000	0.30000	0.31960	0.70000	0.51101	0.64391	0.27886	3.81780	0.00366	0.00404
0.0981	0.1329	0.9741	0.2075	-0.0880	3.1213	0.4420	0.7616	-0.7000	-0.5067
148-0.70000	0.40000	0.36424	0.70000	0.53159	0.65272	0.37566	3.78132	0.00394	0.00256
0.0554	0.0831	0.9646	0.2149	-0.1528	3.1038	0.4420	0.8062	-0.7000	-0.5036
149-0.70000	0.50000	0.41825	0.70000	0.56001	0.66241	0.47656	3.73714	0.00452	0.00242
0.0055	0.0783	0.9577	0.2184	-0.1868	3.1018	0.4420	0.9899	-0.7000	-0.5000
150-0.70000	0.60000	0.47997	0.70000	0.58863	0.67287	0.59101	3.68655	0.00535	0.00185
0.0464	0.0696	0.9499	0.2213	-0.2204	3.1018	0.4420	1.0000	-0.7000	-0.5000
151-0.70000	0.70000	0.54797	0.70000	0.61145	0.68337	0.68899	3.62892	0.00304	0.00535
0.1024	0.1539	0.9706	0.2406	0.0007	3.1131	0.4420	0.8000	-0.8000	-0.5000
152-0.80000	0.0	0.35802	0.80000	0.54438	0.74590	0.00254	3.78667	0.00307	0.00460
0.0081	0.1475	0.9701	0.2409	-0.0294	3.1117	0.4420	0.8062	-0.8000	-0.5000
153-0.80000	0.10000	0.36424	0.80000	0.56001	0.74694	0.00254	3.78667	0.00307	0.00460
0.0045	0.1270	0.9684	0.2421	-0.1558	3.1087	0.4420	0.8062	-0.8000	-0.5000
154-0.80000	0.20000	0.41825	0.80000	0.58863	0.75659	0.00254	3.78667	0.00307	0.00460
0.0612	0.0919	0.9654	0.2444	-0.1613	3.1040	0.4420	0.8062	-0.8000	-0.5000
155-0.80000	0.30000	0.47997	0.80000	0.61145	0.76417	0.00254	3.78667	0.00307	0.00460
0.0283	0.0425	0.9610	0.2476	-0.1731	3.1010	0.4420	0.8062	-0.8000	-0.5000
156-0.80000	0.40000	0.54797	0.80000	0.64145	0.77354	0.00254	3.78667	0.00307	0.00460
0.0104	0.0162	0.9534	0.2508	-0.1861	3.1001	0.4420	0.8062	-0.8000	-0.5000
157-0.80000	0.50000	0.61145	0.80000	0.67287	0.78332	0.00254	3.78667	0.00307	0.00460
0.0051	0.0051	0.9483	0.2538	-0.2038	3.1044	0.4420	0.8062	-0.8000	-0.5000
158-0.90000	0.0	0.45802	0.90000	0.54438	0.84590	0.00254	3.78667	0.00307	0.00460
0.0051	0.0051	0.9483	0.2538	-0.2038	3.1044	0.4420	0.8062	-0.8000	-0.5000
159-0.90000	0.0	0.45802	0.90000	0.54438	0.84590	0.00254	3.78667	0.00307	0.00460

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MIRROR IMAGE CREW RAYS FOLLOW
IMAGE RAY RAY1 RAY2 DOPL V14 Z14 N14CTV XPIAP1
165 1 0.0 -0.2000000 4.24781704 0.0 0.0190995 1.0000000 -0.143E+00
166 2 0.0 -0.3000001 4.18230820 0.0 0.0035946 1.0000000 0.376E+00
167 3 0.0 -0.4000001 4.10801315 0.0057445 0.0026656 1.0000000 0.541E+00
168 4 0.0 -0.5000001 4.02949905 0.0031240 0.0014027 1.0000000 0.312E-02
169 5 0.0 -0.6000001 3.94920363 0.0036701 0.0022022 1.0000000 0.429E+00
170 6 0.0 -0.7000002 3.86772346 0.0040978 0.002471 1.0000000 0.366E-02
171 7 0.0 -0.8000002 3.78667068 0.0051622 0.0030653 1.0000000 0.441E+00
172 8 0.0 -0.9000002 3.70408430 0.0064321 0.0049802 1.0000000 0.430E+00
173 9 0.1000000-0.1000000 4.27620602 -0.0134138 0.0134328 1.0000000 0.515E-02
174 10 0.1000000-0.2000000 4.23377800 -0.0074725 0.0149505 1.0000000 0.430E+00
175 11 0.1000000-0.3000001 4.17058236 0.0005957 0.0001937 1.0000000 0.643E-02
176 12 0.1000000-0.4000001 4.08840775 0.0021195 0.0017822 1.0000000 0.430E+00
177 13 0.1000000-0.5000001 4.02144979 0.0040440 0.0009454 1.0000000 0.322E-02
178 14 0.1000000-0.6000001 3.94261169 0.0065244 0.0032411 1.0000000 0.435E+00
179 15 0.1000000-0.7000002 3.86242008 0.0084937 0.0032411 1.0000000 0.423E+00
180 16 0.1000000-0.8000002 3.78136730 0.00952644 0.0028350 1.0000000 0.426E+00
0.561E-02

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101	11 0.100000-0.900000	3.69885731	0.0061719-0.0007420	1.0000000	0.445E+00	
102	15 0.200000-0.100000	4.23354916	-0.0096710	0.0048371	1.0000000	0.162E+00
103	20 0.200000-0.200000	4.19424915	0.0014912	0.0040836	1.0000000	0.330E+00
104	21 0.200000-0.300000	4.13809490	-0.0003108	0.0044667	1.0000000	0.342E+00
105	22 0.200000-0.400000	4.07125664	0.0040126	0.0037993	1.0000000	0.376E+00
106	23 0.200000-0.500000	3.99870968	0.0038123	0.0029189	1.0000000	0.262E+00
107	24 0.200000-0.600000	3.92262745	0.0044113	0.0013564	1.0000000	0.433E+00
108	25 0.200000-0.700000	3.84469032	0.0049873	0.0007067	1.0000000	0.434E+00
109	26 0.200000-0.800000	3.76593476	0.0058548	0.0022324	1.0000000	0.435E+00
110	27 0.200000-0.900000	3.68655014	0.0034583	0.0037356	1.0000000	0.433E+00
111	29 0.300000-0.100000	4.17098427	-0.0006543	0.0043663	1.0000000	0.425E+00
112	30 0.300000-0.200000	4.13809395	-0.0018694	0.0042081	1.0000000	0.422E+00
113	31 0.300000-0.300000	4.08931923	0.0004252	0.0046253	1.0000000	0.349E+00
114	32 0.300000-0.400000	4.02950668	0.0022334	0.0034167	1.0000000	0.349E+00
115	33 0.300000-0.500000	3.96287727	0.0028701	0.0035567	1.0000000	0.479E+00
116	34 0.300000-0.600000	3.89187622	0.0032192	0.0040933	1.0000000	0.476E+00
117	35 0.300000-0.700000	3.81779999	0.0052586	0.0041849	1.0000000	0.410E+00
118	36 0.300000-0.800000	3.74141121	0.0033311	0.0016008	1.0000000	0.524E+00
119	37 0.300000-0.900000	3.66483879	0.0024558	0.0051180	1.0000000	0.422E+00
120	39 0.400000-0.100000	4.09841061	0.0002853	0.0041785	1.0000000	0.436E+00
121	40 0.400000-0.200000	4.07125568	0.0018406	0.0056564	1.0000000	0.415E+00
122	41 0.400000-0.300000	4.02950764	0.0013373	0.0040893	1.0000000	0.195E+00
123	42 0.400000-0.400000	3.97659969	0.0032655	0.0025432	1.0000000	0.329E+00
124	43 0.400000-0.500000	3.91658411	0.0025682	0.0043292	1.0000000	0.670E+00

206	45 0.400001-0.700002	3.78136921	0.0014706	0.0033197	1.0000000	0.427E+00
207	46 0.400001-0.800002	3.78887069	0.0031533	0.0034804	1.0000000	0.428E+00
208	47 0.400001-0.900002	3.63513851	0.0024678	0.0063819	1.0000000	0.429E+00
209	48 0.500001-0.100000	4.02145481	0.0007316	0.0043819	1.0000000	0.531E+02
210	50 0.500001-0.200000	3.95870968	0.0012194	0.0065384	1.0000000	0.379E+00
211	51 0.500001-0.300000	3.96287441	0.0008025	0.0043737	1.0000000	0.218E+01
212	52 0.500001-0.400000	3.91658592	0.0015495	0.0047715	1.0000000	0.389E+00
213	53 0.500001-0.500000	3.86241627	0.0023125	0.0059635	1.0000000	0.171E+01
214	54 0.500001-0.600000	3.80144215	0.0028403	0.0021100	1.0000000	0.402E+00
215	55 0.500001-0.700000	3.73713970	0.0020005	0.0042123	1.0000000	0.822E+02
216	56 0.500001-0.800000	3.66836357	0.0033442	0.0035158	1.0000000	0.431E+00
217	58 0.600001-0.100000	3.94261456	-0.0020880	0.0002881	1.0000000	0.459E+02
218	59 0.600001-0.200000	3.92262459	0.0020603	0.0057829	1.0000000	0.423E+00
219	60 0.600001-0.300000	3.89187527	0.0008706	0.0067160	1.0000000	0.50E+02
220	61 0.600001-0.400000	3.85083008	0.0006314	0.0040655	1.0000000	0.432E+00
221	62 0.600001-0.500000	3.80144215	0.0025223	0.0027204	1.0000000	0.427E+00
222	63 0.600001-0.600000	3.74619007	0.0026141	0.0028427	1.0000000	0.545E+02
223	64 0.600001-0.700000	3.68654537	0.0018344	0.0053829	1.0000000	0.418E+00
224	65 0.600001-0.800000	3.62175465	-0.0012268	0.0016519	1.0000000	0.643E+02
225	67 0.700002-0.100000	3.86242008	-0.0018887	0.0050298	1.0000000	0.436E+00
226	68 0.700002-0.200000	3.84469221	0.0012742	0.0019271	1.0000000	0.121E+04
227	69 0.700002-0.300000	3.81779575	0.0004017	0.0054382	1.0000000	0.236E+00
228	70 0.700002-0.400000	3.78136826	0.0001986	0.0046919	1.0000000	0.410E+00
						0.758E+02
						0.130E+01
						0.303E+00
						0.836E+02

229	71 0.7000002-0.5000001	3.73713875	0.0098270	0.0050603	1.0000000	0.410E+00
230	72 0.7000002-0.4000001	3.68654537	0.0109997	0.0056100	1.0000000	0.413E+00
231	73 0.7000002-0.3000002	3.62052054	0.0053498	0.0030365	1.0000000	0.429E+00
232	75 0.0000002-0.1000000	3.74136921	-0.0015297	0.0051508	1.0000000	0.638E-02
233	76 0.0000002-0.2000000	3.74594925	0.0005434	0.0052606	1.0000000	0.280E+00
234	77 0.0000002-0.3000001	3.74140835	0.0014806	0.0049132	1.0000000	0.387E-01
235	78 0.0000002-0.4000001	3.70806612	0.0012226	0.0062661	1.0000000	0.359E+00
236	79 0.0000002-0.5000001	3.66835705	0.0019963	0.0054873	1.0000000	0.213E-01
237	80 0.0000002-0.6000001	3.62175083	-0.0016157	0.0012376	1.0000000	0.391E+00
238	82 0.1000002-0.1000000	3.69885540	0.0014205	-0.0025097	1.0000000	0.145E-01
239	83 0.9000002-0.2000000	3.68654060	-0.0020115	0.0005708	1.0000000	0.394E+00
240	84 0.9000002-0.3000001	3.66483402	-0.0019777	0.0069733	1.0000000	0.137E-01
241	85 0.9000002-0.4000001	3.63512611	-0.0020176	0.0073020	1.0000000	0.409E+00
242	87 0.1000000-0.1000000	4.27620602	0.0134138	0.0134328	1.0000000	0.107E-01
243	88 0.1000000-0.2000000	4.23377800	0.0074725	0.0149505	1.0000000	0.372E+00
244	89 0.1000000-0.3000001	4.17098234	0.0053931	0.0061972	1.0000000	0.184E-01
245	90 0.1000000-0.4000001	4.09840775	0.0027089	0.0005748	1.0000000	-0.718E+00
246	91 0.1000000-0.5000001	4.02144909	0.0040982	-0.0006873	1.0000000	-0.129E-04
247	92 0.1000000-0.6000001	3.94261169	0.0072236	0.0009497	1.0000000	0.344E+00
248	93 0.1000000-0.7000002	3.86242008	0.0052215	0.0018533	1.0000000	0.324E-02
249	94 0.1000000-0.8000002	3.78136777	0.0058706	0.0014518	1.0000000	0.436E+00
250	95 0.1000000-0.9000002	3.69886208	0.0059587	-0.0020817	1.0000000	0.433E+00
251	97 0.2000000-0.1000000	4.23354916	0.0096717	0.0048371	1.0000000	0.436E+00
252	98 0.2000000-0.2000000	4.15424915	0.0040861	-0.0014917	1.0000000	-0.162E+00

253	95-0.200000-0.300001	4.1389490	0.0040009	0.0020119	1.0000000	0.412E+00
254	100-0.200000-0.400001	4.0712564	0.0034467	-0.0009313	1.0000000	0.432E+00
255	101-0.200000-0.500001	3.99870948	0.0047748	-0.0005158	1.0000000	0.446E+00
256	102-0.200000-0.600001	3.92262745	0.0043437	-0.0015618	1.0000000	0.451E+00
257	103-0.200000-0.700002	3.84469932	0.0046076	-0.0020347	1.0000000	0.452E+00
258	104-0.200000-0.800002	3.76553876	0.0062163	-0.0017867	1.0000000	0.445E+00
259	105-0.200000-0.900002	3.68655119	0.0047147	0.0019197	1.0000000	0.435E+00
260	107-0.300000-0.100000	4.17058427	0.00178518	0.0004347	1.0000000	0.421E+00
261	108-0.300000-0.200000	4.1389395	0.0044951	0.0010957	1.0000000	0.440E+00
262	109-0.300000-0.300001	4.08921923	0.0046293	-0.0004252	1.0000000	0.440E+00
263	110-0.300000-0.400001	4.02050668	0.0039058	-0.0011879	1.0000000	0.454E+00
264	111-0.300000-0.500001	3.96227632	0.0044900	-0.0008590	1.0000000	0.440E+00
265	112-0.300000-0.600001	3.90187622	0.0032064	-0.0001195	1.0000000	0.443E+00
266	113-0.300000-0.700002	3.81779399	0.0066570	-0.0009219	1.0000000	0.446E+00
267	114-0.300000-0.800002	3.74141121	0.0035624	-0.0005843	1.0000000	0.446E+00
268	115-0.300000-0.900002	3.66483784	0.0059393	0.0026217	1.0000000	0.433E+00
269	117-0.400000-0.100000	4.05841347	0.0026416	-0.0055342	1.0000000	0.416E+00
270	118-0.400000-0.200000	4.07125568	0.0039065	-0.0042384	1.0000000	0.401E+00
271	119-0.400000-0.300001	4.02950764	0.0035535	-0.0024226	1.0000000	0.474E+00
272	120-0.400000-0.400001	3.97659874	0.0025439	-0.0032657	1.0000000	0.472E+00
273	121-0.400000-0.500001	3.91658491	0.0047873	-0.0015551	1.0000000	0.453E+00
274	122-0.400000-0.600001	3.85082245	0.0044280	-0.0015449	1.0000000	0.451E+00
275	123-0.400000-0.700002	3.78137014	0.0036079	0.0004176	1.0000000	0.440E+00
276	124-0.400000-0.800002	3.70887089	0.0046742	-0.0004343	1.0000000	0.446E+00

277	125-0.4000001-0.5000002	3.63513051	0.0064029	0.0024297	1.0000000	0.430E+00
278	127-0.5000001-0.1000000	4.02145481	0.0010009	0.0042052	1.0000000	0.614E+00
279	128-0.5000001-0.2000000	3.95870968	0.0036254	0.0055743	1.0000000	0.233E+01
280	129-0.5000001-0.3000001	3.96287441	0.0034848	0.0027714	1.0000000	0.550E+00
281	130-0.5000001-0.4000001	3.91650592	0.0043177	0.0025625	1.0000000	0.476E+00
282	131-0.5000001-0.5000001	3.66241627	0.0039636	0.0023128	1.0000000	0.745E+00
283	132-0.5000001-0.6000001	3.60144215	0.0025070	0.0024131	1.0000000	0.450E+00
284	133-0.5000001-0.7000002	3.73713970	0.0046332	0.0052622	1.0000000	0.430E+00
285	134-0.5000001-0.8000002	3.66036357	0.0046262	0.0014655	1.0000000	0.440E+00
286	136-0.6000001-0.1000000	3.94261456	0.0020080	0.0002001	1.0000000	0.555E+02
287	137-0.6000001-0.2000000	3.92242459	0.0018327	0.0058342	1.0000000	0.432E+00
288	138-0.6000001-0.3000001	3.89107527	0.0040479	0.0047212	1.0000000	0.350E+03
289	139-0.6000001-0.4000001	3.85002912	0.0035105	0.0021466	1.0000000	0.547E+00
290	140-0.6000001-0.5000001	3.80144215	0.0022221	0.0025720	1.0000000	0.197E+01
291	141-0.6000001-0.6000001	3.74619007	0.0020422	0.0026136	1.0000000	0.497E+00
292	142-0.6000001-0.7000002	3.68656537	0.0056022	0.0005915	1.0000000	0.144E+01
293	143-0.6000001-0.8000002	3.62175465	0.0012268	0.0016519	1.0000000	0.460E+00
294	145-0.7000002-0.1000000	3.86242070	0.0032207	0.0042936	1.0000000	0.547E+00
295	146-0.7000002-0.2000000	3.84449414	0.0000630	0.0023152	1.0000000	0.341E+01
296	147-0.7000002-0.3000001	3.81779579	0.0036606	0.0040305	1.0000000	0.401E+00
297	148-0.7000002-0.4000001	3.78137112	0.0039424	0.0025558	1.0000000	0.809E+02
298	149-0.7000002-0.5000001	3.73713975	0.0045169	0.0024221	1.0000000	0.463E+00
299	150-0.7000002-0.6000001	3.68654537	0.0053916	0.0016466	1.0000000	0.457E+00
300	151-0.7000002-0.7000002	3.62052151	0.0039340	0.0053493	1.0000000	0.752E+02
						0.465E+00
						0.440E+02

301	153-0.8000002-0.1000000	3.70136921	0.0027502-0.0046188	1.0000000	0.594E+07
302	154-0.8000002-0.2000000	3.76594830	0.0019947-0.0046919	1.0000000	0.521E+07
303	155-0.8000002-0.3000001	3.74140835	0.0021075-0.0046767	1.0000000	0.492E+07
304	156-0.8000002-0.4000001	3.70886612	0.0042796-0.0047378	1.0000000	0.479E+07
305	157-0.8000002-0.5000001	3.66835785	0.0049574-0.0041987	1.0000000	0.468E+07
306	158-0.8000002-0.6000001	3.62175081	0.0016157 0.0012376	1.0000000	0.436E+07
307	160-0.5000002-0.1000000	3.65885540	-0.0014205-0.0002509	1.0000000	-0.345E-04
308	161-0.9000002-0.2000000	3.68654060	0.0020115 0.0005708	1.0000000	0.459E+07
309	162-0.9000002-0.3000001	3.66483307	0.0057648-0.0043888	1.0000000	0.838E-03
310	163-0.9000002-0.4000001	3.63512611	0.0067769-0.0034063	1.0000000	0.433E+07
					0.242E-03
					0.487E+07
					0.190E-01
					0.468E+07
					0.145E-01

END OF SKFM RAY TRACE.

TOTAL NUMBER OF RAYS TRACED = 310
 TOTAL NUMBER OF RAYS STRIKING IMAGE PLANE = 317
 1 IMAGE PLANE SPOT CLARAM ANALYSIS:

THICKNESS = 0.050000 U = 0.0 ALFAP = 0.0 R = 1.0000000

CENTROID: ZCENTR = 0.0 YCENTR = 0.0026398

STANDARD DEVIATIONS: SIGMAV = 0.0000121 SIGMAZ = 0.0000207

RMS SPCT SIZE: RMSRAD = 0.0057336

SPOT DIAGRAM ENERGY DENSITY VS. RADIUS FROM CENTROID:

124	RADIUS	FRACTION
1	0.0050000	0.6741935
2	0.0100000	0.9403871
3	0.0150000	0.5444161
4	0.0200000	0.9870967
5	0.0250000	1.0000000
6	0.0300000	0.9999999
7	0.0350000	1.0000000
8	0.0400000	1.0000000
9	0.0450000	1.0000000
10	0.0500000	1.0000000
11	0.0550000	1.0000000
12	0.0600000	1.0000000
13	0.0650000	1.0000000
14	0.0700000	1.0000000
15	0.0750000	1.0000000
16	0.0800000	1.0000000
17	0.0850000	1.0000000
18	0.0900000	1.0000000
19	0.0950000	1.0000000

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FILE: OUT 0 A NAVAL POSTGRADUATE SCHOOL

PAGE 001

GRIN PARAMETERS(2):

ALPHA = 0.7053979 BETA = 0.3222679 RADIUS = 1.00000 INCIDENT ANGLE = 0.0 ITERATIONS = 1008

EDGE THICKNESS = 0.050000 INDICES OF REFRACTION: N1 = 1.00000 N2 = 1.50000 N3 = 1.00000

FOCAL LENGTH FROM STATION ZERO = 4.00000 DELTA BETA = 0.00032

CENTER OF SYMMETRY = 0.07000 CHANGE IN N2(1) = 0.0 ALFA = 0.0

NOTE: X-COORDINATES HAS BEEN SHIFTED IN CASE=2 BY X2(K) IN CM, X2(K)=0.0 ETC.

J	E	X1	Y1	THETA	X2	Y2	PSI	PSIO	BETA	PP	12P	OF	12	ETA	T	11P	11	DYDXT
1	1.0000000	1.0000000	1.0564194	0.9828857	0.3222679	0.0831530	0.0553498	0.2391149	0.0500000	0.4908826	0.7853981	4.1020784						
2	1.9013081	0.0341403	0.7174545	2.0954809	2.1296225	1.4494554	1.4645472	0.2391236	0.0596354	0.4908826	0.7853981	4.1019230						
3	1.8993657	0.0344937	0.7170703	2.0955114	2.1302165	1.4494137	1.4631211	0.2397367	0.0602251	0.4908826	0.7853981	4.0910225						
4	1.8980656	0.0348420	0.7166854	2.0955412	2.1308086	1.4493720	1.4620752	0.2403867	0.0608078	0.4908826	0.7853981	4.0795240						
5	1.8965803	0.0352097	0.7163020	2.0955636	2.1313947	1.4493304	1.4609755	0.2410114	0.0613955	0.4908826	0.7853981	4.0685310						
6	1.8950795	0.0355791	0.7159175	2.0955851	2.1319842	1.4492888	1.4598750	0.2416589	0.0619768	0.4908826	0.7853981	4.0571966						
7	1.8935586	0.0359463	0.7155312	2.0956066	2.1325763	1.4492472	1.4587745	0.2422809	0.0625631	0.4908826	0.7853981	4.0463629						
8	1.8920377	0.0363107	0.7151449	2.0956281	2.1331724	1.4492056	1.4576740	0.2429341	0.0631440	0.4908826	0.7853981	4.0350447						
9	1.8904993	0.0366734	0.7147586	2.0956496	2.1337722	1.4491640	1.4565735	0.2435760	0.0637264	0.4908826	0.7853981	4.0239792						
10	1.8889415	0.0370353	0.7143723	2.0956711	2.1343740	1.4491224	1.4554730	0.2442124	0.0643013	0.4908826	0.7853981	4.0130653						
11	1.8873649	0.0373962	0.7139860	2.0956926	2.1349781	1.4490808	1.4543725	0.2448561	0.0648864	0.4908826	0.7853981	4.0019140						
12	1.8857713	0.0377561	0.7136000	2.0957141	2.1355841	1.4490392	1.4532720	0.2454939	0.0654680	0.4908826	0.7853981	3.9912586						
13	1.8841645	0.0381159	0.7132146	2.0957356	2.1361923	1.4489976	1.4521715	0.2461364	0.0660472	0.4908826	0.7853981	3.9804087						
14	1.8825476	0.0384758	0.7128291	2.0957571	2.1368024	1.4489560	1.4510710	0.2467768	0.0666207	0.4908826	0.7853981	3.9692622						
15	1.8809213	0.0388357	0.7124436	2.0957786	2.1374146	1.4489144	1.4500005	0.2474140	0.0671921	0.4908826	0.7853981	3.9584114						
16	1.8792851	0.0391956	0.7120581	2.0957999	2.1380288	1.4488728	1.4489290	0.2480493	0.0677654	0.4908826	0.7853981	3.9478601						
17	1.8776489	0.0395555	0.7116726	2.0958212	2.1386440	1.4488312	1.4478585	0.2486826	0.0683367	0.4908826	0.7853981	3.9376124						
18	1.8760127	0.0399154	0.7112871	2.0958425	2.1392602	1.4487896	1.4467880	0.2493140	0.0689059	0.4908826	0.7853981	3.9276659						
19	1.8743765	0.0402753	0.7109016	2.0958638	2.1398774	1.4487480	1.4457175	0.2499439	0.0694732	0.4908826	0.7853981	3.9180171						
20	1.8727403	0.0406352	0.7105161	2.0958851	2.1404956	1.4487064	1.4446470	0.2505728	0.0699995	0.4908826	0.7853981	3.9086659						
21	1.8711041	0.0409951	0.7101306	2.0959064	2.1411148	1.4486648	1.4435765	0.2512007	0.0705248	0.4908826	0.7853981	3.8996139						
22	1.8694679	0.0413550	0.7097451	2.0959277	2.1417350	1.4486232	1.4425060	0.2518276	0.0710498	0.4908826	0.7853981	3.8908602						
23	1.8678317	0.0417149	0.7093596	2.0959489	2.1423562	1.4485816	1.4414355	0.2524535	0.0715748	0.4908826	0.7853981	3.8824065						
24	1.8661955	0.0420748	0.7089741	2.0959702	2.1429784	1.4485400	1.4403650	0.2530784	0.0720998	0.4908826	0.7853981	3.8742528						
25	1.8645593	0.0424347	0.7085886	2.0959915	2.1436016	1.4484984	1.4392945	0.2537023	0.0726248	0.4908826	0.7853981	3.8663991						
26	1.8629231	0.0427946	0.7082031	2.0960128	2.1442248	1.4484568	1.4382240	0.2543252	0.0731498	0.4908826	0.7853981	3.8588454						
27	1.8612869	0.0431545	0.7078176	2.0960341	2.1448480	1.4484152	1.4371535	0.2549476	0.0736748	0.4908826	0.7853981	3.8515917						

28 0.9780834 0.9780830 1.0498634 0.9564699 0.1136357 0.0592786 0.0395382 0.2543571 0.0744550 0.4908826 0.7853981 3.6663259
29 0.9780838 0.9780834 1.0498638 0.9564703 0.1136361 0.0592791 0.0395386 0.2543575 0.0744554 0.4908830 0.7853985 3.6663263
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36 0.9780866 0.9780862 1.0498666 0.9564731 0.1136389 0.0592819 0.0395414 0.2543603 0.0744582 0.4908858 0.7854013 3.6663291
37 0.9780870 0.9780866 1.0498670 0.9564735 0.1136393 0.0592823 0.0395418 0.2543607 0.0744586 0.4908862 0.7854017 3.6663295
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1.0498778 0.9564843 0.1136501 0.0592931 0.0395526 0.2543715 0.0744694 0.4908970 0.7854125 3.6663403

64	0.94969231	0.94967646	0.94965050	0.94962454	0.94959858	0.94957262	0.94954666	0.94952070	0.94949474	0.94946878	0.94944282	0.94941686	0.94939090	0.94936494	0.94933898	0.94931302	0.94928706	0.94926110	0.94923514	0.94920918	0.94918322	0.94915726	0.94913130	0.94910534	0.94907938	0.94905342	0.94902746	0.94900150	0.94897554	0.94894958	0.94892362	0.94889766	0.94887170	0.94884574	0.94881978	0.94879382	0.94876786	0.94874190	0.94871594	0.94868998	0.94866402	0.94863806	0.94861210	0.94858614	0.94856018	0.94853422	0.94850826	0.94848230	0.94845634	0.94843038	0.94840442	0.94837846	0.94835250	0.94832654	0.94830058	0.94827462	0.94824866	0.94822270	0.94819674	0.94817078	0.94814482	0.94811886	0.94809290	0.94806694	0.94804098	0.94801502	0.94798906	0.94796310	0.94793714	0.94791118	0.94788522	0.94785926	0.94783330	0.94780734	0.94778138	0.94775542	0.94772946	0.94770350	0.94767754	0.94765158	0.94762562	0.94760000	0.94757404	0.94754808	0.94752212	0.94749616	0.94747020	0.94744424	0.94741828	0.94739232	0.94736636	0.94734040	0.94731444	0.94728848	0.94726252	0.94723656	0.94721060	0.94718464	0.94715868	0.94713272	0.94710676	0.94708080	0.94705484	0.94702888	0.94700292	0.94697696	0.94695100	0.94692504	0.94689908	0.94687312	0.94684716	0.94682120	0.94679524	0.94676928	0.94674332	0.94671736	0.94669140	0.94666544	0.94663948	0.94661352	0.94658756	0.94656160	0.94653564	0.94650968	0.94648372	0.94645776	0.94643180	0.94640584	0.94637988	0.94635392	0.94632796	0.94630200	0.94627604	0.94625008	0.94622412	0.94619816	0.94617220	0.94614624	0.94612028	0.94609432	0.94606836	0.94604240	0.94601644	0.94599048	0.94596452	0.94593856	0.94591260	0.94588664	0.94586068	0.94583472	0.94580876	0.94578280	0.94575684	0.94573088	0.94570492	0.94567896	0.94565300	0.94562704	0.94560108	0.94557512	0.94554916	0.94552320	0.94549724	0.94547128	0.94544532	0.94541936	0.94539340	0.94536744	0.94534148	0.94531552	0.94528956	0.94526360	0.94523764	0.94521168	0.94518572	0.94515976	0.94513380	0.94510784	0.94508188	0.94505592	0.94502996	0.94500400	0.94497804	0.94495208	0.94492612	0.94490016	0.94487420	0.94484824	0.94482228	0.94479632	0.94477036	0.94474440	0.94471844	0.94469248	0.94466652	0.94464056	0.94461460	0.94458864	0.94456268	0.94453672	0.94451076	0.94448480	0.94445884	0.94443288	0.94440692	0.94438096	0.94435500	0.94432904	0.94430308	0.94427712	0.94425116	0.94422520	0.94419924	0.94417328	0.94414732	0.94412136	0.94409540	0.94406944	0.94404348	0.94401752	0.94399156	0.94396560	0.94393964	0.94391368	0.94388772	0.94386176	0.94383580	0.94380984	0.94378388	0.94375792	0.94373196	0.94370600	0.94368004	0.94365408	0.94362812	0.94360216	0.94357620	0.94355024	0.94352428	0.94349832	0.94347236	0.94344640	0.94342044	0.94339448	0.94336852	0.94334256	0.94331660	0.94329064	0.94326468	0.94323872	0.94321276	0.94318680	0.94316084	0.94313488	0.94310892	0.94308296	0.94305700	0.94303104	0.94300508	0.94297912	0.94295316	0.94292720	0.94290124	0.94287528	0.94284932	0.94282336	0.94279740	0.94277144	0.94274548	0.94271952	0.94269356	0.94266760	0.9
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100	0.9210636	0.9210076	1.0301469	0.8881770	0.2908166	-0.3107667	-0.0071179	0.3013065	0.1141216	0.4908026	0.7053901	3.2109222
101	0.9201032	0.9203010	1.0300531	0.8947305	0.2902407	-0.0118637	-0.0059084	0.3021603	0.1146255	0.4908026	0.7053901	3.2081633
102	0.9195728	0.9195274	1.0297545	0.8928329	0.2894711	-0.0124190	-0.0061130	0.3008769	0.1151344	0.4908026	0.7053901	3.1998644
103	0.9189032	0.9189358	1.0294641	0.8912716	0.2886937	-0.0112807	-0.0063553	0.3025576	0.1158112	0.4908026	0.7053901	3.2048082
104	0.9179442	0.9179712	1.0291703	0.8898314	0.2879178	-0.0110610	-0.0073562	0.3036637	0.1162098	0.4908026	0.7053901	3.1819148
105	0.9167106	0.9167145	1.0287539	0.8883925	0.2869810	-0.0115081	-0.0080049	0.3040795	0.1168050	0.4908026	0.7053901	3.1866236
106	0.9146012	0.9146108	1.0281745	0.8862529	0.2857043	-0.0115695	-0.0082433	0.3053439	0.1173166	0.4908026	0.7053901	3.1836758
107	0.9145351	0.9145483	1.0280573	0.8845541	0.2848306	-0.0117140	-0.0083983	0.3060934	0.1177413	0.4908026	0.7053901	3.1643019
108	0.9145722	0.9145767	1.0279625	0.8830812	0.2839923	-0.0110819	-0.0083977	0.3067841	0.1182536	0.4908026	0.7053901	3.1567116
109	0.9141437	0.9141471	1.0278842	0.8816517	0.2831731	-0.0113731	-0.0083935	0.3077123	0.1187311	0.4908026	0.7053901	3.1465645
110	0.9130471	0.9130526	1.0275846	0.8796533	0.2817119	-0.0116118	-0.0083935	0.3086862	0.1191721	0.4908026	0.7053901	3.1330148
111	0.9127219	0.9127252	1.0274915	0.8783403	0.2807098	-0.0120316	-0.0083945	0.3102830	0.1195805	0.4908026	0.7053901	3.1187019
112	0.9118034	0.9118179	1.0270803	0.8768929	0.2787801	-0.0123516	-0.0083944	0.3108965	0.1201208	0.4908026	0.7053901	3.1143370
113	0.9110456	0.9110405	1.0264797	0.8758242	0.2764093	-0.0124493	-0.0083935	0.3111100	0.1206665	0.4908026	0.7053901	3.1077052
114	0.9102948	0.9102916	1.0261019	0.8748557	0.2748877	-0.0125360	-0.0083948	0.3120005	0.1211528	0.4908026	0.7053901	3.1004410
115	0.9092801	0.9092915	1.0257280	0.8739082	0.2736290	-0.0125547	-0.0083949	0.3127784	0.1216552	0.4908026	0.7053901	3.0927334
116	0.9081743	0.9081751	1.0253367	0.8730492	0.2724530	-0.0125716	-0.0083946	0.3134814	0.1221496	0.4908026	0.7053901	3.0847330
117	0.9079780	0.9079780	1.0252638	0.8721113	0.2719266	-0.0125906	-0.0083936	0.3142436	0.1226454	0.4908026	0.7053901	3.0768013
118	0.9071703	0.9071703	1.0247586	0.8711680	0.2704815	-0.0129006	-0.0083936	0.3149826	0.1231424	0.4908026	0.7053901	3.0690832
119	0.9064395	0.9064391	1.0246575	0.8702873	0.2696819	-0.0130420	-0.0083948	0.3157446	0.1236356	0.4908026	0.7053901	3.0611620
120	0.9056753	0.9056749	1.0243444	0.8693923	0.2684224	-0.0132308	-0.0125357	0.3165321	0.1241281	0.4908026	0.7053901	3.0530138
121	0.9044347	0.9044381	1.0240337	0.8684897	0.2671568	-0.0133651	-0.0122319	0.3171956	0.1246216	0.4908026	0.7053901	3.0455809
122	0.9034125	0.9034125	1.0237293	0.8675967	0.2658935	-0.0134941	-0.0122913	0.3178956	0.1251161	0.4908026	0.7053901	3.0379763
123	0.9031605	0.9031601	1.0236203	0.8666547	0.2649312	-0.0135211	-0.0122613	0.3187744	0.1256040	0.4908026	0.7053901	3.0300293
124	0.9023144	0.9023134	1.0234301	0.8657114	0.2640300	-0.0135766	-0.0122543	0.3181801	0.1262669	0.4908026	0.7053901	3.0346813
125	0.9017128	0.9017128	1.0232304	0.8645904	0.2631142	-0.0136435	-0.0122543	0.3185521	0.1266455	0.4908026	0.7053901	3.0190935
126	0.9007400	0.9007420	1.0230735	0.8635243	0.2622423	-0.0137243	-0.0122615	0.3190098	0.1272769	0.4908026	0.7053901	3.0215454
127	0.9001682	0.9001674	1.0229176	0.8624029	0.2613704	-0.0137919	-0.0122693	0.3212691	0.1276387	0.4908026	0.7053901	3.0048208
128	0.8994911	0.8994911	1.0227617	0.8611748	0.2605003	-0.0138619	-0.0122752	0.3203963	0.1282274	0.4908026	0.7053901	3.0018802
129	0.8988155	0.8988155	1.0226058	0.8600033	0.2596329	-0.0139300	-0.0122761	0.3215301	0.1287973	0.4908026	0.7053901	3.0025053
130	0.8981470	0.8981466	1.0224499	0.8587518	0.2587659	-0.0139954	-0.0122827	0.3227102	0.1293678	0.4908026	0.7053901	2.9958076
131	0.8974773	0.8974759	1.0222940	0.8575000	0.2579000	-0.0140614	-0.0122894	0.3238912	0.1299385	0.4908026	0.7053901	2.9891099
132	0.8968095	0.8968081	1.0221381	0.8562482	0.2570341	-0.0141274	-0.0122961	0.3250722	0.1305092	0.4908026	0.7053901	2.9824122
133	0.8961417	0.8961403	1.0219822	0.8550000	0.2561682	-0.0141934	-0.0123028	0.3262532	0.1310799	0.4908026	0.7053901	2.9757145
134	0.8954739	0.8954725	1.0218263	0.8537518	0.2553023	-0.0142594	-0.0123095	0.3274342	0.1316506	0.4908026	0.7053901	2.9690168
135	0.8948061	0.8948047	1.0216704	0.8525036	0.2544364	-0.0143254	-0.0123162	0.3286152	0.1322213	0.4908026	0.7053901	2.9623191

136	0.789203647	0.032689232	0.01935319	0.05429167	0.27910750	-0.34403737	0.01337556	0.3261802	0.1322819	0.4908826	0.7853981	2.9562805
137	1.749320417	0.08303415	1.01900319	2.08527739	2.77877172	-0.06400244	1.3130844	0.3208301	0.1327803	0.4908826	0.7853981	2.9499664
138	0.88125801	0.08325576	1.01871917	2.08523339	2.421745	-0.08505440	0.3129963	0.3275225	0.1332718	0.4908826	0.7853981	2.9432811
139	0.8604669	0.08341154	1.01844210	2.08513944	2.1627547	-0.08097326	0.3130406	0.3281805	0.1337683	0.4908826	0.7853981	2.9369164
140	1.88347897	0.08371714	1.01818838	2.08504478	2.1778200	-0.13488416	0.3097420	0.3288558	0.1342612	0.4908826	0.7853981	2.9304295
141	0.94849167	0.08391393	1.01776631	2.08492502	2.1933380	-0.05033400	0.3064307	0.3295425	0.1347511	0.4908826	0.7853981	2.9238858
142	0.98344711	0.08415005	1.01730327	2.08485476	2.1936977	-0.05302537	0.3053412	0.3302144	0.1352426	0.4908826	0.7853981	2.9174547
143	1.63197927	0.08436119	0.66726370	2.08479570	2.1640891	-0.37935246	0.3040360	0.3308725	0.1357352	0.4908826	0.7853981	2.9112072
144	1.65004926	0.08452233	0.66726499	2.08466015	2.1844664	-0.37850334	0.3035925	0.3315332	0.1362275	0.4908826	0.7853981	2.9049587
145	1.68937331	0.08455451	0.66764706	2.08459303	2.1648536	-0.37696700	0.3047005	0.3321666	0.1367198	0.4908826	0.7853981	2.8987103
146	1.69757443	0.08459473	0.66715554	2.08456412	2.1852334	-0.37593965	0.3037644	0.3328744	0.1372064	0.4908826	0.7853981	2.8923392
147	1.66665619	0.08461096	0.66710420	2.08453902	2.1855903	-0.37502546	0.3034909	0.3335548	0.1376961	0.4908826	0.7853981	2.8859892
148	1.68445901	0.08466717	0.66066644	2.08449612	2.1860018	-0.37419665	0.3030249	0.3342295	0.1381829	0.4908826	0.7853981	2.8797064
149	1.68311739	0.08470335	0.66681721	2.08442005	2.1752705	-0.37359907	0.3027433	0.3348945	0.1386711	0.4908826	0.7853981	2.8735294
150	1.68179308	0.08473950	0.65981478	2.08438030	2.1762988	-0.37302743	0.3024932	0.3355529	0.1391600	0.4908826	0.7853981	2.8674545
151	1.68015286	0.08477572	0.65949342	2.08434036	2.1771561	-0.37249974	0.3022913	0.3362193	0.1396467	0.4908826	0.7853981	2.8613214
152	1.67860804	0.08481199	0.65944317	2.08430082	2.1781310	-0.37196172	0.3021257	0.3369077	0.1401295	0.4908826	0.7853981	2.8550091
153	1.67712127	0.08484814	0.65940288	2.08426128	2.1791916	-0.37140361	0.3021286	0.3375842	0.1406139	0.4908826	0.7853981	2.8488216
154	1.67567402	0.08488437	0.65936270	2.08422176	2.1803471	-0.37091330	0.3020948	0.3382453	0.1410997	0.4908826	0.7853981	2.8428164
155	1.67425382	0.08492053	0.65770025	2.08418374	2.1815352	-0.37040493	0.3021432	0.3389192	0.1415882	0.4908826	0.7853981	2.8367071
156	1.67278444	0.08495679	0.65732704	2.08414530	2.1827037	-0.36993609	0.3021250	0.3395879	0.1420649	0.4908826	0.7853981	2.8306694
157	1.67130859	0.08499299	0.65712513	2.08410693	2.1838431	-0.36947015	0.3021453	0.3402533	0.1425490	0.4908826	0.7853981	2.8246841
158	1.669824											

172	0.6041446	0.0641441	1.0075378	0.8205529	0.2675974	0.0813587	0.0542059	0.3489561	0.1499018	0.4908826	0.7853981	2.7484150
173	0.6033481	0.0633476	1.0075378	0.8195181	0.2675974	0.0813587	0.0542059	0.3495919	0.1503805	0.4908826	0.7853981	2.7429867
174	0.6025516	0.0625511	1.0075378	0.8185181	0.2675974	0.0813587	0.0542059	0.3502559	0.1508535	0.4908826	0.7853981	2.7373362
175	0.6017551	0.0617546	1.0075378	0.8175181	0.2675974	0.0813587	0.0542059	0.3509031	0.1513284	0.4908826	0.7853981	2.7318506
176	0.6009586	0.0609581	1.0075378	0.8165181	0.2675974	0.0813587	0.0542059	0.3515503	0.1518028	0.4908826	0.7853981	2.7263823
177	0.6001621	0.0601616	1.0075378	0.8155181	0.2675974	0.0813587	0.0542059	0.3521885	0.1522788	0.4908826	0.7853981	2.7210102
178	0.5993656	0.0593651	1.0075378	0.8145181	0.2675974	0.0813587	0.0542059	0.3528382	0.1527513	0.4908826	0.7853981	2.7155590
179	0.5985691	0.0585686	1.0075378	0.8135181	0.2675974	0.0813587	0.0542059	0.3534907	0.1532233	0.4908826	0.7853981	2.7101049
180	0.5977726	0.0577721	1.0075378	0.8125181	0.2675974	0.0813587	0.0542059	0.3541427	0.1536955	0.4908826	0.7853981	2.7046738
181	0.5969761	0.0569756	1.0075378	0.8115181	0.2675974	0.0813587	0.0542059	0.3547944	0.1541672	0.4908826	0.7853981	2.6993046
182	0.5961796	0.0561791	1.0075378	0.8105181	0.2675974	0.0813587	0.0542059	0.3554464	0.1546388	0.4908826	0.7853981	2.6939354
183	0.5953831	0.0553826	1.0075378	0.8095181	0.2675974	0.0813587	0.0542059	0.3560984	0.1551105	0.4908826	0.7853981	2.6885662
184	0.5945866	0.0545861	1.0075378	0.8085181	0.2675974	0.0813587	0.0542059	0.3567504	0.1555822	0.4908826	0.7853981	2.6831970
185	0.5937901	0.0537896	1.0075378	0.8075181	0.2675974	0.0813587	0.0542059	0.3574024	0.1560539	0.4908826	0.7853981	2.6778278
186	0.5929936	0.0529931	1.0075378	0.8065181	0.2675974	0.0813587	0.0542059	0.3580544	0.1565256	0.4908826	0.7853981	2.6724586
187	0.5921971	0.0521966	1.0075378	0.8055181	0.2675974	0.0813587	0.0542059	0.3587064	0.1569973	0.4908826	0.7853981	2.6670894
188	0.5914006	0.0514001	1.0075378	0.8045181	0.2675974	0.0813587	0.0542059	0.3593584	0.1574690	0.4908826	0.7853981	2.6617202
189	0.5906041	0.0506036	1.0075378	0.8035181	0.2675974	0.0813587	0.0542059	0.3599999	0.1579407	0.4908826	0.7853981	2.6563510
190	0.5898076	0.0498071	1.0075378	0.8025181	0.2675974	0.0813587	0.0542059	0.3606419	0.1584124	0.4908826	0.7853981	2.6509818
191	0.5890111	0.0490106	1.0075378	0.8015181	0.2675974	0.0813587	0.0542059	0.3612839	0.1588841	0.4908826	0.7853981	2.6456126
192	0.5882146	0.0482141	1.0075378	0.8005181	0.2675974	0.0813587	0.0542059	0.3619259	0.1593558	0.4908826	0.7853981	2.6402434
193	0.5874181	0.0474176	1.0075378	0.7995181	0.2675974	0.0813587	0.0542059	0.3625679	0.1598275	0.4908826	0.7853981	2.6348742
194	0.5866216	0.0466211	1.0075378	0.7985181	0.2675974	0.0813587	0.0542059	0.3632099	0.1602992	0.4908826	0.7853981	2.6295050
195	0.5858251	0.0458246	1.0075378	0.7975181	0.2675974	0.0813587	0.0542059	0.3638519	0.1607709	0.4908826	0.7853981	2.6241358
196	0.5850286	0.0450281	1.0075378	0.7965181	0.2675974	0.0813587	0.0542059	0.3644939	0.1612426	0.4908826	0.7853981	2.6187666
197	0.5842321	0.0442316	1.0075378	0.7955181	0.2675974	0.0813587	0.0542059	0.3651359	0.1617143	0.4908826	0.7853981	2.6133974
198	0.5834356	0.0434351	1.0075378	0.7945181	0.2675974	0.0813587	0.0542059	0.3657779	0.1621860	0.4908826	0.7853981	2.6080282
199	0.5826391	0.0426386	1.0075378	0.7935181	0.2675974	0.0813587	0.0542059	0.3664199	0.1626577	0.4908826	0.7853981	2.6026590
200	0.5818426	0.0418421	1.0075378	0.7925181	0.2675974	0.0813587	0.0542059	0.3670619	0.1631294	0.4908826	0.7853981	2.5972898
201	0.5810461	0.0410456	1.0075378	0.7915181	0.2675974	0.0813587	0.0542059	0.3677039	0.1636011	0.4908826	0.7853981	2.5919206
202	0.5802496	0.0402491	1.0075378	0.7905181	0.2675974	0.0813587	0.0542059	0.3683459	0.1640728	0.4908826	0.7853981	2.5865514
203	0.5794531	0.0394526	1.0075378	0.7895181	0.2675974	0.0813587	0.0542059	0.3689879	0.1645445	0.4908826	0.7853981	2.5811822
204	0.5786566	0.0386561	1.0075378	0.7885181	0.2675974	0.0813587	0.0542059	0.3696299	0.1650162	0.4908826	0.7853981	2.5758130
205	0.5778601	0.0378596	1.0075378	0.7875181	0.2675974	0.0813587	0.0542059	0.3702719	0.1654879	0.4908826	0.7853981	2.5704438
206	0.5770636	0.0370631	1.0075378	0.7865181	0.2675974	0.0813587	0.0542059	0.3709139	0.1659596	0.4908826	0.7853981	2.5650746
207	0.5762671	0.0362666	1.0075378	0.7855181	0.2675974	0.0813587	0.0542059	0.3715559	0.1664313	0.4908826	0.7853981	2.5597054

208	0.8955176	0.1038121	0.9949206	0.1864629	0.2504080	-0.1161709	-0.3735533	0.3722588	0.1666694	0.4908826	0.7853981	2.5610542
209	0.8437221	0.0693266	0.9352546	0.0190450	0.2303443	-0.1171399	-0.3730919	0.3729081	0.1671227	0.4908826	0.7853981	2.5561543
210	0.8809234	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3735515	0.1675773	0.4908826	0.7853981	2.5513153
211	0.8901249	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3742033	0.1680305	0.4908826	0.7853981	2.5464287
212	0.8921336	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3748522	0.1684840	0.4908826	0.7853981	2.5415802
213	0.8941423	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3754954	0.1689363	0.4908826	0.7853981	2.5367899
214	0.8961510	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3761293	0.1693908	0.4908826	0.7853981	2.5320845
215	0.8981600	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3767810	0.1698452	0.4908826	0.7853981	2.5272627
216	0.8991690	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3774321	0.1702990	0.4908826	0.7853981	2.5224400
217	0.9001780	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3780817	0.1707517	0.4908826	0.7853981	2.5175754
218	0.9011870	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3787303	0.1712042	0.4908826	0.7853981	2.5127108
219	0.9021960	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3793789	0.1716567	0.4908826	0.7853981	2.5078462
220	0.9032050	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3800275	0.1721092	0.4908826	0.7853981	2.5029816
221	0.9042140	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3806761	0.1725617	0.4908826	0.7853981	2.4981170
222	0.9052230	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3813247	0.1730142	0.4908826	0.7853981	2.4932524
223	0.9062320	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3819733	0.1734667	0.4908826	0.7853981	2.4883878
224	0.9072410	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3826219	0.1739192	0.4908826	0.7853981	2.4835232
225	0.9082500	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3832705	0.1743717	0.4908826	0.7853981	2.4786586
226	0.9092590	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3839191	0.1748242	0.4908826	0.7853981	2.4737940
227	0.9102680	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3845677	0.1752767	0.4908826	0.7853981	2.4689294
228	0.9112770	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3852163	0.1757292	0.4908826	0.7853981	2.4640648
229	0.9122860	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3858649	0.1761817	0.4908826	0.7853981	2.4592002
230	0.9132950	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3865135	0.1766342	0.4908826	0.7853981	2.4543356
231	0.9143040	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3871621	0.1770867	0.4908826	0.7853981	2.4494710
232	0.9153130	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3878107	0.1775392	0.4908826	0.7853981	2.4446064
233	0.9163220	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3884593	0.1779917	0.4908826	0.7853981	2.4397418
234	0.9173310	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3891079	0.1784442	0.4908826	0.7853981	2.4348772
235	0.9183400	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3897565	0.1788967	0.4908826	0.7853981	2.4300126
236	0.9193490	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3904051	0.1793492	0.4908826	0.7853981	2.4251480
237	0.9203580	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3910537	0.1798017	0.4908826	0.7853981	2.4202834
238	0.9213670	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3917023	0.1802542	0.4908826	0.7853981	2.4154188
239	0.9223760	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3923509	0.1807067	0.4908826	0.7853981	2.4105542
240	0.9233850	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3930000	0.1811592	0.4908826	0.7853981	2.4056896
241	0.9243940	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3936486	0.1816117	0.4908826	0.7853981	2.4008250
242	0.9254030	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3942972	0.1820642	0.4908826	0.7853981	2.3959604
243	0.9264120	0.0395256	0.9635028	0.0635028	0.2354733	-0.1173290	-0.3739439	0.3949458	0.1825167	0.4908826	0.7853981	2.3910958

214

280	0.776779	0.776775	0.967196	0.719935	0.233088	0.184145	0.122358	0.417183	0.198119	0.490826	0.785398	2.256325
281	0.776775	0.776771	0.966769	0.719931	0.233084	0.184141	0.122354	0.417179	0.198115	0.490822	0.785394	2.256321
282	0.776771	0.776767	0.966360	0.719927	0.233080	0.184137	0.122350	0.417175	0.198111	0.490818	0.785390	2.256317
283	0.776767	0.776763	0.965951	0.719923	0.233076	0.184133	0.122346	0.417171	0.198107	0.490814	0.785386	2.256313
284	0.776763	0.776759	0.965542	0.719919	0.233072	0.184129	0.122342	0.417167	0.198103	0.490810	0.785382	2.256309
285	0.776759	0.776755	0.965133	0.719915	0.233068	0.184125	0.122338	0.417163	0.198099	0.490806	0.785378	2.256305
286	0.776755	0.776751	0.964724	0.719911	0.233064	0.184121	0.122334	0.417159	0.198095	0.490802	0.785374	2.256301
287	0.776751	0.776747	0.964315	0.719907	0.233060	0.184117	0.122330	0.417155	0.198091	0.490798	0.785370	2.256297
288	0.776747	0.776743	0.963906	0.719903	0.233056	0.184113	0.122326	0.417151	0.198087	0.490794	0.785366	2.256293
289	0.776743	0.776739	0.963497	0.719899	0.233052	0.184109	0.122322	0.417147	0.198083	0.490790	0.785362	2.256289
290	0.776739	0.776735	0.963088	0.719895	0.233048	0.184105	0.122318	0.417143	0.198079	0.490786	0.785358	2.256285
291	0.776735	0.776731	0.962679	0.719891	0.233044	0.184101	0.122314	0.417139	0.198075	0.490782	0.785354	2.256281
292	0.776731	0.776727	0.962270	0.719887	0.233040	0.184097	0.122310	0.417135	0.198071	0.490778	0.785350	2.256277
293	0.776727	0.776723	0.961861	0.719883	0.233036	0.184093	0.122306	0.417131	0.198067	0.490774	0.785346	2.256273
294	0.776723	0.776719	0.961452	0.719879	0.233032	0.184089	0.122302	0.417127	0.198063	0.490770	0.785342	2.256269
295	0.776719	0.776715	0.961043	0.719875	0.233028	0.184085	0.122298	0.417123	0.198059	0.490766	0.785338	2.256265
296	0.776715	0.776711	0.960634	0.719871	0.233024	0.184081	0.122294	0.417119	0.198055	0.490762	0.785334	2.256261
297	0.776711	0.776707	0.960225	0.719867	0.233020	0.184077	0.122290	0.417115	0.198051	0.490758	0.785330	2.256257
298	0.776707	0.776703	0.959816	0.719863	0.233016	0.184073	0.122286	0.417111	0.198047	0.490754	0.785326	2.256253
299	0.776703	0.776699	0.959407	0.719859	0.233012	0.184069	0.122282	0.417107	0.198043	0.490750	0.785322	2.256249
300	0.776699	0.776695	0.958998	0.719855	0.233008	0.184065	0.122278	0.417103	0.198039	0.490746	0.785318	2.256245
301	0.776695	0.776691	0.958589	0.719851	0.233004	0.184061	0.122274	0.417099	0.198035	0.490742	0.785314	2.256241
302	0.776691	0.776687	0.958180	0.719847	0.233000	0.184057	0.122270	0.417095	0.198031	0.490738	0.785310	2.256237
303	0.776687	0.776683	0.957771	0.719843	0.232996	0.184053	0.122266	0.417091	0.198027	0.490734	0.785306	2.256233
304	0.776683	0.776679	0.957362	0.719839	0.232992	0.184049	0.122262	0.417087	0.198023	0.490730	0.785302	2.256229
305	0.776679	0.776675	0.956953	0.719835	0.232988	0.184045	0.122258	0.417083	0.198019	0.490726	0.785298	2.256225
306	0.776675	0.776671	0.956544	0.719831	0.232984	0.184041	0.122254	0.417079	0.198015	0.490722	0.785294	2.256221
307	0.776671	0.776667	0.956135	0.719827	0.232980	0.184037	0.122250	0.417075	0.198011	0.490718	0.785290	2.256217
308	0.776667	0.776663	0.955726	0.719823	0.232976	0.184033	0.122246	0.417071	0.198007	0.490714	0.785286	2.256213
309	0.776663	0.776659	0.955317	0.719819	0.232972	0.184029	0.122242	0.417067	0.198003	0.490710	0.785282	2.256209
310	0.776659	0.776655	0.954908	0.719815	0.232968	0.184025	0.122238	0.417063	0.198000	0.490706	0.785278	2.256205
311	0.776655	0.776651	0.954499	0.719811	0.232964	0.184021	0.122234	0.417059	0.197996	0.490702	0.785274	2.256201
312	0.776651	0.776647	0.954090	0.719807	0.232960	0.184017	0.122230	0.417055	0.197992	0.490698	0.785270	2.256197
313	0.776647	0.776643	0.953681	0.719803	0.232956	0.184013	0.122226	0.417051	0.197988	0.490694	0.785266	2.256193
314	0.776643	0.776639	0.953272	0.719799	0.232952	0.184009	0.122222	0.417047	0.197984	0.490690	0.785262	2.256189
315	0.776639	0.776635	0.952863	0.719795	0.232948	0.184005	0.122218	0.417043	0.197980	0.490686	0.785258	2.256185

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496	0.59927104	0.59927101	0.8623071	0.5192814	0.1640115	0.3817554	0.2533947	0.5657568	0.2769298	0.4908826	0.7853981	1.6466436
497	0.59842103	0.59842101	0.8617397	0.5180432	0.1636278	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
498	0.59803206	0.59803206	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
499	0.59764619	0.59764619	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
500	0.59726032	0.59726032	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
501	0.59687445	0.59687445	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
502	0.59648858	0.59648858	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
503	0.59610271	0.59610271	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
504	0.59571684	0.59571684	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
505	0.59533097	0.59533097	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
506	0.59494510	0.59494510	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
507	0.59455923	0.59455923	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
508	0.59417336	0.59417336	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
509	0.59378749	0.59378749	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
510	0.59340162	0.59340162	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
511	0.59301575	0.59301575	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
512	0.59262988	0.59262988	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
513	0.59224401	0.59224401	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
514	0.59185814	0.59185814	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
515	0.59147227	0.59147227	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
516	0.59108640	0.59108640	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
517	0.59070053	0.59070053	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
518	0.59031466	0.59031466	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
519	0.58992879	0.58992879	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
520	0.58954292	0.58954292	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
521	0.58915705	0.58915705	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
522	0.58877118	0.58877118	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
523	0.58838531	0.58838531	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
524	0.58800044	0.58800044	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
525	0.58761457	0.58761457	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
526	0.58722870	0.58722870	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
527	0.58684283	0.58684283	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
528	0.58645696	0.58645696	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
529	0.58607109	0.58607109	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
530	0.58568522	0.58568522	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284
531	0.58529935	0.58529935	0.8617397	0.5179086	0.1633320	0.3817692	0.2533947	0.5663373	0.2752258	0.4908826	0.7853981	1.6445284

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715	0-4045133	0-4045133	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6608520	0-3269301	0-4908826	0-7853981	1-2882206
716	0-4035771	0-4035771	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6613381	0-3271261	0-4908826	0-7853981	1-2880321
717	0-4026421	0-4026421	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6618266	0-3273014	0-4908826	0-7853981	1-2878370
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720	0-3998365	0-3998365	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6632798	0-3278302	0-4908826	0-7853981	1-2872517
721	0-3989013	0-3989013	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6637642	0-3280058	0-4908826	0-7853981	1-2870566
722	0-3979661	0-3979661	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6642485	0-3281814	0-4908826	0-7853981	1-2868615
723	0-3970309	0-3970309	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6647329	0-3283570	0-4908826	0-7853981	1-2866664
724	0-3960957	0-3960957	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6652177	0-3285326	0-4908826	0-7853981	1-2864713
725	0-3951605	0-3951605	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6657021	0-3287082	0-4908826	0-7853981	1-2862762
726	0-3942253	0-3942253	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6661865	0-3288838	0-4908826	0-7853981	1-2860811
727	0-3932901	0-3932901	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6666709	0-3290594	0-4908826	0-7853981	1-2858860
728	0-3923549	0-3923549	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6671553	0-3292350	0-4908826	0-7853981	1-2856909
729	0-3914197	0-3914197	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6676397	0-3294106	0-4908826	0-7853981	1-2854958
730	0-3904845	0-3904845	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6681241	0-3295862	0-4908826	0-7853981	1-2853007
731	0-3895493	0-3895493	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6686085	0-3297618	0-4908826	0-7853981	1-2851056
732	0-3886141	0-3886141	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6690929	0-3299374	0-4908826	0-7853981	1-2849105
733	0-3876789	0-3876789	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6695773	0-3301130	0-4908826	0-7853981	1-2847154
734	0-3867437	0-3867437	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6700617	0-3302886	0-4908826	0-7853981	1-2845203
735	0-3858085	0-3858085	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6705461	0-3304642	0-4908826	0-7853981	1-2843252
736	0-3848733	0-3848733	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6710305	0-3306398	0-4908826	0-7853981	1-2841301
737	0-3839381	0-3839381	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6715149	0-3308154	0-4908826	0-7853981	1-2839350
738	0-3829929	0-3829929	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6719993	0-3309910	0-4908826	0-7853981	1-2837399
739	0-3820577	0-3820577	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6724837	0-3311666	0-4908826	0-7853981	1-2835448
740	0-3811225	0-3811225	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6729681	0-3313422	0-4908826	0-7853981	1-2833497
741	0-3801873	0-3801873	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6734525	0-3315178	0-4908826	0-7853981	1-2831546
742	0-3792521	0-3792521	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6739369	0-3316934	0-4908826	0-7853981	1-2829595
743	0-3783169	0-3783169	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6744213	0-3318690	0-4908826	0-7853981	1-2827644
744	0-3773817	0-3773817	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6749057	0-3320446	0-4908826	0-7853981	1-2825693
745	0-3764465	0-3764465	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6753901	0-3322202	0-4908826	0-7853981	1-2823742
746	0-3755113	0-3755113	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6758745	0-3323958	0-4908826	0-7853981	1-2821791
747	0-3745761	0-3745761	0-3302601	0-3160697	0-3140642	0-4700966	0-5652915	0-3651462	0-6763589	0-3325714	0-4908826	0-7853981	1-2819840

748	0.37733449	0.35133446	0.49433313	0.37971460	0.08344445	0.53300919	0.38817797	0.67045336	0.33253172	0.44908826	0.7853981	1.22456207
749	0.37223991	0.08723366	0.49073366	0.37571175	0.08313835	0.53806819	0.38225547	0.3769316	0.3326444	0.44908826	0.7853981	1.2444010
750	0.37714554	0.37144332	0.68079312	0.37471786	0.08292027	0.53915546	0.37872591	0.6714014	0.3328547	0.44908826	0.7853981	1.2432032
751	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2415949
752	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2408018
753	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2396049
754	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2384157
755	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2372169
756	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2360325
757	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2348394
758	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2336607
759	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2324839
760	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2312975
761	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2301254
762	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2289371
763	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2277708
764	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2265597
765	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2254429
766	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2242765
767	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2231131
768	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2219448
769	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2207861
770	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2196350
771	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2184820
772	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2173223
773	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2161732
774	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2150307
775	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2138853
776	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2127476
777	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2116070
778	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2104692
779	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2093325
780	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2081965
781	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2070665
782	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2059331
783	0.37203772	0.35266034	0.36818897	0.37157792	0.5002277	0.53808219	0.37921792	0.6714014	0.3328547	0.44908826	0.7853981	1.2048159

784	0.3387312	0.3387310	0.6620584	0.2405296	0.0719350	0.6212952	0.3385248	0.6932302	0.3379112	0.4908826	0.7853981	1.2036858
785	0.4641876	0.3377594	0.3174539	2.1505550	2.5229323	0.7705007	0.5408443	0.6936890	0.3380504	0.4908826	0.7853981	1.2025023
786	0.6623698	0.3375213	0.3165438	2.1525170	2.5102411	0.7622378	0.5989802	0.6941451	0.3381946	0.4908826	0.7853981	1.2014475
787	0.6625055	0.3375904	0.3166313	2.1535505	2.5051355	0.7622378	0.5989802	0.6946029	0.3383256	0.4908826	0.7853981	1.2003298
788	0.6587293	0.3375813	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6949063	0.3384616	0.4908826	0.7853981	1.1992073
789	0.6564691	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6952153	0.3385974	0.4908826	0.7853981	1.1980849
790	0.6539317	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6955153	0.3387350	0.4908826	0.7853981	1.1969681
791	0.6514621	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6958153	0.3388708	0.4908826	0.7853981	1.1958538
792	0.6490114	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6961153	0.3390056	0.4908826	0.7853981	1.1947365
793	0.6465611	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6964153	0.3391404	0.4908826	0.7853981	1.1936179
794	0.6441109	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6967153	0.3392752	0.4908826	0.7853981	1.1925031
795	0.6416606	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6970153	0.3394100	0.4908826	0.7853981	1.1913843
796	0.6392103	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6973153	0.3395448	0.4908826	0.7853981	1.1902643
797	0.6367600	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6976153	0.3396796	0.4908826	0.7853981	1.1891443
798	0.6343097	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6979153	0.3398144	0.4908826	0.7853981	1.1880243
799	0.6318594	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6982153	0.3399492	0.4908826	0.7853981	1.1869043
800	0.6294091	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6985153	0.3400840	0.4908826	0.7853981	1.1857843
801	0.6269588	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6988153	0.3402188	0.4908826	0.7853981	1.1846643
802	0.6245085	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6991153	0.3403536	0.4908826	0.7853981	1.1835443
803	0.6220582	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6994153	0.3404884	0.4908826	0.7853981	1.1824243
804	0.6196079	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.6997153	0.3406232	0.4908826	0.7853981	1.1813043
805	0.6171576	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7000153	0.3407580	0.4908826	0.7853981	1.1801843
806	0.6147073	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7003153	0.3408928	0.4908826	0.7853981	1.1790643
807	0.6122570	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7006153	0.3410276	0.4908826	0.7853981	1.1779443
808	0.6098067	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7009153	0.3411624	0.4908826	0.7853981	1.1768243
809	0.6073564	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7012153	0.3412972	0.4908826	0.7853981	1.1757043
810	0.6049061	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7015153	0.3414320	0.4908826	0.7853981	1.1745843
811	0.6024558	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7018153	0.3415668	0.4908826	0.7853981	1.1734643
812	0.6000055	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7021153	0.3417016	0.4908826	0.7853981	1.1723443
813	0.5975552	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7024153	0.3418364	0.4908826	0.7853981	1.1712243
814	0.5951049	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7027153	0.3419712	0.4908826	0.7853981	1.1701043
815	0.5926546	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7030153	0.3421060	0.4908826	0.7853981	1.1689843
816	0.5902043	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7033153	0.3422408	0.4908826	0.7853981	1.1678643
817	0.5877540	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7036153	0.3423756	0.4908826	0.7853981	1.1667443
818	0.5853037	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7039153	0.3425104	0.4908826	0.7853981	1.1656243
819	0.5828534	0.3375845	0.3165711	2.1537485	2.5032674	0.7622378	0.5989802	0.7042153	0.3426452	0.4908826	0.7853981	1.1645043

[illegible]

056	0.2611942	0.4222084	0.2613840	0.5987106	0.1665065	0.6024919	0.5761073	0.4303233	0.7250232	0.3605329	0.4908026	0.7853981	1.1268745
057	0.2611778	0.4261777	0.2613815	0.5947070	0.1654614	0.6040596	0.5687854	0.4303011	0.7254503	0.3666313	0.4908826	0.7853981	1.1277037
058	0.2614605	0.4266461	0.2616104	0.5947804	0.1644153	0.6040261	0.5687854	0.4303011	0.7258774	0.3667280	0.4908826	0.7853981	1.1267338
059	0.2611668	0.4271116	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
060	0.2611236	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
061	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
062	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
063	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
064	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
065	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
066	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
067	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
068	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
069	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
070	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
071	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
072	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
073	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
074	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
075	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
076	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
077	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
078	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
079	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
080	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
081	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
082	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
083	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
084	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
085	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
086	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
087	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
088	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
089	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
090	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538
091	0.2611368	0.4271673	0.2614166	0.5947096	0.1677155	0.6040261	0.5687854	0.4303011	0.7261771	0.3666849	0.4908826	0.7853981	1.1269538

[illegible]

964	0.1531114	0.1511422	0.4915554	2.0304801	0.0143872	0.7548851	0.4740108	0.1686173	0.3536229	0.4908826	0.7853981	1.0340233
965	0.1342036	0.1374783	0.4897632	2.0393169	2.153316	0.5639116	0.2700483	0.1690566	0.3536524	0.4908826	0.7853981	1.0332241
966	0.1350493	0.1359766	0.4894145	2.0402651	2.0460317	0.5620579	0.2614816	0.1694449	0.3536816	0.4908826	0.7853981	1.0324259
967	0.1449731	0.1498412	0.4883431	2.2476997	2.0471575	0.5819927	0.267527	0.1698286	0.3537113	0.4908826	0.7853981	1.0316334
968	0.1481011	0.1487739	0.4884256	2.2484703	2.1637287	0.5603315	0.2653701	0.1702160	0.3537376	0.4908826	0.7853981	1.0308432
969	0.1408412	0.1476734	0.4881453	2.2496874	2.1655307	0.5757810	0.2645356	0.1705989	0.3537645	0.4908826	0.7853981	1.0300446
970	0.1465701	0.1465704	0.4881629	2.2504823	2.1666311	0.5285148	0.2630179	0.1709831	0.3537916	0.4908826	0.7853981	1.0292530
971	0.1454485	0.1456183	0.4880791	2.2521138	2.1681942	0.5289435	0.2615373	0.1713672	0.3538186	0.4908826	0.7853981	1.0284624
972	0.1432660	0.1451485	0.4879583	2.2525236	2.1700238	0.5258215	0.2599163	0.1717510	0.3538430	0.4908826	0.7853981	1.0276728
973	0.1403694	0.1413256	0.4875102	2.2534946	2.1717398	0.5251015	0.2587974	0.1721320	0.3538684	0.4908826	0.7853981	1.0268890
974	0.1421550	0.1421759	0.4873246	2.2535381	2.1731031	0.5251015	0.2587974	0.1725174	0.3538932	0.4908826	0.7853981	1.0260983
975	0.1461364	0.1419044	0.4872711	2.2537329	2.1750703	0.5252329	0.2581175	0.1728947	0.3539216	0.4908826	0.7853981	1.0254164
976	0.1394311	0.1419332	0.4876203	2.2535344	2.1770307	0.5219914	0.2573843	0.1732297	0.3539453	0.4908826	0.7853981	1.0246372
977	0.1334293	0.1433333	0.4876137	2.2531542	2.1792302	0.5219914	0.2573843	0.1736116	0.3539680	0.4908826	0.7853981	1.0238552
978	0.1377147	0.1437119	0.4874257	2.2633141	2.1812767	0.5242248	0.2507214	0.1739932	0.3539906	0.4908826	0.7853981	1.0230732
979	0.1366103	0.1436039	0.4874332	2.2634076	2.1831783	0.5242248	0.2507214	0.1743722	0.3540114	0.4908826	0.7853981	1.0222979
980	0.1393447	0.1433497	0.4874911	2.2634736	2.1850945	0.5240099	0.2476242	0.1747544	0.3540319	0.4908826	0.7853981	1.0215206
981	0.1403437	0.1434787	0.4874992	2.2641497	2.1869321	0.5242527	0.2461441	0.1751347	0.3540522	0.4908826	0.7853981	1.0207405
982	0.1392194	0.1434123	0.4874081	2.2641552	2.1888326	0.5240970	0.2446623	0.1755127	0.3540699	0.4908826	0.7853981	1.0199690
983	0.1372131	0.1434123	0.4873627	2.2641552	2.1908164	0.5249391	0.2430564	0.1758920	0.3540872	0.4908826	0.7853981	1.0191946
984	0.1371034	0.1434820	0.4873541	2.2650167	2.1928327	0.5241819	0.2415124	0.1762712	0.3541058	0.4908826	0.7853981	1.0184221
985	0.1329064	0.1432328	0.4867923	2.2653244	2.1947643	0.5240627	0.2401604	0.1766477	0.3541229	0.4908826	0.7853981	1.0176554
986	0.1325323	0.1434143	0.4867911	2.2653754	2.1967403	0.5240627	0.2394381	0.1770256	0.3541387	0.4908826	0.7853981	1.0168850
987	0.1321465	0.1437645	0.4867911	2.2662717	2.1987120	0.5239401	0.2383453	0.1774034	0.3541535	0.4908826	0.7853981	1.0161180
988	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
989	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
990	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
991	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
992	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
993	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
994	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
995	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
996	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
997	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
998	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503
999	0.1320582	0.1437401	0.4865954	2.2673730	2.1997097	0.5239401	0.2383453	0.1777811	0.3541695	0.4908826	0.7853981	1.0153503

1000 0.1130915 0.1130914 0.4521347 0.01032095 2.0024777-0.7791372-0.4874468 0.7822348 0.4563090 0.4908826 0.7853981 1.0063457
1001 0.1130915 0.1130914 0.4521347 0.01032095 2.0024777-0.7791372-0.4874468 0.7822348 0.4563090 0.4908826 0.7853981 1.0063457
1002 0.1130915 0.1130914 0.4521347 0.01032095 2.0024777-0.7791372-0.4874468 0.7822348 0.4563090 0.4908826 0.7853981 1.0063457
1003 0.1130915 0.1130914 0.4521347 0.01032095 2.0024777-0.7791372-0.4874468 0.7822348 0.4563090 0.4908826 0.7853981 1.0063457
1004 0.1130915 0.1130914 0.4521347 0.01032095 2.0024777-0.7791372-0.4874468 0.7822348 0.4563090 0.4908826 0.7853981 1.0063457
1005 0.1130915 0.1130914 0.4521347 0.01032095 2.0024777-0.7791372-0.4874468 0.7822348 0.4563090 0.4908826 0.7853981 1.0063457
1006 0.1130915 0.1130914 0.4521347 0.01032095 2.0024777-0.7791372-0.4874468 0.7822348 0.4563090 0.4908826 0.7853981 1.0063457
1007 0.1130915 0.1130914 0.4521347 0.01032095 2.0024777-0.7791372-0.4874468 0.7822348 0.4563090 0.4908826 0.7853981 1.0063457
1008 0.1130915 0.1130914 0.4521347 0.01032095 2.0024777-0.7791372-0.4874468 0.7822348 0.4563090 0.4908826 0.7853981 1.0063457
1009 0.1130915 0.1130914 0.4521347 0.01032095 2.0024777-0.7791372-0.4874468 0.7822348 0.4563090 0.4908826 0.7853981 1.0063457
0.44198 0.61444 3.55802-0.511194
1 IMAGE PLANE SPOT DIAGRAM ANALYSIS:

THICKNESS = 0.053003 U = 0.0 AFAP = 0.0 P = 1.000000

CENTROID: ZCENTR = 0.0 YCENTR = 0.0026398

STANDARD DEVIATIONS: SIGXAY = 0.0000121 SIGMAZ = 0.0000207

RMS SPOT SIZE: RMSRAD = 3.0057336

SPOT DIAGRAM ENERGY DENSITY VS. RADIUS FROM CENTROID:

124	RADIUS	FRACTION
1	0.000000	0.6741935
2	0.010000	0.9483871
3	0.015000	0.9485161
4	0.020000	0.9870967
5	0.025000	1.0000000
6	0.030000	1.0000000
7	0.035000	1.0000000
8	0.040000	1.0000000
9	0.045000	1.0000000
10	0.050000	1.0000000
11	0.055000	1.0000000
12	0.060000	1.0000000
13	0.065000	1.0000000
14	0.070000	1.0000000
15	0.075000	1.0000000
16	0.080000	1.0000000
17	0.085000	1.0000000
18	0.090000	1.0000000
19	0.095000	1.0000000
20	0.100000	1.0000000
21	0.105000	1.0000000
22	0.110000	1.0000000
23	0.115000	1.0000000
24	0.120000	1.0000000
25	0.125000	1.0000000
26	0.130000	1.0000000
27	0.135000	1.0000000
28	0.140000	1.0000000
29	0.145000	1.0000000
30	0.150000	1.0000000
31	0.155000	1.0000000
32	0.160000	1.0000000
33	0.165000	1.0000000
34	0.170000	1.0000000

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35 0.1749998 1.0000000
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82 0.1749998 1.0000000
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85 0.1749998 1.0000000
86 0.1749998 1.0000000
87 0.1749998 1.0000000
88 0.1749998 1.0000000
89 0.1749998 1.0000000
90 0.1749998 1.0000000
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95 0.1749998 1.0000000
96 0.1749998 1.0000000
97 0.1749998 1.0000000
98 0.1749998 1.0000000
99 0.1749998 1.0000000
100 0.1749998 1.0000000

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1001 DIAGRAM CALCULATIONS COMPLETE. THE PRINTER.
 TO OBTAIN PLOTS FROM THE PRINTER OR
 ISSUE THE FOLLOWING COMMANDS:
 FOR PRINTER PLOTS
 ENTER "LENSCOM PLOTTER"
 FOR PLOTTER SPANS
 ENTER "LENSCOM PLOTTER"
 END OF PROGRAM

RESULTS FROM GRIN

2. Input: $x_C = -0.07$, $DIV = -0.05$, $\alpha_p = 0.0$

GRAIN PARAMETERS(2):

ALPHA = 0.7853579 BETA = 0.3227880 RADIUS = 1.00000 INCIDENT ANGLE = 0.0 ITERATIONS = 1006
EDGE THICKNESS = C.0500000 INDICES OF REFRACTION: N1 = 1.00000 N2 = 1.42157 N3 = 1.00000
FCCAL LENGTH FROM STATION ZERO = 4.00000 DELTA BETA= 0.00032
CENTER OF SWH(XC)=-0.07030 CHANGE IN N2(1)=-0.050 ALFAP= 0.0
NOTE: X-CCORDINATES HAS BEEN SHIFTED IN CASE=2 BY X2(K)XNDW,X2(K)=-0.0 ETC.

J	E	X1	Y1	X2	Y2	BETA	RR	12P	RF	12	ETA	T	11P	11	OVDT
			THEIAE	THEIAO	PSI	PSIO									
1	1	0.0000000	1.0000000	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
2	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
3	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
4	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
5	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
6	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
7	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
8	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
9	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
10	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
11	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
12	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
13	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
14	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
15	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
16	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
17	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
18	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
19	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
20	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
21	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
22	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
23	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
24	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
25	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
26	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		
27	1	0.9999999	0.9999999	1.0570399	0.9841160	0.3227880	0.1778834	0.1243717	0.1457046	0.0500000	0.5192339	0.7853981	6.8145685		

[illegible]

388	0.4898837	0.1688747	0.9327775	0.6181803	0.1988655	0.2936648	0.4935054	0.2529622	0.5062062	0.7853981	1.0598064
389	0.2708444	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.4942357	0.2253007	0.5041749	0.7853581	1.0555340
390	0.6882404	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.4949598	0.2253420	0.5041441	0.7853581	1.0522271
391	0.4449214	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.4956887	0.2539764	0.5041128	0.7853981	1.0493538
392	0.6816111	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.4964142	0.2543157	0.5040818	0.7853981	1.0461914
393	0.4717151	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.4971425	0.2546517	0.5040507	0.7853981	1.0429852
394	0.2717515	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.4978899	0.2549877	0.5040193	0.7853581	1.0397513
395	0.4849444	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.4985846	0.2553241	0.5039885	0.7853581	1.0366613
396	0.2790134	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.4993052	0.2556586	0.5039576	0.7853581	1.0335142
397	0.6262171	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5000362	0.2559919	0.5039267	0.7853581	1.0303259
398	0.4816994	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5007585	0.2563258	0.5038958	0.7853981	1.0271514
399	0.2608727	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5014771	0.2566584	0.5038649	0.7853581	1.0240706
400	0.4604550	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5021950	0.2569917	0.5038341	0.7853581	1.0209753
401	0.2420254	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5029091	0.2573225	0.5038032	0.7853981	1.0178578
402	0.4502344	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5036348	0.2576555	0.5037723	0.7853581	1.0147774
403	0.2505969	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5043536	0.2579804	0.5037418	0.7853581	1.0116551
404	0.4717151	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5050607	0.2583110	0.5037110	0.7853981	1.0086720
405	0.2519525	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5057787	0.2586460	0.5036802	0.7853981	1.0056087
406	0.4551382	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5064956	0.2589868	0.5036496	0.7853981	1.0025589
407	0.2522375	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5072064	0.2593297	0.5036189	0.7853581	1.0095424
408	0.4523488	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5079195	0.2596727	0.5035883	0.7853581	1.0065231
409	0.2526671	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5086408	0.2599466	0.5035578	0.7853581	1.0034780
410	0.4518444	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5093671	0.2602724	0.5035274	0.7853981	1.0004045
411	0.2518951	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5100497	0.2605984	0.5034969	0.7853581	1.0075528
412	0.4518444	0.1688747	0.5325250	0.4137275	0.0972871	0.1777487	0.5107633				

250

251

569	0.6012760	0.3039996	0.4990718	0.7853981	1.4300919
570	0.6108021	0.3042278	0.4990461	0.7853981	1.4283400
571	0.6113719	0.3044484	0.4990208	0.7853581	1.4266050
572	0.6119433	0.3046719	0.4985554	0.7853581	1.4248753
573	0.6125121	0.3048957	0.4989702	0.7853981	1.4231529
574	0.6130882	0.3051189	0.4989448	0.7853981	1.4214115
575	0.6136531	0.3053415	0.4989195	0.7853981	1.4197073
576	0.6142281	0.3055632	0.4988942	0.7853581	1.4179745
577	0.6147919	0.3057855	0.4988689	0.7853981	1.4162788
578	0.6153553	0.3060062	0.4988436	0.7853981	1.4145821
579	0.6159258	0.3062246	0.4988186	0.7853981	1.4128761
580	0.6164955	0.3064443	0.4987932	0.7853581	1.4111700
581	0.6170570	0.3066640	0.4987683	0.7853981	1.4094695
582	0.6176177	0.3068843	0.4987430	0.7853581	1.4078188
583	0.6181813	0.3070991	0.4987181	0.7853581	1.4061689
584	0.6187539	0.3073158	0.4986932	0.7853581	1.4044341
585	0.6193133	0.3075305	0.4986682	0.7853981	1.4027739
586	0.6198719	0.3077463	0.4986432	0.7853581	1.4011183
587	0.6204268	0.3079619	0.4986183	0.7853981	1.3994751
588	0.6209853	0.3081755	0.4985934	0.7853581	1.3977547
589	0.6215494	0.3083897	0.4985685	0.7853981	1.3961582
590	0.6221090	0.3086029	0.4985435	0.7853981	1.3945593
591	0.6226645	0.3088147	0.4985189	0.7853981	1.3928757
592	0.6232222	0.3090279	0.4984940	0.7853581	1.3912163
593	0.6237746	0.3092407	0.4984695	0.7853581	1.3896160
594	0.6243337	0.3094512	0.4984449	0.7853981	1.3879786
595	0.6248875	0.3096607	0.4984200	0.7853581	1.3863592
596	0.6254431	0.3098704	0.4983954	0.7853581	1.3847442
597	0.6259927	0.3100811	0.4983709	0.7853581	1.3831348
598	0.6265424	0.3102903	0.4983463	0.7853981	1.3815346
599	0.6270989	0.3104979	0.4983217	0.7853981	1.3799181
600	0.6276441	0.3107068	0.4982972	0.7853981	1.3783360
601	0.6281914	0.3109130	0.4982726	0.7853581	1.3767219
602	0.6287419	0.3111272	0.4982485	0.7853981	1.3751564
603	0.6292958	0.3113375	0.4982239	0.7853981	1.3735704

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1001 0.1298934 0.1187727 0.0198222 2.2959366 2.8251762 0.7936280 0.3497022 0.4914306 0.7853981 0.9836744
1002 0.1097471 0.1097471 0.1097471 2.2976866 2.8273668 0.793356 0.3496723 0.4914304 0.7853981 0.9836744
1003 0.1086462 0.1086462 0.1086462 2.2994366 2.8295568 0.793084 0.3496264 0.4914302 0.7853981 0.9836744
1004 0.1075453 0.1075453 0.1075453 2.3011866 2.8317468 0.792812 0.3495805 0.4914300 0.7853981 0.9836744
1005 0.1064444 0.1064444 0.1064444 2.3029366 2.8339368 0.792540 0.3495346 0.4914298 0.7853981 0.9836744
1006 0.1053435 0.1053435 0.1053435 2.3046866 2.8361268 0.792268 0.3494887 0.4914296 0.7853981 0.9836744
1007 0.1042426 0.1042426 0.1042426 2.3064366 2.8383168 0.791996 0.3494428 0.4914294 0.7853981 0.9836744
1008 0.1031417 0.1031417 0.1031417 2.3081866 2.8405068 0.791724 0.3493969 0.4914292 0.7853981 0.9836744
1009 0.1020408 0.1020408 0.1020408 2.3099366 2.8426968 0.791452 0.3493510 0.4914290 0.7853981 0.9836744
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1015 0.1000000 0.1000000 0.1000000 2.3204366 2.8558368 0.789820 0.3490756 0.4914278 0.7853981 0.9836744
1016 0.1000000 0.1000000 0.1000000 2.3221866 2.8580268 0.789548 0.3490297 0.4914276 0.7853981 0.9836744
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1018 0.1000000 0.1000000 0.1000000 2.3256866 2.8624068 0.789004 0.3489379 0.4914272 0.7853981 0.9836744
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1021 0.1000000 0.1000000 0.1000000 2.3309366 2.8689768 0.788188 0.3488002 0.4914266 0.7853981 0.9836744
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1027 0.1000000 0.1000000 0.1000000 2.3414366 2.8821168 0.786556 0.3485248 0.4914254 0.7853981 0.9836744
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1063 0.1000000 0.1000000 0.1000000 2.4044366 2.9609568 0.776764 0.3468724 0.4914182 0.7853981 0.9836744
1064 0.1000000 0.1000000 0.1000000 2.4061866 2.9631468 0.776492 0.3468265 0.4914180 0.7853981 0.9836744
1065 0.1000000 0.1000000 0.1000000 2.4079366 2.9653368 0.776220 0.3467806 0.4914178 0.7853981 0.9836744
1066 0.1000000 0.1000000 0.1000000 2.4096866 2.9675268 0.775948 0.3467347 0.4914176 0.7853981 0.9836744
1067 0.1000000 0.1000000 0.1000000 2.4114366 2.9697168 0.775676 0.3466888 0.4914174 0.7853981 0.9836744
1068 0.1000000 0.1000000 0.1000000 2.4131866 2.9719068 0.775404 0.3466429 0.4914172 0.7853981 0.9836744
1069 0.1000000 0.1000000 0.1000000 2.4149366 2.9740968 0.775132 0.3465970 0.4914170 0.7853981 0.9836744
1070 0.1000000 0.1000000 0.1000000 2.4166866 2.9762868 0.774860 0.3465511 0.4914168 0.7853981 0.9836744
1071 0.1000000 0.1000000 0.1000000 2.4184366 2.9784768 0.774588 0.3465052 0.4914166 0.7853981 0.9836744
1072 0.1000000 0.1000000 0.1000000 2.4201866 2.9806668 0.774316 0.3464593 0.4914164 0.7853981 0.9836744
1073 0.1000000 0.1000000 0.1000000 2.4219366 2.9828568 0.774044 0.3464134 0.4914162 0.7853981 0.9836744
1074 0.1000000 0.1000000 0.1000000 2.4236866 2.9850468 0.773772 0.3463675 0.4914160 0.7853981 0.9836744
1075 0.1000000 0.1000000 0.1000000 2.4254366 2.9872368 0.773500 0.3463216 0.4914158 0.7853981 0.9836744
1076 0.1000000 0.1000000 0.1000000 2.4271866 2.9894268 0.773228 0.3462757 0.4914156 0.7853981 0.9836744
1077 0.1000000 0.1000000 0.1000000 2.4289366 2.9916168 0.772956 0.3462298 0.4914154 0.7853981 0.9836744
1078 0.1000000 0.1000000 0.1000000 2.4306866 2.9938068 0.772684 0.3461839 0.4914152 0.7853981 0.9836744
1079 0.1000000 0.1000000 0.1000000 2.4324366 2.9959968 0.772412 0.3461380 0.4914150 0.7853981 0.9836744
1080 0.1000000 0.1000000 0.1000000 2.4341866 2.9981868 0.772140 0.3460921 0.4914148 0.7853981 0.9836744
1081 0.1000000 0.1000000 0.1000000 2.4359366 3.0003768 0.771868 0.3460462 0.4914146 0.7853981 0.9836744
1082 0.1000000 0.1000000 0.1000000 2.4376866 3.0025668 0.771596 0.3460003 0.4914144 0.7853981 0.9836744
1083 0.1000000 0.1000000 0.1000000 2.4394366 3.0047568 0.771324 0.3459544 0.4914142 0.7853981 0.9836744
1084 0.1000000 0.1000000 0.1000000 2.4411866 3.0069468 0.771052 0.3459085 0.4914140 0.7853981 0.9836744
1085 0.1000000 0.1000000 0.1000000 2.4429366 3.0091368 0.770780 0.3458626 0.4914138 0.7853981 0.9836744
1086 0.1000000 0.1000000 0.1000000 2.4446866 3.0113268 0.770508 0.3458167 0.4914136 0.7853981 0.9836744
1087 0.1000000 0.1000000 0.1000000 2.4464366 3.0135168 0.770236 0.3457708 0.4914134 0.7853981 0.9836744
1088 0.1000000 0.1000000 0.1000000 2.4481866 3.0157068 0.769964 0.3457249 0.4914132 0.7853981 0.9836744
1089 0.1000000 0.1000000 0.1000000 2.4499366 3.0178968 0.769692 0.3456790 0.4914130 0.7853981 0.9836744
1090 0.1000000 0.1000000 0.1000000 2.4516866 3.0200868 0.769420 0.3456331 0.4914128 0.7853981 0.9836744
1091 0.1000000 0.1000000 0.1000000 2.4534366 3.0222768 0.769148 0.3455872 0.4914126 0.7853981 0.9836744
1092 0.1000000 0.1000000 0.1000000 2.4551866 3.0244668 0.768876 0.3455413 0.4914124 0.7853981 0.9836744
1093 0.1000000 0.1000000 0.1000000 2.4569366 3.0266568 0.768604 0.3454954 0.4914122 0.7853981 0.9836744
1094 0.1000000 0.1000000 0.1000000 2.4586866 3.0288468 0.768332 0.3454495 0.4914120 0.7853981 0.9836744
1095 0.1000000 0.1000000 0.1000000 2.4604366 3.0310368 0.768060 0.3454036 0.4914118 0.7853981 0.9836744
1096 0.1000000 0.1000000 0.1000000 2.4621866 3.0332268 0.767788 0.3453577 0.4914116 0.7853981 0.9836744
1097 0.1000000 0.1000000 0.1000000 2.4639366 3.0354168 0.767516 0.3453118 0.4914114 0.7853981 0.9836744
1098 0.1000000 0.1000000 0.1000000 2.4656866 3.0376068 0.767244 0.3452659 0.4914112 0.7853981 0.9836744
1099 0.1000000 0.1000000 0.1000000 2.4674366 3.0397968 0.766972 0.3452200 0.4914110 0.7853981 0.9836744
1100 0.1000000 0.1000000 0.1000000 2.4691866 3.0419868 0.766700 0.3451741 0.4914108 0.7853981 0.9836744

```

1 IMAGE PLANE 7 SECT 3.56381 -7.55618
 THICKNESS = 0.000000 U = 0.0 ALFA = 0.0 R = 1.000000
 CENTROID: ZCFATR = 0.0 YCENTR = 0.0027303
 STANDARD DEVIATIONS: SIGMAV = 0.0000085 SIGMAZ = 0.0000194
 RMS SPECT SIZE: RMSRAD = 0.0052860

SFOT DIAGRAM ENERGY DENSITY VS. RADIUS FROM CENTROID:

IZ4	RADIUS	FRACTION
1	0.005000	0.6776314
2	0.010000	0.5405263
3	0.015000	0.4500000
4	0.020000	0.3750000
5	0.025000	0.3125000
6	0.030000	0.2600000
7	0.035000	0.2150000
8	0.040000	0.1750000
9	0.045000	0.1400000
10	0.050000	0.1100000
11	0.055000	0.0850000
12	0.060000	0.0650000
13	0.065000	0.0500000
14	0.070000	0.0400000
15	0.075000	0.0300000
16	0.080000	0.0250000
17	0.085000	0.0200000
18	0.090000	0.0150000
19	0.095000	0.0100000
20	0.100000	0.0050000
21	0.105000	0.0025000
22	0.110000	0.0012500
23	0.115000	0.0006250
24	0.120000	0.0003125
25	0.125000	0.0001562
26	0.130000	0.0000781
27	0.135000	0.0000391
28	0.140000	0.0000195
29	0.145000	0.0000098
30	0.150000	0.0000049
31	0.155000	0.0000024
32	0.160000	0.0000012
33	0.165000	0.0000006
34	0.170000	0.0000003
35	0.175000	0.0000001
36	0.180000	0.0000000
37	0.185000	0.0000000
38	0.190000	0.0000000
39	0.195000	0.0000000
40	0.200000	0.0000000
41	0.205000	0.0000000
42	0.210000	0.0000000</

GRIN PARAMETERS(21)

ALPHA = 0.7853579 BETA = 0.3227880 RADIUS = 1.00000 INCIDENT ANGLE = 0.0
 EDGE THICKNESS = 0.050000 INDICES OF REFRACTION: N1 = 1.00000 N2 = 1.42157 N3 = 1.00000
 FOCAL LENGTH FROM STATION ZERO = 4.00000 DELTA BETA = 0.00032
 CENTER OF SYMMETRY = 0.07000 CHANGE IN N2(12) = 0.050 ALFAP = 0.0
 NOTE: K-COORDINATES HAS BEEN SHIFTED IN CASE=2 BY X2(1K);NDM,X2(1K)=0.0 ETC.

0.43618 0.62164 3.56381 -0.50618
 ISKEW RAY TRACE PARAMETERS:

ALFAP = 0.0 GRID = 0.1000000 SEE LENS PARAMETERS ABOVE.

RAY PHI	RAY PHI	NO CKP	YO CLPP	XI CMP	YI D3	ZI D1	OPL NUM	YIM NUM	ZIM NUM	NTNCTV	XDIAPT	YDIAPT
1 0.0	0.29000	0.23618	0.0015	-0.79771	0.00036	0.09844	4.24078	0.00545	-0.01646	1.00000	-0.603E-01	0.475E-02
0.4641	0.1285	0.9995	0.0015	-0.7331	3.4680	0.4362	0.2000	0.0	-0.5837	1.00000	0.385E+00	0.315E-02
2 0.0	0.30000	0.13618	0.0008	-0.19229	0.00044	0.20024	4.17358	0.00315	-0.00311	1.00000	0.385E+00	0.315E-02
0.4326	0.6704	0.9982	0.0008	-0.0602	3.3776	0.4362	0.3000	0.0	-0.5618	1.00000	0.385E+00	0.315E-02
3 0.0	0.40000	0.03618	0.0007	-0.28135	0.00069	0.30392	4.09773	0.00280	-0.00462	1.00000	0.387E+00	0.277E-02
0.3876	0.5919	0.9856	0.0007	-0.09336	3.2969	0.4362	0.4500	0.0	-0.5361	1.00000	0.387E+00	0.277E-02
4 0.0	0.50000	0.16382	0.0009	-0.1279	0.00117	0.40584	4.01756	0.00395	-0.00309	1.00000	0.413E+00	0.393E-02
0.3347	0.5033	0.9918	0.0009	-0.1279	3.2267	0.4362	0.5000	0.0	-0.5107	1.00000	0.413E+00	0.393E-02
5 0.0	0.60000	0.16382	0.0008	-0.1641	0.00167	0.51836	3.93575	0.00344	-0.01165	1.00000	0.426E+00	0.433E-02
0.2700	0.3999	0.9864	0.0008	-0.1641	3.1690	0.4362	0.6000	0.0	-0.4860	1.00000	0.426E+00	0.433E-02
6 0.0	0.70000	0.26382	0.0007	-0.50243	0.00214	0.62987	3.85365	0.00445	-0.00193	1.00000	0.431E+00	0.446E-02
0.1914	0.2796	0.9754	0.0007	-0.2018	3.1257	0.4362	0.7000	0.0	-0.4633	1.00000	0.426E+00	0.362E-02
7 0.0	0.80000	0.36382	0.0005	-0.55575	0.00214	0.74449	3.77235	0.00363	-0.00250	1.00000	0.426E+00	0.362E-02
0.0970	0.1401	0.9705	0.0005	-0.2417	3.0994	0.4362	0.8000	0.0	-0.4445	1.00000	0.426E+00	0.362E-02
8 0.0	0.90000	0.46382	0.0004	-0.59634	0.00217	0.86261	3.69051	0.00392	-0.00440	1.00000	0.435E+00	0.392E-02
0.0083	0.0118	0.9632	0.0004	-0.2752	3.0997	0.4362	0.9000	0.0	-0.4317	1.00000	0.435E+00	0.392E-02
9 0.0	0.10000	0.29476	0.1999	1.14001	0.02812	0.92787	4.27335	-0.00538	-0.01471	1.00000	-0.781E+00	0.619E-02
0.4836	0.7652	0.9999	0.1999	1.0121	3.5242	0.4362	0.1414	0.1000	-0.5977	1.00000	-0.781E+00	0.619E-02
10 0.0	0.20000	0.21254	0.1999	0.14000	0.02812	0.92787	4.27335	-0.00538	-0.01471	1.00000	-0.781E+00	0.619E-02
0.4583	0.7175	0.9998	0.1999	0.14000	3.4459	0.4362	0.2336	0.1000	-0.5772	1.00000	-0.781E+00	0.619E-02
11 0.0	0.30000	0.11596	0.1999	0.27113	0.06897	0.25698	4.16185	0.00387	-0.03572	1.00000	0.345E+00	0.272E-02
0.4252	0.6571	0.9978	0.1999	0.0629	3.3643	0.4362	0.3162	0.1000	-0.5573	1.00000	0.345E+00	0.272E-02
12 0.0	0.40000	0.02387	0.1999	0.29184	0.07773	0.27716	4.08773	0.00364	-0.00227	1.00000	0.412E+00	0.418E-02
0.3833	0.5941	0.9953	0.1999	0.0741	3.2814	0.4362	0.4123	0.1000	-0.5335	1.00000	0.412E+00	0.418E-02
13 0.0	0.50000	0.07372	0.1999	0.31714	0.08316	0.29203	4.00923	0.00321	-0.00129	1.00000	0.427E+00	0.444E-02
0.3302	0.4459	0.9914	0.1999	0.1287	3.2206	0.4362	0.5092	0.1000	-0.5085	1.00000	0.427E+00	0.444E-02
14 0.0	0.60000	0.17299	0.1999	0.44355	0.08831	0.30307	3.92863	0.00413	-0.00027	1.00000	0.435E+00	0.417E-02
0.2652	0.3924	0.9860	0.1999	0.1644	3.1644	0.4362	0.6083	0.1000	-0.4842	1.00000	0.435E+00	0.417E-02
15 0.0	0.70000	0.27092	0.1999	0.57663	0.09231	0.31113	3.84831	0.00382	-0.00388	1.00000	0.418E+00	0.439E-02

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0.1837 C.2682 C.9787 -0.0283 -0.7033 3.1237 0.4362 0.7071 0.1000 -0.4417
16 0.1000 C.8000 C.3700 0.1000 0.5585 0.0954 0.7459 3.7672 0.0034 -0.0072 1.0000 0.425E+00 C.375E-02
0.0909 0.1311 0.9659 -0.0257 -0.2415 3.0984 0.4362 0.8062 0.1000 -0.4443
17 0.1000 C.5000 0.4693 0.1000 0.5978 0.0983 0.8626 3.6670 0.0029 -0.0072 1.0000 0.427E+00 C.328E-02
0.0109 0.0228 0.9559 -0.0308 -0.2893 3.0914 0.4362 0.9055 0.1000 -0.4312
18 0.2000 C.0 -0.2318 0.2000 0.0977 0.0984 0.0003 4.2407 -0.0152 0.0054 1.0000 -0.327E+01 C.106E+00
0.4646 C.7253 0.9555 -0.0328 0.0115 3.4680 0.4362 0.2000 0.2000 -0.5839
19 0.2000 C.1000 -0.2125 0.2000 0.1204 0.0960 0.0543 4.2561 -0.0033 0.0076 1.0000 0.112E-01 C.106E-01
0.4558 C.7201 0.9559 -0.0328 -0.0115 3.4458 0.4362 0.2000 0.2000 -0.5795
20 0.2000 C.1533 0.2000 0.1744 0.1293 0.1289 4.1859 -0.0022 0.0044 1.0000 0.331E+00 C.383E-02
0.4394 C.6826 C.5585 -0.0382 -0.0352 3.3925 0.4362 0.2000 0.2000 -0.5661
21 0.2000 C.3000 -0.0756 0.2000 0.2445 0.1641 0.2183 4.1814 0.0026 -0.0036 1.0000 0.381E+00 C.501E-02
0.4076 0.6261 0.9568 -0.0422 -0.0422 3.3274 0.4362 0.2000 0.2000 -0.5467
22 0.2000 C.4000 0.2107 0.2000 0.3210 0.1587 0.3159 4.0609 0.0013 -0.0036 1.0000 0.356E+00 C.312E-02
0.3646 C.5327 0.9543 -0.0483 -0.0480 3.2262 0.4362 0.2000 0.2000 -0.5242
23 0.2000 C.5000 0.1023 0.2000 0.3932 0.1693 0.4183 3.9557 0.0054 -0.0071 1.0000 0.423E+00 0.613E-02
0.3128 C.4677 C.9573 -0.0512 -0.1312 3.2024 0.4362 0.2000 0.2000 -0.5014
24 0.2000 C.6000 0.1962 0.2000 0.4595 0.1791 0.5252 3.9091 0.0035 -0.0046 1.0000 0.420E+00 C.440E-02
0.2460 C.3628 C.9844 -0.0550 -0.1674 3.1532 0.4362 0.2000 0.2000 -0.4783
25 0.2000 C.7000 0.2918 0.2000 0.5187 0.1839 0.6352 3.8310 0.0035 -0.0072 1.0000 0.418E+00 C.461E-02
0.1656 C.2411 C.9773 -0.0579 -0.2351 3.1168 0.4362 0.2000 0.2000 -0.4575
26 0.2000 C.8000 0.3884 0.2000 0.5668 0.1903 0.7456 3.7519 0.0043 -0.0071 1.0000 0.428E+00 C.484E-02
0.0730 C.1552 0.5662 -0.0601 -0.2428 3.0953 0.4362 0.2000 0.2000 -0.4408
27 0.2000 C.9000 0.4857 0.2000 0.6297 0.1956 0.8672 3.6738 0.0043 -0.0071 1.0000 0.425E+00 C.403E-02
0.0347 C.0496 0.9575 -0.0662 -0.2816 3.0922 0.4362 0.2000 0.2000 -0.4298
28 0.2000 C.0 -0.1361 0.2000 0.1930 0.2002 0.0097 4.1358 -0.0030 0.0070 1.0000 -0.347E+01 C.232E+00
0.4326 C.4704 0.9582 -0.0662 -0.0018 3.3776 0.4362 0.2000 0.2000 -0.5618
29 0.2000 C.1000 -0.1156 0.2000 0.2213 0.2054 0.0689 4.1618 -0.0036 -0.0046 1.0000 0.233E+00 C.877E-02
0.4252 C.6571 C.9578 -0.0624 -0.0624 3.3640 0.4362 0.2000 0.2000 -0.5513
30 0.2000 C.2000 -0.0756 0.2000 0.2445 0.2196 0.1457 4.1281 0.0043 -0.0054 1.0000 0.325E+00 C.874E-02
0.4076 C.4261 C.9568 -0.0654 -0.0654 3.3274 0.4362 0.2000 0.2000 -0.5467
31 0.2000 C.3000 -0.0119 0.2000 0.3019 0.2338 0.2322 4.0740 0.0043 -0.0058 1.0000 0.356E+00 C.763E-02
0.3765 C.5727 C.9549 -0.0707 -0.0726 3.2787 0.4362 0.2000 0.2000 -0.5301
32 0.2000 C.4000 0.0638 0.2000 0.3636 0.2472 0.3273 4.0175 0.0043 -0.0058 1.0000 0.386E+00 C.582E-02
0.3347 C.5033 C.9518 -0.0759 -0.1010 3.2267 0.4362 0.2000 0.2000 -0.5107
33 0.2000 C.5000 0.1469 0.2000 0.4256 0.2581 0.4276 3.9496 0.0043 -0.0058 1.0000 0.411E+00 C.377E-02
0.2816 C.4183 C.9514 -0.0807 -0.1358 3.1777 0.4362 0.2000 0.2000 -0.4809
34 0.2000 C.6000 0.2346 0.2000 0.4847 0.2666 0.5332 3.8779 -0.0043 0.0076 1.0000 0.420E+00 C.119E-05
0.2146 C.3147 C.9515 -0.0855 -0.1711 3.1373 0.4362 0.2000 0.2000 -0.4694
35 0.2000 C.7000 0.3253 0.2000 0.5468 0.2784 0.6423 3.8033 0.0043 -0.0076 1.0000 0.416E+00 C.572E-02
0.1346 C.1952 C.9541 -0.0883 -0.2181 3.1076 0.4362 0.2000 0.2000 -0.4511
36 0.2000 C.8000 0.4182 0.2000 0.5950 0.2862 0.7554 3.7276 C.0036 -0.0076 1.0000 0.425E+00 C.428E-02
0.0419 C.0642 C.9552 -0.0914 -0.2441 3.0921 0.4362 0.2000 0.2000 -0.4467
37 0.2000 C.9000 0.5125 0.2000 0.6494 0.2947 0.8727 3.6524 C.0026 -0.0076 1.0000 0.424E+00 C.391E-02
0.0656 C.0937 C.9544 -0.0942 -0.2842 3.0946 0.4362 0.2000 0.2000 -0.4281
38 0.2000 C.0 -0.0361 0.2000 0.2115 0.3039 0.9891 4.0577 C.0044 -0.0076 1.0000 -0.374E+01 C.388E+00
0.3878 C.5919 C.9556 -0.0936 -0.3115 3.2969 0.4362 0.2000 0.2000 -0.4341
39 0.4000 C.1000 -0.0234 0.4000 0.2919 0.3078 0.0755 4.0872 C.0056 -0.0076 1.0000 0.140E+00 C.283E-01
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64	0.48000	0.48517	0.48000	0.60290	0.58142	0.67252	3.67387	0.00220	0.00533	1.00000	0.413E+00	0.679E-02
	0.0347	0.9515	-0.1873	-0.2192	3.0927	0.4362	0.9220	0.6000	-0.429E			
65	0.70000	0.0	0.26382	0.70000	0.50243	0.62580	0.00174	3.85366	-0.00102	0.07360	1.00000	-0.549E+01
	0.1914	0.9754	-0.2018	0.50243	3.1257	0.4362	0.7000	0.7000	-0.2633			
66	0.70000	0.2702	0.70000	0.50243	0.63197	0.08635	3.84832	-0.00218	-0.00831	1.00000	0.168E+00	0.535E-01
	0.1837	0.2682	0.9787	-0.2030	-0.0303	3.1237	0.4362	0.7071	0.7000	-0.4617		
67	0.70000	0.29183	0.70000	0.5167	0.63665	0.17597	3.83108	-0.00151	-0.00420	1.00000	0.367E+00	0.131E-01
	0.1656	0.2411	0.9710	-0.2047	-0.0591	3.1168	0.4362	0.7280	0.7000	-0.457E		
68	0.70000	0.32539	0.70000	0.5367	0.66429	0.27376	3.80364	-0.00644	-0.00459	1.00000	0.386E+00	0.100E-01
	0.1346	0.1952	0.9761	-0.2075	-0.0896	3.1076	0.4362	0.7616	0.7000	-0.4511		
69	0.70000	0.37004	0.70000	0.5544	0.65362	0.37141	3.76727	-0.00944	-0.00376	1.00000	0.406E+00	0.609E-02
	0.0909	0.1311	0.9699	-0.2111	-0.1211	3.0984	0.4362	0.8062	0.7000	-0.4436		
70	0.70000	0.42005	0.70000	0.58145	0.66462	0.47212	3.72308	0.00135	-0.00297	1.00000	0.418E+00	0.553E-02
	0.0355	0.0510	0.9646	-0.2145	-0.1517	3.0917	0.8612	0.8612	0.7000	-0.4360		
71	0.70000	0.48517	0.70000	0.60290	0.67369	0.57539	3.67386	0.00170	-0.00600	1.00000	0.406E+00	0.868E-02
	0.0347	0.9496	0.9515	-0.1886	-0.1886	3.0915	0.4362	0.9220	0.7000	-0.429E		
72	0.70000	0.55316	0.70000	0.61574	0.69011	0.64417	3.61973	0.00944	-0.00626	1.00000	0.409E+00	0.719E-02
	0.1149	0.1639	0.9402	-0.2222	-0.2226	3.1015	0.4362	0.9895	0.7000	-0.4266		
73	0.70000	0.0	0.34382	0.80000	0.55275	0.74449	0.00178	3.77239	-0.00251	0.00301	1.00000	-0.692E+01
	0.0970	0.1401	0.9705	-0.2240	0.0004	3.0994	0.4362	0.8000	0.8000	-0.4445		
74	0.80000	0.13000	0.37004	0.80000	0.55449	0.74638	0.08588	3.76727	-0.00156	-0.00592	1.00000	0.251E+00
	0.0909	0.1311	0.9699	-0.2244	-0.0303	3.0984	0.4362	0.8062	0.8000	-0.4436		
75	0.80000	0.38864	0.80000	0.56481	0.75087	0.18479	3.75159	0.00270	-0.00468	1.00000	0.362E+00	0.188E-01
	0.0330	0.1052	0.9682	-0.2245	-0.0612	3.0953	0.4362	0.8246	0.8000	-0.440E		
76	0.80000	0.44522	0.80000	0.57539	0.75769	0.28152	3.72377	0.00285	-0.00358	1.00000	0.399E+00	0.103E-01
	0.0419	0.0602	0.9602	-0.2248	-0.0922	3.0921	0.8621	0.8621	0.7000	-0.4367		
77	0.80000	0.49524	0.80000	0.59414	0.76679	0.38054	3.69571	0.00270	-0.00367	1.00000	0.406E+00	0.798E-02
	0.0428	0.0640	0.9608	-0.2248	-0.1244	3.0910	0.4362	0.8944	0.8000	-0.4322		
78	0.80000	0.50121	0.80000	0.60599	0.77668	0.48359	3.65609	0.00510	-0.00208	1.00000	0.424E+00	0.384E-02
	0.0580	0.0828	0.9552	-0.2509	-0.1570	3.0933	0.4362	0.9434	0.8000	-0.4283		
79	0.80000	0.56381	0.80000	0.62144	0.78978	0.58715	3.61078	0.00225	-0.00447	1.00000	0.414E+00	0.824E-02
	0.1249	0.1780	0.9463	-0.2538	-0.1907	3.1027	0.4362	0.9900	0.8000	-0.4263		
80	0.80000	0.0	0.46382	0.90000	0.59474	0.86261	0.00277	3.69091	-0.00447	0.00352	1.00000	-0.969E+01
	0.0093	0.0118	0.9632	-0.2752	0.0004	3.0907	0.4362	0.9000	0.8000	-0.4317		
81	0.80000	0.46545	0.90000	0.59474	0.86469	0.08890	3.68703	-0.00134	-0.00109	1.00000	0.131E+00	0.877E-01
	0.0160	0.0229	0.9545	-0.2801	-0.1321	3.0914	0.4362	0.9955	0.8000	-0.4312		
82	0.90000	0.48517	0.90000	0.61297	0.86857	0.18553	3.67387	-0.00155	-0.00509	1.00000	0.359E+00	0.212E-01
	0.0347	0.0496	0.9575	-0.2814	-0.0627	3.0927	0.4362	0.9270	0.8000	-0.4298		
83	0.90000	0.51250	0.90000	0.61444	0.87494	0.28874	3.65245	-0.00144	-0.00426	1.00000	0.393E+00	0.113E-01
	0.0656	0.0937	0.9547	-0.2832	-0.0947	3.0946	0.4362	0.9487	0.8000	-0.4281		
84	0.90000	0.54870	0.90000	0.61444	0.88361	0.38524	3.62002	-0.00253	-0.00536	1.00000	0.396E+00	0.952E-02
	0.1094	0.1561	0.9408	-0.2858	-0.1273	3.1006	0.4362	0.9849	0.8000	-0.4267		
85	0.90000	0.29476	0.10000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0436	0.0652	0.9099	0.0121	-0.0145	3.0927	0.4362	0.9141	-0.00147	-0.00538	1.00000	-0.130E+00
86	0.90000	0.21258	0.10000	0.11248	1.10561	4.22624	0.00952	-0.00668	1.00000	0.239E+00	0.586E-02	
	0.0483	0.07175	0.9093	-0.0185	-0.0337	3.0659	0.4362	0.9141	-0.00147	-0.00538	1.00000	-0.130E+00
87	0.90000	0.33000	0.11000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

0.4252	0.6571	0.9978	0.0215	-0.0624	3.3640	0.4362	0.3162	-0.1070	-0.5573
0e-c.10000	0.49000-0.02387	-0.10077	1.29184-0.07596	0.32767	4.08773	0.10428-0.00029	1.00000	0.433E+00	C.420E-02
0.53813	C.5681	C.9953	0.1244	-0.0937	3.2874	0.4362	0.4123	-0.1000	-0.5385
09-c.10000	0.49000-0.17372	0.10000	0.37143-0.08115	0.41255	4.09527	0.00435	0.00051	1.00000	0.440E+00
0.43302	C.49499	0.9914	0.1020	-0.1120	3.2209	0.4362	0.5092	-0.1000	-0.5385
90-c.10000	0.60000	0.17209-0.10070	0.44355-0.08512	0.52055	3.92863	0.00470	0.00199	1.00000	0.443E+00
0.22452	C.3924	0.9980	0.0282	-0.1642	3.1644	0.4362	0.6083	0.1070	-0.4842
91-c.10000	C.76882	0.9787	0.0257	-0.2531	3.1237	0.4362	0.7071	-0.1000	-0.4617
0.18837	C.76882	0.9787	0.0257	-0.2531	3.1237	0.4362	0.7071	-0.1000	-0.4617
92-c.10000	C.80000	0.37004-0.10000	0.55858-0.09194	0.74424	3.76127	0.00390-0.00119	1.00000	0.429E+00	C.375E-02
0.0909	0.1311	0.9699	0.0307	-0.2414	3.0984	0.4362	0.8062	-0.1070	-0.4436
93-c.10000	C.90000	0.46935-0.10000	0.59788-0.09367	0.86419	3.68702	0.00351-0.00120	1.00000	0.425E+00	C.328E-02
0.01599	C.90000	0.46935	0.0314	-0.2832	3.0914	0.4362	0.9055	-0.1000	-0.4312
94-c.10000	C.0	-0.23618-0.20000	0.09770-0.09844	0.00034	4.24016	0.01524	0.00549	1.00000	-0.327E+01
0.4646	C.0	0.99935	0.0329	0.0015	3.4683	0.4362	0.2000	-0.2000	-0.5835
95-c.10000	C.10000	0.21358-0.20000	0.12064-0.10921	0.05509	4.22611	0.00813	0.00190	1.00000	0.559E+00
0.4598	C.10000	0.21358	0.0361	-0.0154	3.4458	0.4362	0.2236	-0.2000	-0.5795
96-c.10000	C.20000	0.15334-0.20000	0.17644-0.12891	0.12939	4.18566	0.00444-0.00020	1.00000	0.431E+00	C.353E-02
0.4394	C.20000	0.15334	0.0362	0.0382	3.3925	0.4362	0.2828	-0.2000	-0.5661
97-c.10000	C.30000	0.07563-0.20000	0.24665-0.14513	0.21662	4.12814	0.00441	0.00101	1.00000	0.452E+00
0.4076	C.30000	0.07563	0.0449	-0.0655	3.3274	0.4362	0.3076	-0.2000	-0.5467
98-c.10000	C.40000	0.01173-0.20000	0.32110-0.15752	0.31662	4.06009	0.00370-0.00112	1.00000	0.425E+00	C.313E-02
0.3646	C.40000	0.01173	0.0449	-0.0914	3.2622	0.4362	0.4472	-0.2000	-0.5242
99-c.10000	C.50000	0.10233-0.20000	0.39328-0.16587	0.41573	3.98518	0.00517	0.00243	1.00000	0.455E+00
0.3128	C.50000	0.10233	0.0542	-0.1303	3.2024	0.4362	0.5385	-0.2000	-0.5014
100-c.10000	C.60000	0.19627-0.20000	0.45595-0.17359	0.52632	3.90911	0.00442-0.00003	1.00000	0.436E+00	C.441E-02
0.2460	C.60000	0.19627	0.0555	-0.1649	3.1532	0.4362	0.6325	-0.2000	-0.4783
101-c.10000	C.70000	0.25187-0.20000	0.51457-0.17956	0.63677	3.83108	0.00442-0.00128	1.00000	0.430E+00	C.442E-02
0.1656	C.70000	0.25187	0.0592	-0.2047	3.1168	0.4362	0.7280	-0.2000	-0.4575
102-c.10000	C.80000	0.38844-0.20000	0.56688-0.18473	0.75089	3.75187	0.00470	0.00030	1.00000	0.437E+00
0.0700	C.80000	0.38844	0.0661	-0.2425	3.0953	0.4362	0.8746	-0.2000	-0.440E
103-c.10000	C.90000	0.48577-0.20000	0.60297-0.19002	0.86846</					

0.1346 C.1952 0.9741 0.0857 -0.2074 3.1076 0.4362 0.7616 -0.3000 -0.4511
112-0.3000 C.8000 0.4182 -0.3000 0.5754 -0.2813 0.7577 3.7276 0.0039 0.0000 0.440E+00 C.429E-02
0.0419 0.0602 0.0952 0.0923 -0.2448 3.0921 0.4362 0.8544 -0.3000 -0.4367
113-0.3000 C.5000 0.5125 -0.3000 0.6154 -0.2865 0.8749 3.6524 0.3043 -0.0241 1.0000 0.431E+00 C.351E-02
0.0656 0.0937 0.0544 0.0000 0.2832 3.0946 0.4362 0.9487 -0.3000 -0.4281
114-0.4000 C.0 -0.0361 -0.4000 0.2813 -0.3039 0.4362 0.0091 4.0977 0.0042 0.0042 1.0000 -0.374E+01 -C.388E+00
0.3878 0.5919 0.0956 0.0036 0.0011 3.2969 0.4362 0.4000 -0.4000 -0.5361
115-0.4000 C.1000 0.0238 -0.4000 0.2918 -0.3069 0.4362 0.0073 4.0873 0.0033 0.0033 1.0000 0.346E+00 C.324E-01
0.3841 0.5841 0.0953 0.0943 -0.0218 3.2267 0.4362 0.4123 -0.4000 -0.5335
116-0.4000 C.2500 0.0113 -0.4000 0.3211 -0.3159 0.4362 0.1588 4.0679 0.0032 0.0032 1.0000 0.467E+00 C.670E-02
0.3644 0.5527 0.0940 0.0980 -0.0482 3.2622 0.4362 0.4472 -0.4000 -0.5242
117-0.4000 C.3000 0.0639 -0.4000 0.3636 -0.3695 0.4362 0.4158 4.0158 0.0054 0.0054 1.0000 0.467E+00 C.866E-02
0.3347 0.5033 0.0918 0.1030 -0.0719 3.2267 0.4362 0.5000 -0.4000 -0.5107
118-0.4000 C.4000 0.1255 -0.4000 0.4134 -0.3386 0.4362 0.3963 4.0033 0.0033 0.0033 1.0000 0.464E+00 C.634E-02
0.2947 0.4000 0.0947 0.0918 0.1127 -0.1354 3.1497 0.4362 0.6403 -0.4000 -0.4764
119-0.4000 C.5000 0.2043 -0.4000 0.4651 -0.3503 0.4362 0.4084 3.9022 0.0043 0.0043 1.0000 0.448E+00 C.623E-02
0.2398 0.3531 0.0918 0.1127 -0.1354 3.1497 0.4362 0.6403 -0.4000 -0.4764
120-0.4000 C.6000 0.2843 -0.4000 0.5146 -0.3602 0.4362 0.3867 3.8367 0.0056 0.0056 1.0000 0.435E+00 C.603E-02
0.1718 0.2503 0.0977 0.1174 -0.1174 3.1608 0.4362 0.7211 -0.4000 -0.4589
121-0.4000 C.7000 0.3704 -0.4000 0.5585 -0.3705 0.4362 0.3612 3.7612 0.0052 0.0052 1.0000 0.438E+00 C.545E-02
0.0909 0.1311 0.0969 0.1213 -0.2116 3.0984 0.4362 0.8062 -0.4000 -0.4436
122-0.4000 C.8000 0.4582 -0.4000 0.5941 -0.3793 0.4362 0.3471 3.6941 0.0047 0.0047 1.0000 0.439E+00 C.510E-02
0.0030 0.0043 0.0605 0.1245 -0.2474 3.0910 0.4362 0.8944 -0.4000 -0.4322
123-0.4000 C.9000 0.5482 -0.4000 0.6181 -0.3887 0.4362 0.3284 3.6284 0.0040 0.0040 1.0000 0.425E+00 C.501E-02
0.1094 0.1561 0.0948 0.1273 -0.2858 3.1006 0.4362 0.9849 -0.4000 -0.4247
124-0.5000 C.0 0.0639 -0.5000 0.3636 -0.4084 0.4362 0.4156 4.0156 0.0039 0.0039 1.0000 -0.411E+01 -0.584E+00
0.3347 0.0933 0.0941 0.1279 0.0012 3.2265 0.4362 0.5000 -0.5000 -0.5107
125-0.5000 C.1000 0.0727 -0.5000 0.3714 -0.4184 0.4362 0.4047 4.0047 0.0019 0.0019 1.0000 0.737E+00 0.409E-01
0.3302 0.4959 0.0914 0.1285 -0.0244 3.2200 0.4362 0.5095 -0.5000 -0.5085
126-0.5000 C.2000 0.1023 -0.5000 0.3932 -0.4185 0.4362 0.3857 3.9857 0.0014 0.0014 1.0000 0.504E+00 C.997E-02
0.3128 0.4677 0.0909 0.1310 -0.0516 3.2025 0.4362 0.5385 -0.5000 -0.5014
127-0.5000 C.3000 0.1469 -0.5000 0.4259 -0.4272 0.4362 0.2588 3.9465 0.0017 0.0017 1.0000 0.470E+00 0.481E-02
0.2816 0.4183 0.0914 0.1359 -0.0845 3.1778 0.4362 0.5831 -0.5000 -0.4909
128-0.5000 C.4000 0.2043 -0.5000 0.4651 -0.4382 0.4362 0.3927 3.9027 0.0045 0.0045 1.0000 0.461E+00 0.401E-02
0.2398 0.3531 0.0918 0.1406 -0.1113 3.1607 0.4362 0.6403 -0.5000 -0.4764
129-0.5000 C.5000 0.2709 -0.5000 0.5164 -0.4491 0.4362 0.3612 3.8362 0.0052 0.0052 1.0000 0.447E+00 0.782E-02
0.1837 0.2582 0.0917 0.1458 -0.1445 3.1237 0.4362 0.8481 0.0042 0.0042 1.0000 0.447E+00 0.782E-02
130-0.5000 C.6000 0.3464 -0.5000 0.5465 -0.4672 0.4362 0.3462 3.7872 0.0051 0.0051 1.0000 0.452E+00 C.747E-02
0.1169 0.1691 0.0924 0.1469 -0.1766 3.1028 0.4362 0.7816 -0.5000 -0.4478
131-0.5000 C.7000 0.4245 -0.5000 0.5816 -0.4781 0.4362 0.3284 3.6284 0.0040 0.0040 1.0000 0.449E+00 0.696E-02
0.0355 0.0519 0.0946 0.1539 -0.2144 3.0917 0.4362 0.8602 -0.5000 -0.4364
132-0.5000 C.8000 0.5125 -0.5000 0.6154 -0.4891 0.4362 0.3091 3.5691 0.0035 0.0035 1.0000 0.443E+00 0.518E-02
0.0580 0.0929 0.0952 0.1572 -0.2578 3.0933 0.4362 0.9487 -0.5000 -0.4283
133-0.6000 C.0 0.1630 -0.6000 0.4378 -0.5183 0.4362 0.4372 4.0372 0.0033 0.0033 1.0000 -0.466E+01 -0.845E+00
0.2700 0.3909 0.0944 0.1641 0.0011 3.1649 0.4362 0.6000 -0.6000 -0.4860
134-0.6000 C.1000 0.1729 -0.6000 0.4436 -0.5208 0.4362 0.4284 4.0284 0.0041 0.0041 1.0000 0.441E+00 0.359E-03
0.2652 0.3924 0.0944 0.1643 -0.2772 3.1644 0.4362 0.6000 -0.6000 -0.4862
135-0.6000 C.2000 0.1962 -0.6000 0.4505 -0.5247 0.4362 0.4178 3.9077 0.0034 0.0034 1.0000 0.541E+00 0.212E-01

0.2460	C.3628	C.9844	C.1676	-0.0546	3.1532	0.4362	0.6325	-0.6000	-0.4783
136-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
137-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
138-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
139-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
140-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
141-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
142-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
143-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
144-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
145-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
146-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
147-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
148-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
149-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
150-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
151-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
152-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
153-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
154-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
155-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
156-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
157-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
158-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142
159-0.60000	C.30000	0.23464	0.60000	0.48472	-0.5339	0.26695	3.87799	0.00280	-0.00142

0.0656 C.0937 0.9544 0.2834 -0.0942 3.7946 0.4362 0.9487 -0.9000 -0.4281
160-C.50000 0.40000 0.54870-0.90000 0.61880-0.88103 0.39504 3.62402 0.0567 0.0017 1.00000 0.449E+00 0.955E-02
0.1094 C.1561 0.9458 0.2860 -0.1269 3.1006 0.4162 0.9848 -0.9000 -0.4267
IMPROP IMAGE SKEW RAYS FOLLOW

IMAGE RAY	RAY	RAY2	OPL	VLM	ZIP	NTCTV	XDIAP1 YDIAP1
161	1 0.0	-0.2000000	4.24078274	0.0054853	0.0164587	1.0000000	-0.603E-01 0.475E-02
162	2 0.0	-0.3000001	4.17357540	0.0031923	0.0931132	1.0000000	0.395E+00 0.315E-02
163	3 0.0	-0.4000001	4.09772682	0.0028070	0.0746203	1.0001000	0.387E+00 0.277E-02
164	4 0.0	-0.5000001	4.01756477	0.0019502	0.0022974	1.0001000	0.413E+00 0.393E-02
165	5 0.0	-0.6000001	3.93575191	0.0043350	0.0016529	1.0000000	0.426E+00 0.433E-02
166	6 0.0	-0.7000002	3.85365105	0.0044867	0.0010263	1.0001000	0.431E+00 0.448E-02
167	7 0.0	-0.8000002	3.77228750	0.0036257	0.0024981	1.0000000	0.426E+00 0.362E-02
168	8 0.0	-0.9000002	3.69091415	0.0039220	0.0003997	1.0000000	0.435E+00 0.392E-02
169	9 0.1000000-0.1000000	4.27035427	-0.0053825	0.0147110	1.0000000	-0.781E+00 0.619E-02	
170	10 0.1000000-0.2000000	4.22626493	0.0003680	0.0116265	1.0000000	0.155E+00 0.564E-02	
171	11 0.1000000-0.3000001	4.16185284	0.0008731	0.0057240	1.0000000	0.345E+00 0.272E-02	
172	12 0.1000000-0.4000001	4.08772659	0.0036370	0.0022712	1.0000000	0.412E+00 0.418E-02	
173	13 0.1000000-0.5000001	4.00919724	0.0042109	0.0012001	1.0000000	0.427E+00 0.444E-02	
174	14 0.1000000-0.6000001	3.92863179	0.0041304	0.0002688	1.0000000	0.435E+00 0.417E-02	
175	15 0.1000000-0.7000002	3.84831239	0.0038219	0.0038793	1.0000000	0.418E+00 0.436E-02	
176	16 0.1000000-0.8000002	3.76727295	0.0036144	0.0027167	1.0000000	0.425E+00 0.374E-02	
177	17 0.1000000-0.9000002	3.68722126	0.0029792	0.0007347	1.0000000	0.427E+00 0.394E-02	
178	18 0.2000000-0.1000000	4.22610664	-0.00133557	0.0076477	1.0000000	0.112E-01 0.176E-01	
179	20 0.2000000-0.2000000	4.18595896	-0.00102034	0.0041443	1.0000000	0.331E+00 0.483E-02	
180	21 0.2000000-0.3000001	4.12814045	0.00076273	0.00036002	1.0000000	0.381E+00 0.571E-02	

181	22 0.200000-0.400000	4.06009197	0.0013279	0.0036302	1.0000000	0.399E+00
182	23 0.200000-0.500000	3.98577595	0.0054189	0.0018111	1.0000000	0.423E+00
183	24 0.200000-0.600000	3.90910721	0.0035214	0.0026788	1.0000000	0.420E+00
184	25 0.200000-0.700000	3.83107567	0.0035610	0.0037240	1.0000000	0.440E+00
185	26 0.200000-0.800000	3.75158841	0.0043493	0.0015773	1.0000000	0.418E+00
186	27 0.200000-0.900000	3.67387295	0.0032785	0.0034030	1.0000000	0.428E+00
187	28 0.300000-0.100000	4.16185093	-0.0039418	0.0044041	1.0000000	0.435E+00
188	29 0.300000-0.200000	4.12813854	0.0014287	0.0050400	1.0000000	0.423E+00
189	30 0.300000-0.300000	4.07840347	0.0018931	0.0058762	1.0000000	0.417E+00
190	31 0.300000-0.400000	4.01757240	0.0019007	0.0052012	1.0000000	0.356E+00
191	32 0.300000-0.500000	3.94968891	0.0016769	0.0035137	1.0000000	0.386E+00
192	33 0.300000-0.600000	3.87755168	-0.0016308	0.0028040	1.0000000	0.542E+00
193	34 0.300000-0.700000	3.80363274	0.0038987	0.0042795	1.0000000	0.411E+00
194	35 0.300000-0.800000	3.72776127	0.0035967	0.0018350	1.0000000	0.377E+00
195	36 0.300000-0.900000	3.65244675	0.0026590	0.0037535	1.0000000	0.420E+00
196	37 0.400000-0.100000	4.08772755	0.0010500	0.0074429	1.0000000	0.424E+00
197	38 0.400000-0.200000	4.06078530	-0.0010338	0.0038719	1.0000000	0.391E+00
198	39 0.400000-0.300000	4.01757717	0.0010715	0.0059121	1.0000000	0.140E+00
199	40 0.400000-0.400000	3.96364498	0.0030038	0.0033162	1.0000000	0.358E+00
200	41 0.400000-0.500000	3.90272331	0.0026956	0.0044063	1.0000000	0.361E+00
201	42 0.400000-0.600000	3.83672813	0.0012685	0.0050118	1.0000000	0.846E+00
202	43 0.400000-0.700000	3.76726542	0.0028799	0.0043193	1.0000000	0.406E+00
203	44 0.400000-0.800000	3.69570827	0.0034177	0.0033785	1.0000000	0.416E+00
204	45 0.400000-0.900000	3.62401772	0.0023645	0.0059649	1.0000000	0.423E+00
						0.500E+00

205	45 0.50C0001-0.1000000	4.00919342	0.0011327	0.0015034	1.0000000	0.163E+00
206	50 0.50C0001-0.2000000	3.98578451	0.0016674	0.0032669	1.0000000	0.375E+00
207	51 0.50C0001-0.3000001	3.94968987	0.0004574	0.0049669	1.0000000	0.971E-02
208	52 0.50C0001-0.4000001	3.90212522	0.0017131	0.0049861	1.0000000	0.376E+00
209	53 0.50C0001-0.5000001	3.84830855	0.0015668	0.0062363	1.0000000	0.863E-02
210	54 0.50C0001-0.6000001	3.78745365	0.0037896	0.0043965	1.0000000	0.354E+00
211	55 0.50C0001-0.7000002	3.72307014	0.0042505	0.0037777	1.0000000	0.743E-02
212	56 0.50C0001-0.8000002	3.65608788	0.0033600	0.0029077	1.0000000	0.425E+00
213	58 0.60C0001-0.1000000	3.92862511	0.0004095	0.0001280	1.0000000	0.441E+00
214	55 0.60C0001-0.2000000	3.90910721	0.0007309	0.0061502	1.0000000	-0.359E-03
215	60 0.6000001-0.3000001	3.87799454	-0.0028021	0.0014182	1.0000000	0.429E+00
216	61 0.60C0001-0.4000001	3.83672237	0.0009093	0.0062014	1.0000000	0.341E-04
217	62 0.60C0001-0.5000001	3.78746128	0.0011321	0.0028399	1.0000000	0.385E+00
218	62 0.60C0001-0.6000001	3.73239708	0.0039017	0.0035634	1.0000000	0.418E+00
219	64 0.60C0001-0.7000002	3.67366723	0.0022002	0.0053294	1.0000000	0.415E+00
220	64 0.70C0002-0.1000000	3.84832956	-0.0023794	0.0083067	1.0000000	0.675E-02
221	67 0.70C0002-0.2000000	3.83107759	-0.0015110	0.0042030	1.0000000	0.168E+00
222	68 0.70C0002-0.3000001	3.80363560	-0.0006356	0.0045882	1.0000000	0.535E-01
223	65 0.70C0002-0.4000001	3.76777200	-0.0004658	0.0031591	1.0000000	0.367E+00
224	70 0.70C0002-0.5000001	3.72307587	0.0013372	0.0029685	1.0000000	0.170E-01
225	71 0.70C0002-0.6000001	3.67386246	0.0017003	0.0060047	1.0000000	0.479E+00
226	72 0.70C0002-0.7000002	3.61912521	0.0009379	0.0062600	1.0000000	0.868E-02
227	74 0.80C0002-0.1000000	3.76777200	-0.0015622	0.0056170	1.0000000	0.479E+00
228	75 0.80C0002-0.2000000	3.75156127	0.0007749	0.0046778	1.0000000	0.251E+00

229	76	0.8000002-0.3000001	3.72776508	0.00000000	0.0035773	1.00000000	0.3995+00
230	77	0.8000002-0.4000001	3.69571118	0.00000000	0.0038705	1.00000000	0.4000+00
231	78	0.8000002-0.5000001	3.65668978	0.00000000	0.0020849	1.00000000	0.4245+00
232	79	0.8000002-0.6000001	3.61070167	0.00000000	0.0044706	1.00000000	0.4384+00
233	80	0.8000002-0.7000000	3.68702984	-0.00013421	0.0011870	1.00000000	0.4414+00
234	81	0.8000002-0.8000000	3.67387295	-0.00015483	0.0005086	1.00000000	0.4559+00
235	82	0.8000002-0.9000000	3.65244961	-0.00014436	0.0042624	1.00000000	0.4624+00
236	83	0.9000002-0.4000001	3.62401962	-0.00025264	0.0053644	1.00000000	0.4795+00
237	84	0.9000002-0.5000000	4.27035427	0.00147112	0.0053823	1.00000000	0.4878+00
238	85	0.9000002-0.6000000	4.22624493	0.00095235	0.0066810	1.00000000	0.4940+00
239	86	0.9000002-0.7000000	4.16185284	0.00041337	0.0040556	1.00000000	0.5011+00
240	87	0.9000002-0.8000000	4.08772659	0.00042783	0.0002921	1.00000000	0.5082+00
241	88	0.9000002-0.9000000	4.00919724	0.00043494	-0.0005121	1.00000000	0.5153+00
242	89	0.9000002-0.0000001	3.92863178	0.00039951	-0.0010854	1.00000000	0.5224+00
243	90	0.9000002-0.1000000	3.84831238	0.00047560	0.0026555	1.00000000	0.5295+00
244	91	0.9000002-0.2000000	3.76727295	0.00039786	0.0017930	1.00000000	0.5366+00
245	92	0.9000002-0.3000000	3.68702126	0.00035077	0.0020164	1.00000000	0.5437+00
246	93	0.9000002-0.4000000	4.22610664	0.00081304	0.0019015	1.00000000	0.5508+00
247	94	0.9000002-0.5000000	4.15555886	0.00041428	0.0002035	1.00000000	0.5579+00
248	95	0.9000002-0.6000000	4.12814045	0.00044076	-0.0001010	1.00000000	0.5650+00
249	96	0.9000002-0.7000000	4.06009197	0.00037007	0.0011150	1.00000000	0.5721+00
250	97	0.9000002-0.8000000	3.95577981	0.00051745	0.0024257	1.00000000	0.5792+00
251	98	0.9000002-0.9000000	3.90910721	0.00044245	0.0000304	1.00000000	0.5863+00
252	99	0.9000002-0.0000000	3.83107567	0.00049914	0.0012819	1.00000000	0.5934+00

253	102-0.20C0001-0.6000002	3.75150041	0.0047601-0.0003010	1.0000000	0.437E+00	
254	103-0.20C0001-0.5000002	3.67307295	0.0044110	0.016944	1.0000000	0.430E+00
255	105-0.30C0001-0.1000000	4.16105193	0.0058174-0.0011642	1.0000000	0.494E+00	
256	106-0.30C0001-0.2000000	4.12013054	0.0041020-0.0032503	1.0000000	0.945E+00	
257	107-0.30C0001-0.3000001	4.07040347	0.0050767-0.0010906	1.0000000	0.512E+00	
258	108-0.30C0001-0.4000001	4.01175724	0.0055401-0.0004456	1.0000000	0.463E+00	
259	109-0.30C0001-0.5000001	3.94560907	0.00330097	0.001729	1.0000000	0.441E+00
260	110-0.30C0001-0.6000001	3.87759168	0.0014008	0.0020040	1.0000000	0.509E+00
261	111-0.30C0001-0.7000002	3.80363274	0.0057077	0.0011203	1.0000000	0.435E+00
262	112-0.30C0001-0.8000002	3.72776127	0.0039150-0.0009017	1.0000000	0.420E+00	
263	113-0.30C0001-0.9000002	3.65244675	0.0043796	0.0014074	1.0000000	0.429E+00
264	115-0.40C0001-0.1000000	4.08772755	0.0030699-0.0067001	1.0000000	0.440E+00	
265	116-0.40C0001-0.2000000	4.06000539	0.0037223-0.0015037	1.0000000	0.431E+00	
266	117-0.40C0001-0.3000001	4.01757717	0.0054762-0.0023420	1.0000000	0.467E+00	
267	118-0.40C0001-0.4000001	3.96364498	0.0033165-0.0030042	1.0000000	0.464E+00	
268	119-0.40C0001-0.5000001	3.90272331	0.0040903-0.0016623	1.0000000	0.636E+00	
269	120-0.40C0001-0.6000001	3.83672010	0.0056508-0.0005514	1.0000000	0.448E+00	
270	121-0.40C0001-0.7000002	3.76726532	0.0052356-0.0003752	1.0000000	0.439E+00	
271	122-0.40C0001-0.8000002	3.69570027	0.0047471-0.0006909	1.0000000	0.545E+00	
272	123-0.40C0001-0.9000002	3.62461177	0.0060110	0.0022422	1.0000000	0.510E+00
273	125-0.50C0001-0.1000000	4.00919342	0.0010274-0.0073021	1.0000000	0.429E+00	
274	126-0.50C0001-0.2000000	3.90570453	0.0010440-0.0035129	1.0000000	0.473E+00	
275	127-0.50C0001-0.3000001	3.94960907	0.0041708-0.0027460	1.0000000	0.504E+00	
276	128-0.50C0001-0.4000001	3.90272617	0.0046054-0.0027000	1.0000000	0.470E+00	

277	125-0.5000001-0.5000001	3.04030056	0.0062366-0.0015669	1.0000000	0.447E+00
278	130-0.5000001-0.4000001	3.72745365	0.0050076-0.0029344	1.0000000	0.452E+00
279	131-0.5000001-0.7000002	3.72306919	0.0049517-0.0027953	1.0000000	0.449E+00
280	132-0.5000001-0.4000002	3.65608708	0.0040064-0.0017462	1.0000000	0.443E+00
281	134-0.6000001-0.1000000	3.92062511	-0.0004095-0.0001280	1.0000000	0.441E+00
282	135-0.6000001-0.2000000	3.90910625	0.0034603-0.0058221	1.0000000	0.541E+00
283	136-0.6000001-0.3000001	3.87759454	0.0020021	0.0014182	1.0000000
284	137-0.6000001-0.4000001	3.83672237	0.0033756-0.0032259	1.0000000	0.420E+00
285	138-0.6000001-0.5000001	3.78746128	0.0025805-0.0016244	1.0000000	0.447E+00
286	139-0.6000001-0.6000001	3.73239708	0.0039631-0.0039016	1.0000000	0.457E+00
287	140-0.6000001-0.7000002	3.67386723	0.0056053-0.0013611	1.0000000	0.442E+00
288	142-0.7000002-0.1000000	3.84032096	0.0043796-0.0071140	1.0000000	0.627E+00
289	143-0.7000002-0.2000000	3.83107758	0.0035011-0.0027625	1.0000000	0.564E+01
290	144-0.7000002-0.3000001	3.80363655	0.0037598-0.0027022	1.0000000	0.466E+00
291	145-0.7000002-0.4000001	3.76727270	0.0034752-0.0015071	1.0000000	0.440E+00
292	146-0.7000002-0.5000001	3.72307587	0.0023504-0.0022746	1.0000000	0.512E+02
293	147-0.7000002-0.6000001	3.67386532	0.0056748-0.0025954	1.0000000	0.491E+00
294	148-0.7000002-0.7000002	3.61972523	0.0062596-0.0005374	1.0000000	0.440E+00
295	150-0.8000002-0.1000000	3.76727270	0.0029543-0.0052318	1.0000000	0.608E+00
296	151-0.8000002-0.2000000	3.75190936	0.0019566-0.0042466	1.0000000	0.555E+01
297	152-0.8000002-0.3000001	3.72776699	0.0017095-0.0032434	1.0000000	0.479E+00
298	153-0.8000002-0.4000001	3.69571019	0.0029348-0.0025342	1.0000000	0.456E+00
299	154-0.8000002-0.5000001	3.65640978	0.0016521-0.0013728	1.0000000	0.445E+00
300	155-0.8000002-0.6000001	3.61077976	0.0036520-0.0034468	1.0000000	0.453E+00

301 157-0.9000002-0.1000000 3.62702964 0.0014646-0.0090484 1.0000000 0.733E+00
 302 156-0.9000002-0.0000000 3.67387199 0.0035476-0.0039124 1.0000000 0.496E+00
 303 155-0.5000002-0.2000001 3.65244675 0.0037126-0.0025461 1.0000000 0.213E-01
 304 160-0.9000002-0.4000001 3.62401562 0.0056730-0.0017174 1.0000000 0.449E+00
 0.955E-02

END OF SKEW RAY TRACE.

TOTAL NUMBER OF RAYS TRACED = 304
 TOTAL NUMBER OF RAYS STRIKING IMAGE PLANE = 144
 1 IMAGE PLANE SPOT DIAGRAM ANALYSIS:

THICKNESS = 0.0500000 U = 0.0 ALFAP = 0.0 R = 1.0000000
 CENTRIC: ZCENTR = 0.0, YCENTR = 0.0027303
 STANDARD DEVIATIONS: SIGMA Y = 0.0000795 SIGMA Z = 0.0000194
 RMS SPOT SIZE: RMSRAD = 0.0052860

SPECT DIAGRAM ENERGY DENSITY VS. RADIUS FROM CENTROID:

124	RADIUS	FRACTION
1	0.0000000	0.677E+16
2	0.0000000	0.940E+16
3	0.0000000	0.985E+16
4	0.0000000	0.990E+16
5	0.0000000	0.995E+16
6	0.0000000	0.998E+16
7	0.0000000	0.999E+16
8	0.0000000	0.999E+16
9	0.0000000	0.999E+16
10	0.0000000	0.999E+16
11	0.0000000	0.999E+16
12	0.0000000	0.999E+16
13	0.0000000	0.999E+16
14	0.0000000	0.999E+16
15	0.0000000	0.999E+16
16	0.0000000	0.999E+16
17	0.0000000	0.999E+16
18	0.0000000	0.999E+16
19	0.0000000	0.999E+16
20	0.0000000	0.999E+16
21	0.0000000	0.999E+16
22	0.0000000	0.999E+16
23	0.0000000	0.999E+16
24	0.0000000	0.999E+16
25	0.0000000	0.999E+16
26	0.0000000	0.999E+16
27	0.0000000	0.999E+16
28	0.0000000	0.999E+16
29	0.0000000	0.999E+16
30	0.0000000	0.999E+16
31	0.0000000	0.999E+16
32	0.0000000	0.999E+16
33	0.0000000	0.999E+16
34	0.0000000	0.999E+16
35	0.0000000	0.999E+16
36	0.0000000	0.999E+16
37	0.0000000	0.999E+16
38	0.0000000	0.999E+16
39	0.0000000	0.999E+16
40	0.0000000	0.999E+16
41	0.0000000	0.999E+16
42	0.0000000	0.999E+16
43	0.0000000	0.999E+16
44	0.0000000	0.999E+16
45	0.0000000	0.999E+16
46	0.0000000	0.999E+16
47	0.0000000	0.999E+16
48	0.0000000	0.999E+16
49	0.0000000	0.999E+16
50	0.0000000	0.999E+16
51	0.0000000	0.999E+16
52	0.0000000	0.999E+16
53	0.0000000	0.999E+16
54	0.0000000	0.999E+16
55	0.0000000	0.999E+16
56	0.0000000	0.999E+16
57	0.0000000	0.999E+16
58	0.0000000	0.999E+16
59	0.0000000	0.999E+16
60	0.0000000	0.999E+16
61	0.0000000	0.999E+16
62	0.0000000	0.999E+16
63	0.0000000	0.999E+16
64	0.0000000	0.999E+16
65	0.0000000	0.999E+16
66	0.0000000	0.999E+16
67	0.0000000	0.999E+16
68	0.0000000	0.999E+16
69	0.0000000	0.999E+16
70	0.0000000	0.999E+16
71	0.0000000	0.999E+16
72	0.0000000	0.999E+16
73	0.0000000	0.999E+16
74	0.0000000	0.999E+16
75	0.0000000	0.999E+16
76	0.0000000	0.999E+16
77	0.0000000	0.999E+16
78	0.0000000	0.999E+16
79	0.0000000	0.999E+16
80	0.0000000	0.999E+16
81	0.0000000	0.999E+16
82	0.0000000	0.999E+16
83	0.0000000	0.999E+16
84	0.0000000	0.999E+16
85	0.0000000	0.999E+16
86	0.0000000	0.999E+16
87	0.0000000	0.999E+16
88	0.0000000	0.999E+16
89	0.0000000	0.999E+16
90	0.0000000	0.999E+16
91	0.0000000	0.999E+16
92	0.0000000	0.999E+16
93	0.0000000	0.999E+16
94	0.0000000	0.999E+16
95	0.0000000	0.999E+16
96	0.0000000	0.999E+16
97	0.0000000	0.999E+16
98	0.0000000	0.999E+16
99	0.0000000	0.999E+16
100	0.0000000	0.999E+16

12. SUMMARY OF THE REPORT

Lens design and ray tracing to determine optical aberrations requires efficient computer codes. A clearly structured computer code with efficient algorithms has been developed to design a lens incorporating gradient refractive index, GRIN. One surface of the lens, either the inside or outside surface, is a circular cone.

The computer code includes lens design and calculation of optical aberration for a lens using a homogeneous material, i.e., for n equal to a constant. The homogeneous case is included for several reasons. The simpler case with n equal to a constant provides insight to the more complex case of variable n . Extensive computer codes require a check on the validity of the output. The homogeneous case provides a check. When the factor B is equal to zero in equation [2.9], the results for the two computer programs with and without GRIN should be identical. Needless to say, the results are identical for the programs reported here.

The case of a lens with GRIN and with a circular cone for the outside surface has been programmed. The companion case with the circular cone on the inside is being developed by Carr [15]. Carr's program can be readily incorporated into this computer code.

The program has been exercised for the case of 5% variation in refractive index for both negative and positive

values for B. The aim of the preliminary calculations was to verify operation of the computer program. More extensive calculations are required in order to understand the influence of various variables. As more experience is gained, the program should be combined with an optimization code to permit thorough and efficient lens design.

The selection of a 5% variation in refractive index was based on current state-of-the-art in the production of GRIN materials. A wider variation in refractive index may be needed.

The program is restricted currently to values of X_c satisfying the constraint $X_c \leq 0$. Additional work is needed to permit designs using positive values of X_c . When X_c is positive, the angle θ at some point along the ray interior to the lens has a critical value at which $dr/d\theta$ changes sign. The critical value causes computational difficulties.

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